Lessons Learned from the ITER Magnets: Materials Development and Materials Industrialisation

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- 4. Brief Status of the ITER Magnets

5. Conclusions

Manufacture of the ITER magnets started in 2008 with the superconducting strands, and over 10 years has progressed through the completion of the conductor supply to reach the stage of full scale industrial production of the final coils, with final first-of-kind items nearing delivery and the remainder soon following.

Looking at the material development before 2008 and the industrialisation post 2008 provides illustrative lessons on the extent to which novel materials could be rapidly brought into mainstream production cost effectively. The most critical materials have been: Insulation Systems Superconductors Structural Metals High Strength Composites

Also worth looking at: Superconducting joints, W&R&I technology (future paper...)

1. What are the ITER Magnets

ITER is a superconducting Tokamak

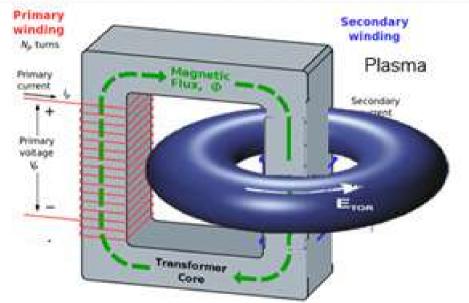
Inner poloidal field coils

(Primary transformer circuit) Poloidal magnetic field Outer poloidal field coils (for plasma positioning and shaping) JG05.537-10 **Resulting helical magnetic field Toroidal field coils** Plasma electric current **Toroidal magnetic field** (secondary transformer circuit) C 2010, ITEN OIGUINZALION

Designed to achieve 500MW fusion power

Plasma carrying a current up to 15MA confined by
Toroidal Field Coils
Central Solenoid Stack
Poloidal Field Coils

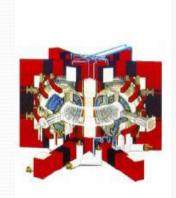
Creating the Plasma Current

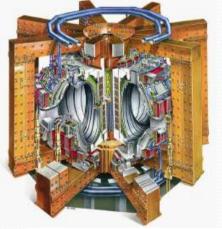


- Break down the plasma (applied electric field and/or ECRH) as a secondary 1 turn coil in a conventional transformer
- Primary winding is largely CS supported by PF
- As well as creating conditions to drive current, need a field configuration that allows plasma to form

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Some tokamaks use an iron core to improve coupling to plasma

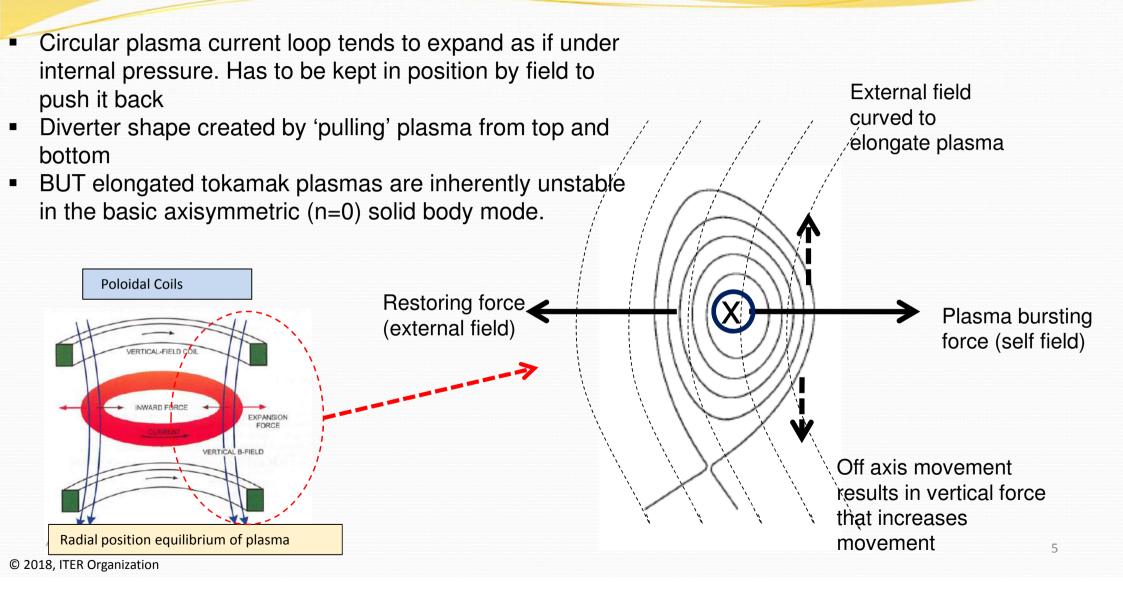




Tore Supra V_{plasma} 25 m³ P_{fusion} ~0 t_{plasma} ~400 s

JET V_{plasma} 80 m³ P_{fusion} ~16 MW 2s t_{plasma} ~30 s

Plasma Shaping



Role of Toroidal Field Coils and Resulting Loads

Because of poloidal fields, structures have to react a complex 3D force pattern....not at all like a pressure vessel

