

# Zero Mass Detector Project

Seth Zenz, 7 September 2022  
Future UK Silicon Vertex & Tracker R&D Workshop

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- Other example applications
- Large scale module construction
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  - Electrical performance
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- Summary

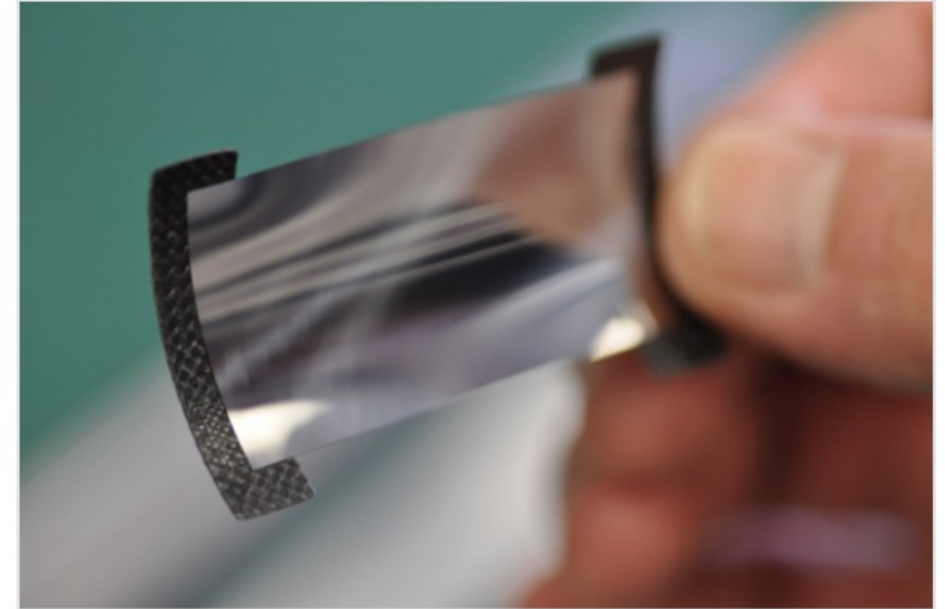


# Rationale

- Tracker mass degrades performance
- We want to:
  - Minimise support material
  - Minimise sensor material
  - Maintain electrical properties and measurement capability
  - Maintain consistent and well-described position

# Early Concept Prototyping

- Ultrathin silicon has long been known to be flexible
- Thin film theory predicts dislocations lock in on the surface, making strong stable structures
- Don't need to provide full frame to support a curved sensor
- **June 2012:** the STFC funded Arachnid project [CMOS MAPS] made curved silicon mechanical tokens and studied the shape. Tokens remain intact today; consistent with expectations.
  - Radius down to 13mm
  - 50  $\mu\text{m}$  samples easier to handle than 25  $\mu\text{m}$
- Rigid supports on two sides sufficient for a self-supporting silicon structure, but this talk focuses on results with 4-sided supports



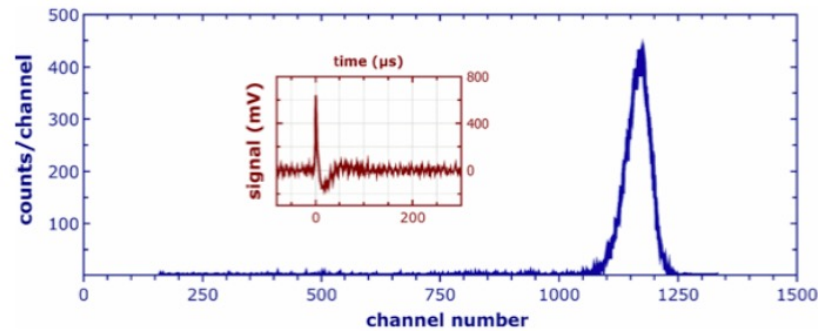
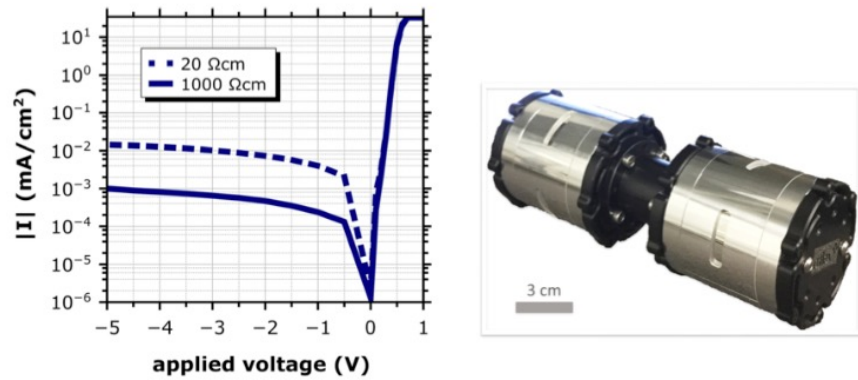
Curved silicon with a 2.5 cm radius of curvature on a carbon-fibre support, demonstrating the feasibility of making low-mass, rigid FCC-ee detector systems. Credit: Queen Mary University of London.

<https://cerncourier.com/a/spotlight-on-fcc-physics/>

# Other example applications

## Flexible silicon-based alpha-particle detector

C. S. Schuster et al., Appl. Phys. Lett. 111, 073505 (2017);  
<https://doi.org/10.1063/1.4999322>



## Imaging sensors: Curve One, CEA Leti, Sony produce these

Sensor plane matching the Petzal surface results in simpler optics (cheaper cameras)

e.g. Brian Guenter et al.

<https://doi.org/10.1364/OE.25.013010>

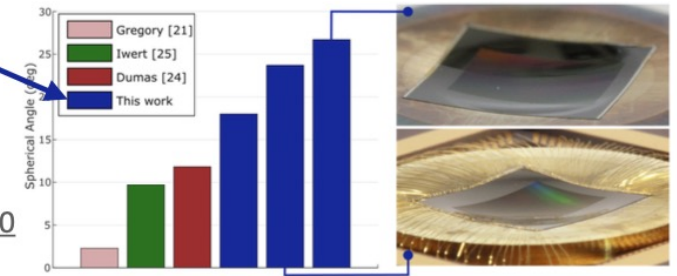
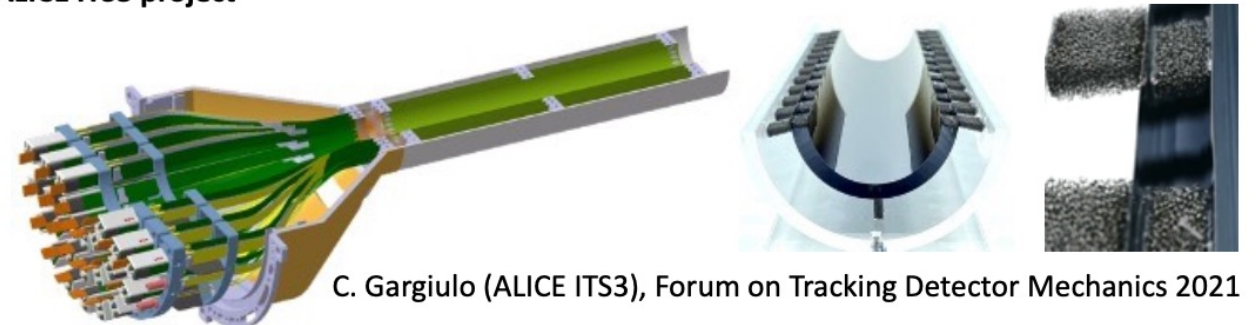


Fig. 5. Comparative graph of curvature achieved in working sensors between this work and the significant work from the literature. A wirebonded sensor used for one camera in this study is shown in the lower right, having a spherical curvature of 23.7°. The working sensor in the upper right has a curvature of 26.7° but could not be used for this study as it does not match the lens.