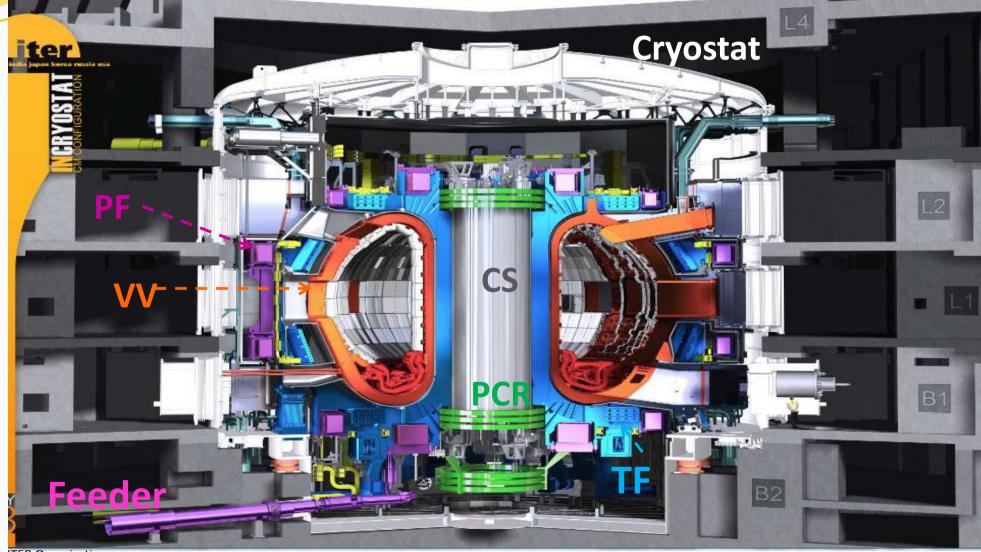
charged plasma Wedged particle CS TF 50000t Collision In-plane **Coil Contact Area** Also forces moving particles to orbit. These orbits have characteristic on Sides frequencies that can be coupled to radio frequency heating SOB Force magnitudes are huge...in SOF 50000t plane force on each TF coil is XPF 40000t NUL IM Upper and lower parts of CS Hoop Compression apply 50000t at the centre CS 40000t TF plane loads on TF Coils 6 © 2018 objEReforganization

Toroidal Field makes it more difficult for charged particles to

leave by providing a restoring force for outward movement

Magnetic field lines

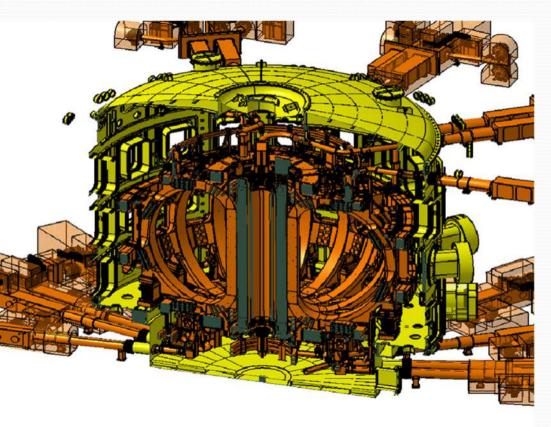
Overall Magnet System and Neighbours



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Superconducting Magnet In-Cryostat Environment

Magnets and Cryostat



Magnets, Cryostat and Thermal Shield

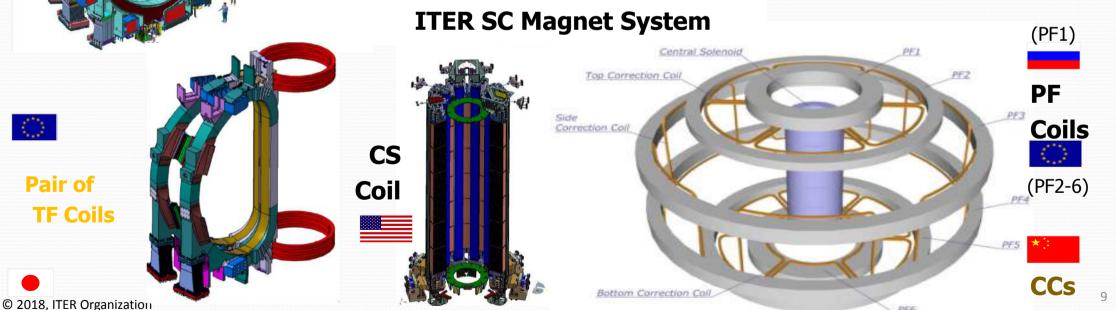
Magnets, Cryostat and VV

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ITER Magnet System – Superconducting Coils

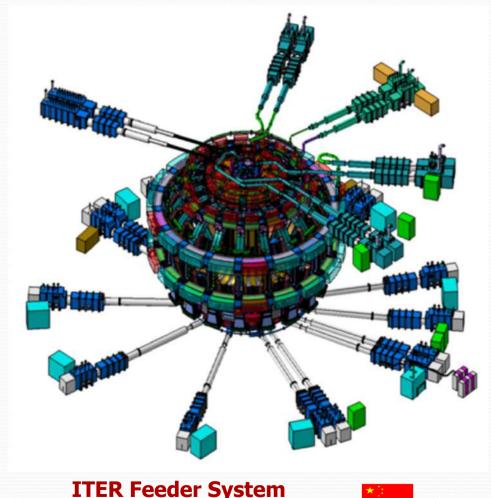


- 18 Nb₃Sn Toroidal Field (TF) Coils,
- a 6-module Nb₃Sn Central Solenoid (CS),
- 6 Nb-Ti Poloidal Field (PF) Coils,
- 9 Nb-Ti pairs of Correction Coils (CCs).



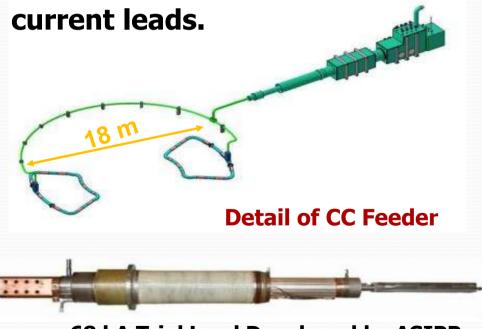
ITER Magnet System – Superconducting Feeders

• ITER magnets are supplied with current/cryogenic fluids by **31 Feeders.**



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- Nb-Ti CICC busbars (MB & CB),
- Ag-Au(5.4%) BiSCCO 2223 HTS



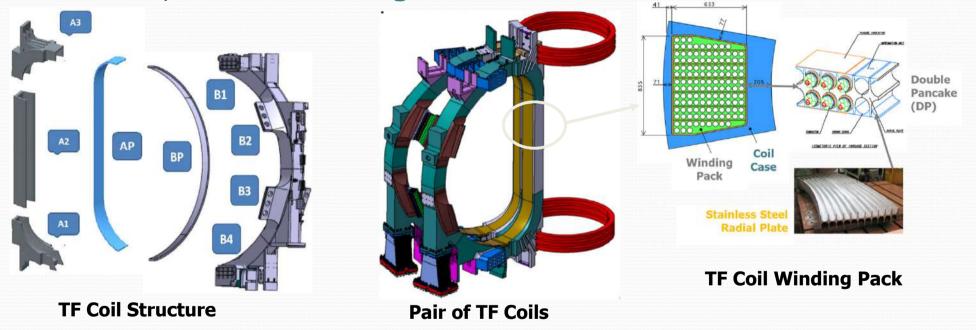
68 kA Trial Lead Developed by ASIPP

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[•] The magnet Feeders include