## ALICE ITS3 project

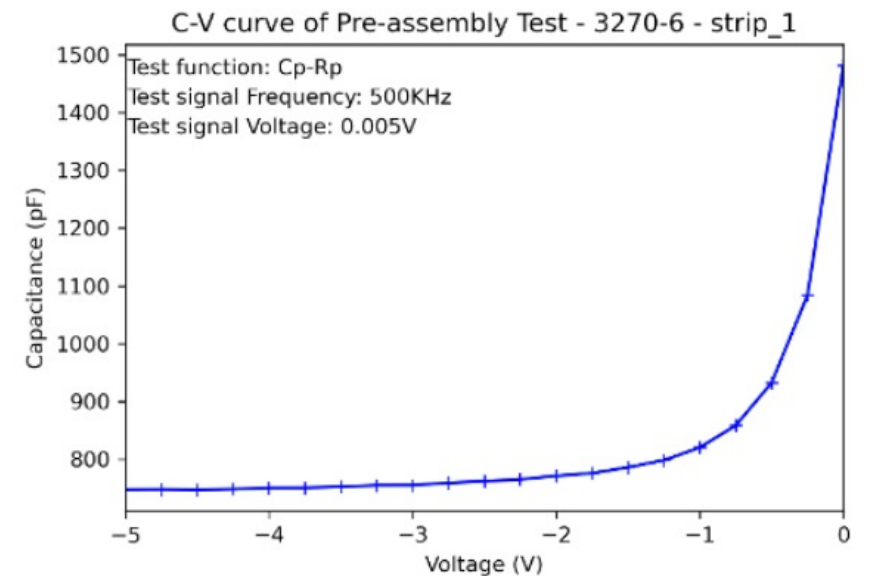
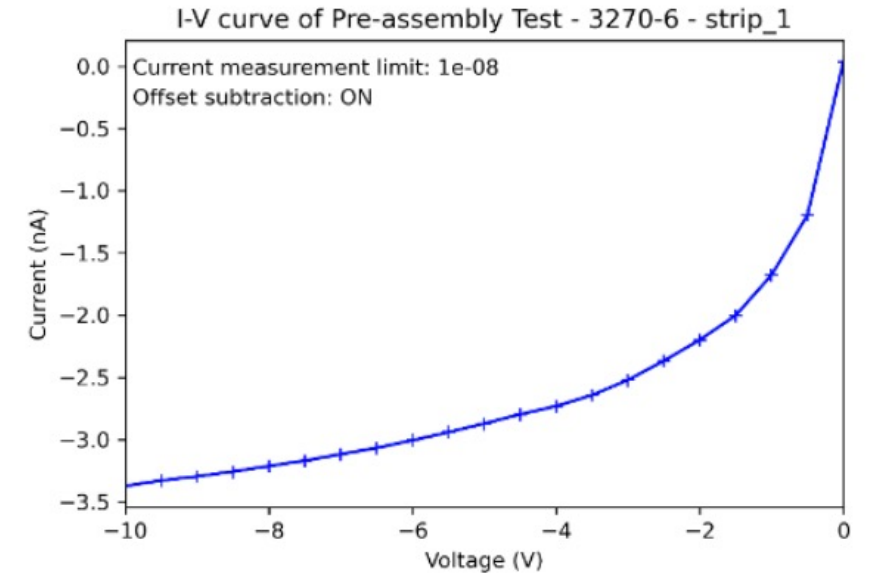
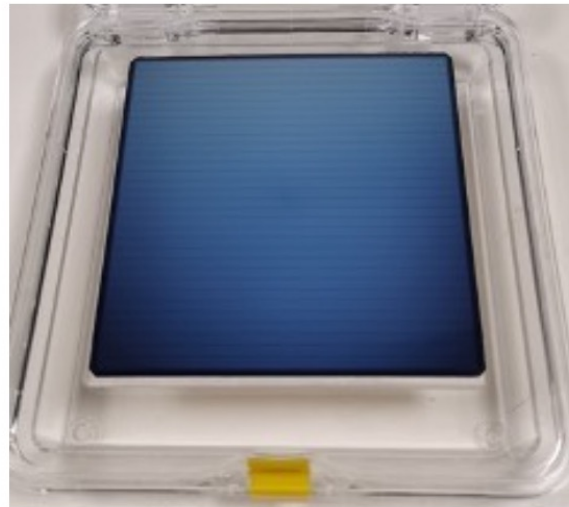


C. Gargiulo (ALICE ITS3), Forum on Tracking Detector Mechanics 2021

# Large Module Construction

- DC coupled TTT10 from Micron Semiconductor
- Sensors nominally  $50\mu\text{m}$ , with range of  $30\text{-}50\ \mu\text{m}$

Specification	TTT10
Thickness	$50\mu\text{m}$
Active Area	$100\text{mm}\times 100\text{mm}$
No. of Strips	32
Strip Pitch	3mm
Wafer Type	N-Type
Wafer Resistivity	5K ohm·cm
Metalizing	300nm Al
Wafer Technology	Float Zone
Orientation	[100]
Junction Depth	$0.5\mu\text{m}$
Strip Leakage Current	10nA Max

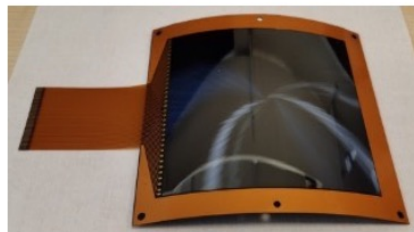


# Large Module Construction

- Focus on flat and R=150mm modules to demonstrate the concept
- Tokens made with R down to 13mm, so plenty of scope for changing the radius either way



Flat

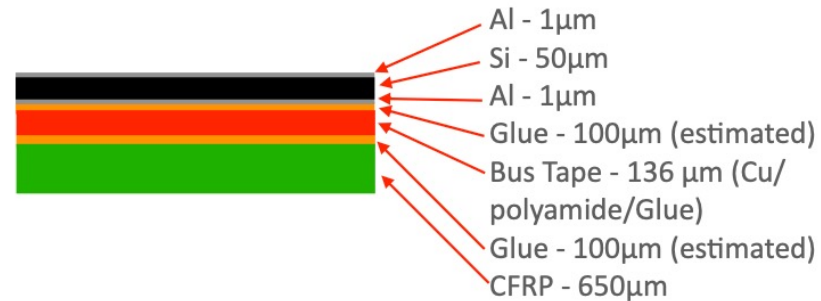


Convex, R=150mm

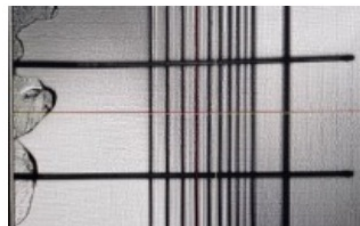


Concave, R=150mm

- Module layup for each of these variations is the same:



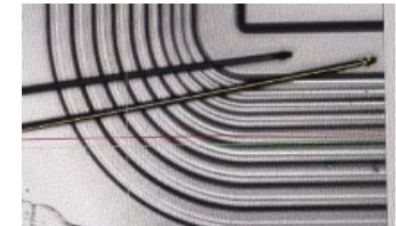
- Wirebonding is a little more tricky than with a flat module:



Bonding to a strip



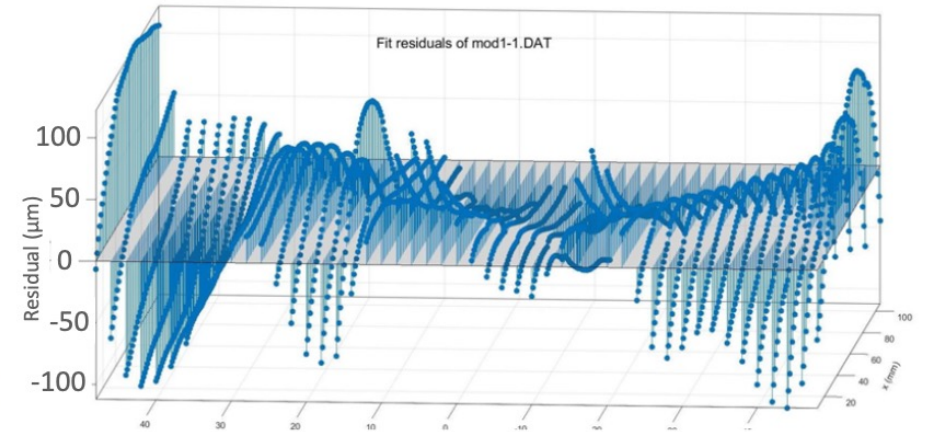
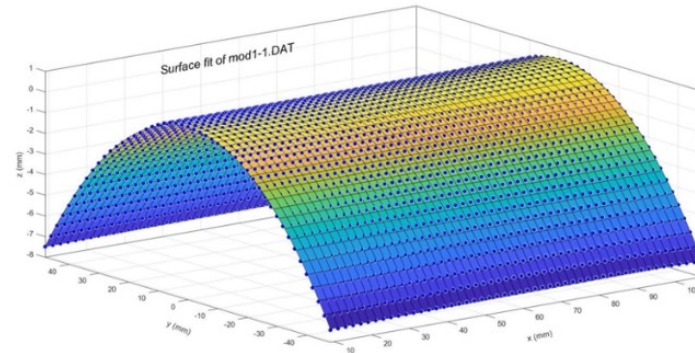
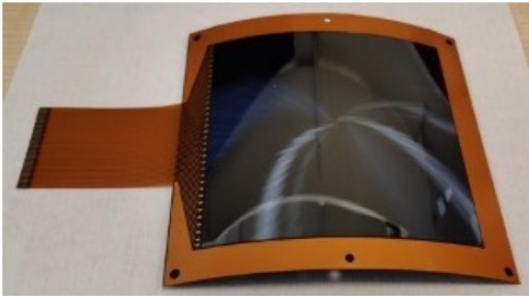
Overview



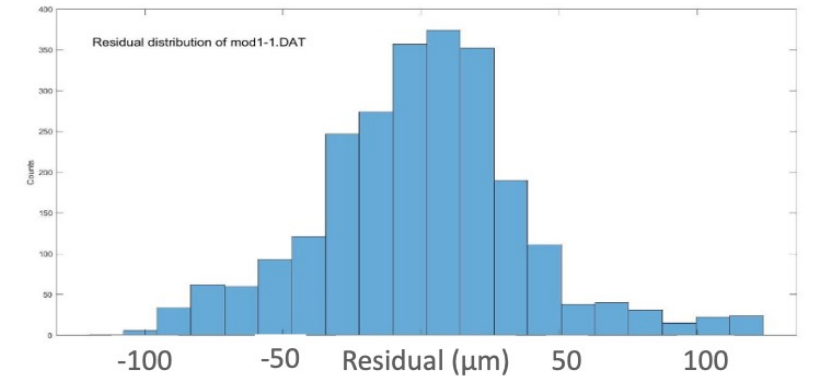
Guard Ring

# Test Results: Surface Shape

- Use a smartscope laser-scan of the surface to measure the form
- Matlab fits the surface to a given model (cylinder shown)



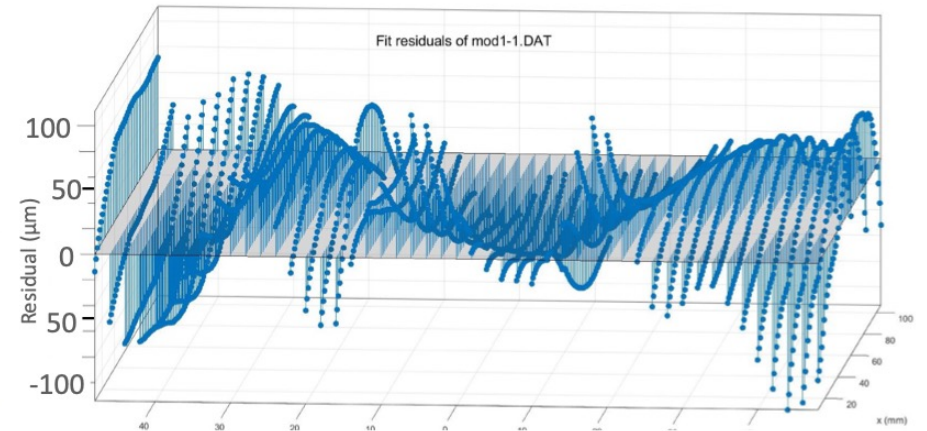
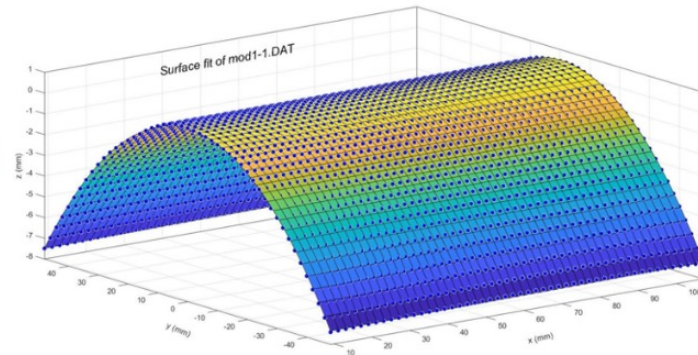
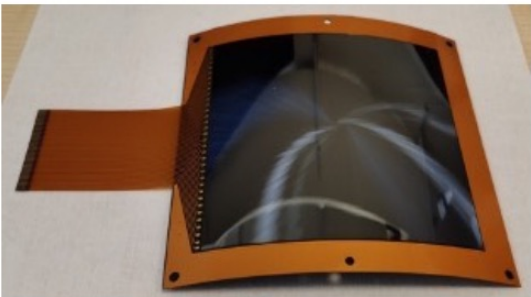
- Residuals vary across the module but remain acceptable
- Room for improvement with tooling and assembly procedure



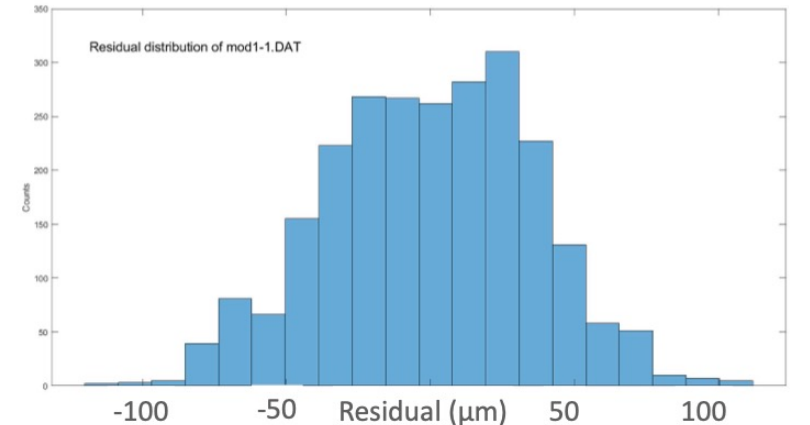


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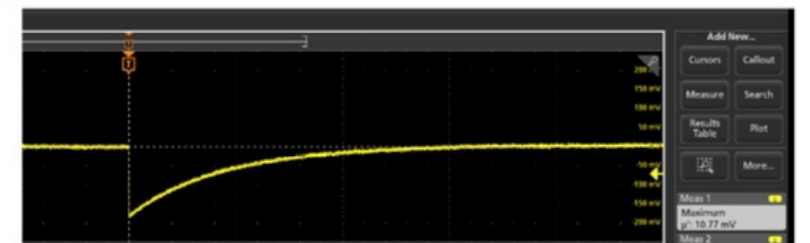
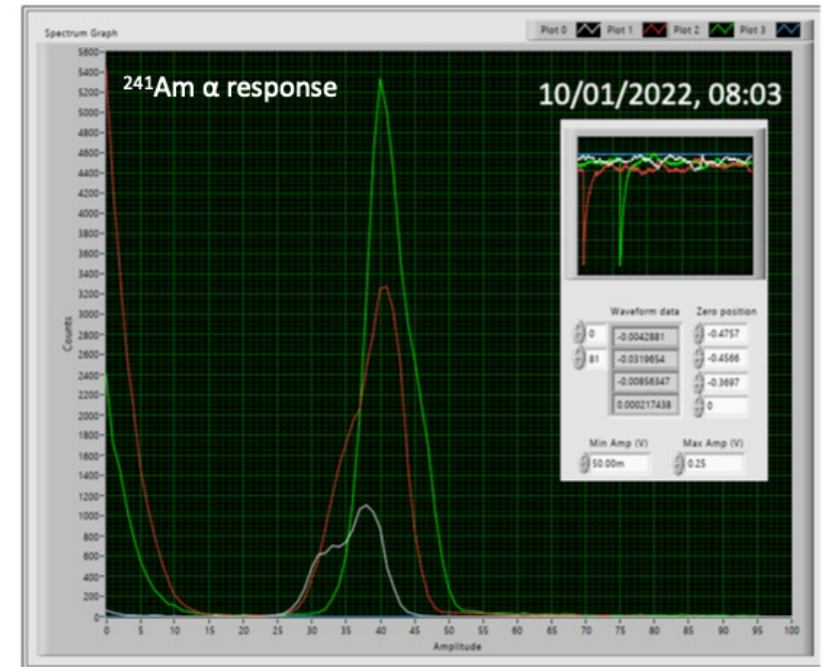
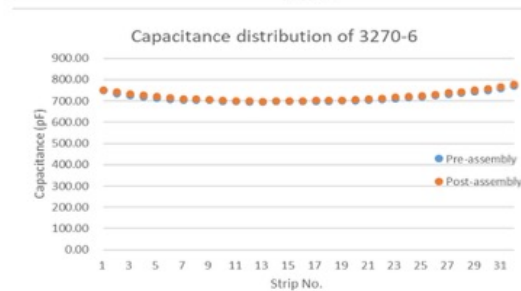
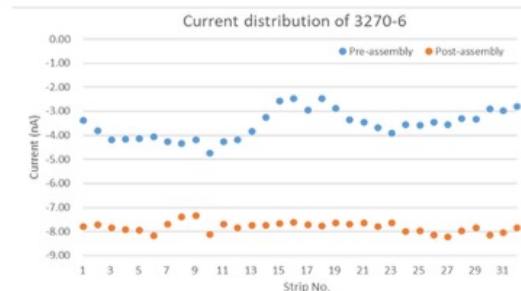
- Residuals vary across the module but remain acceptable
  - Slight improvement if we allow for a twist term (\*)
- Room for improvement with tooling and assembly procedure



(\*) See backup

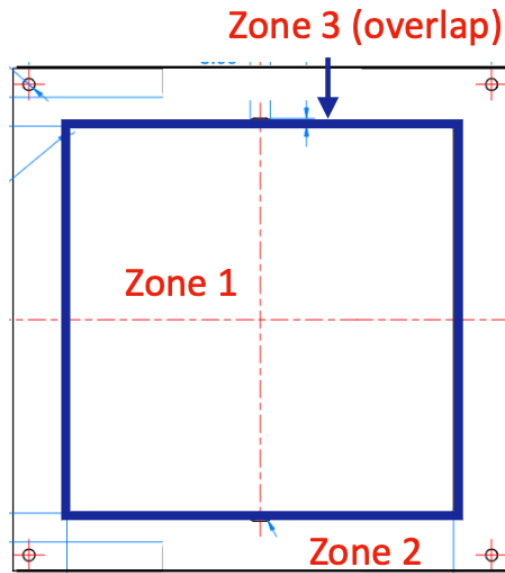
# Test Results: Electrical Performance

- Post assembly there is an increase in leakage current of 4-5 nA in sensors, but no notable change in the capacitance
- Use a Cremat amp coupled with either a CRIO NI DAQ or a Tektronix MSO scope for testing
- Clear signals observed
- 3 neighbouring strips shown:
  - Closest to source (Green)
  - Adjacent (Red/White)



# Test Results: $X/X_0$

- Break the module down into 3 zones to calculate  $X/X_0$



- Current design provides

Zone	$X/X_0$ (%)
1	0.054
2	0.619
3	0.703
Average	0.281

- Dominated by CFRP and Cu contributions
- Clear improvements possible to drive down to 0.17% by modifying bus tape and support
- Could be advantageous for passively cooled trackers

# Future Directions

- Current Project
  - Compare to flat module (ongoing)
  - Tooling for precision construction
- Future work with TTT10
  - More systematic measurements and comparisons
  - Irradiation
  - Thermal simulation: how far can we get with passive cooling?
  - Get a really good handle on impact of thinning and curvature with a well-characterized module!
- Move from strip sensors to CMOS

# Conclusions

- Constructed curved modules up to 10cm x 10cm
- Leakage current increase observed for curved module, but acceptable level for particle detection
- Tested using  $^{241}\text{Am}$   $\alpha$  particles in the lab
- More to explore and improve, but we think this is a promising approach to consider for a future low mass tracker system
- Looking forward to building collaborations that take advantage of this technology and the practical experience we are building with it!

# Backup

- Fitting the module surface; in addition to using a cylinder based model, also explore the use of Legendre polynomials following the CMS alignment method [1]:

$c_{ij}$  are coefficients describing orientation and shape of the silicon

$L_{i,j}$  are Legendre polynomials

$w(u, v)$  is surface model

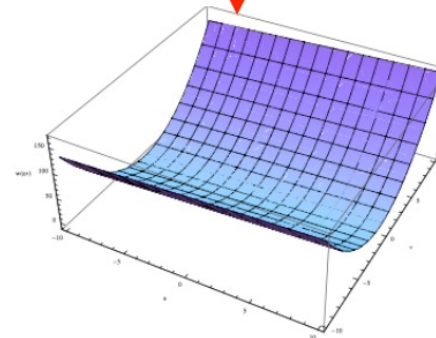
$(x, y)$  is in sensor plane coordinate system,  $(u, v)$  is 3-space coordinate system of the instrument

$N$  is order of expansion

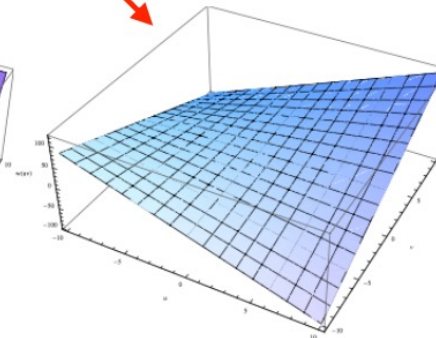
$$w(u, v) = \sum_{i=0}^N \sum_{j=0}^i c_{ij} L_j(u) L_{i-j}(v)$$

$$w(u, v) = \underbrace{c_{00} + c_{10}v + c_{11}u + c_{20} \frac{3v^2 - 1}{2}}_{\text{Planar orientation}} + c_{21}uv + c_{22} \frac{3u^2 - 1}{2}$$

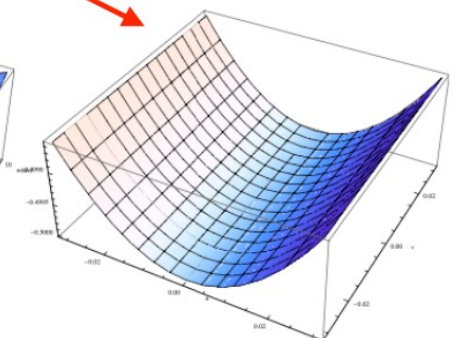
Planar orientation



Cylinder along axis v



twist



Cylinder along axis u

[1] F. Meier C. Kleinwort. Alignment of the CMS Silicon Tracker – and how to improve detectors in the future. Nucl.Instrum.Meth., A650:240–244, 2011.