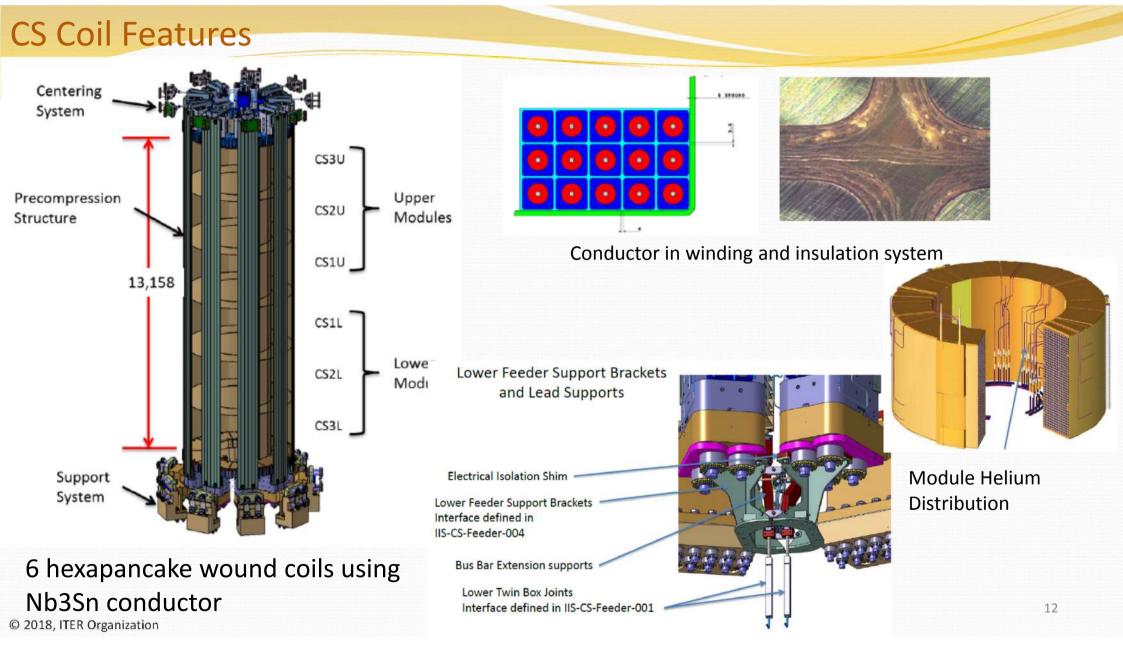
Main Features of ITER TF Coils

• The TF coil is made up of a winding pack **(WP)** inserted inside a thick **coil case** made of welded, stainless steel **segments**.



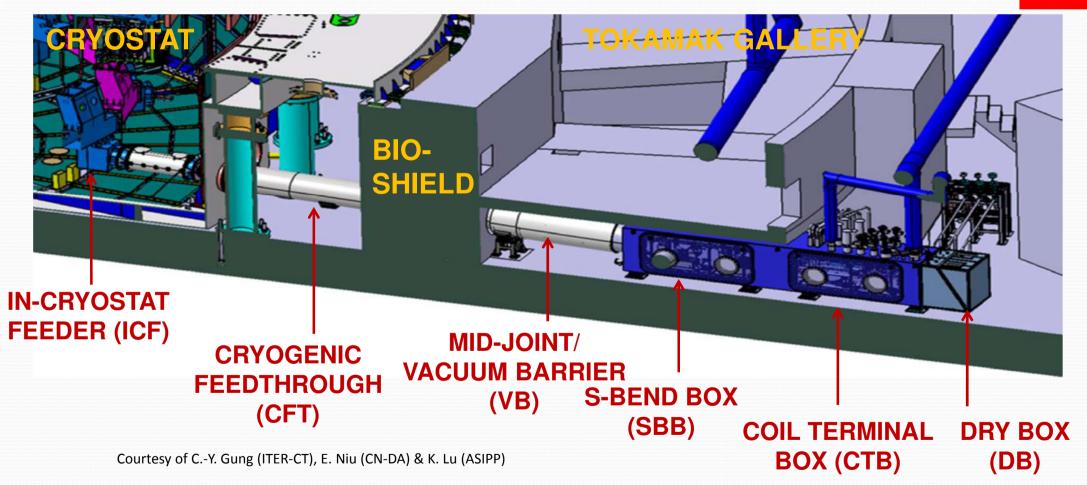
• Each winding pack (WP) comprises 7 double pancakes (DPs), made up of a

radial plate with precisely machined grooves into which the CICC is transferred upon heat treatment completion. © 2018, ITER Organization



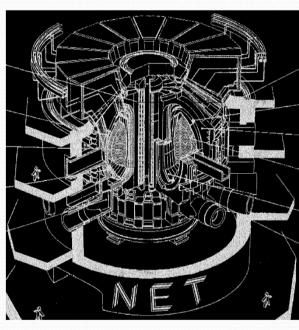
ITER Magnet Feeder Layout

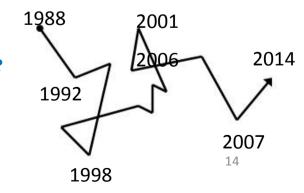
The magnet feeders are deeply integrated into to the tokamak.



2. ITER Magnet History and Innovations

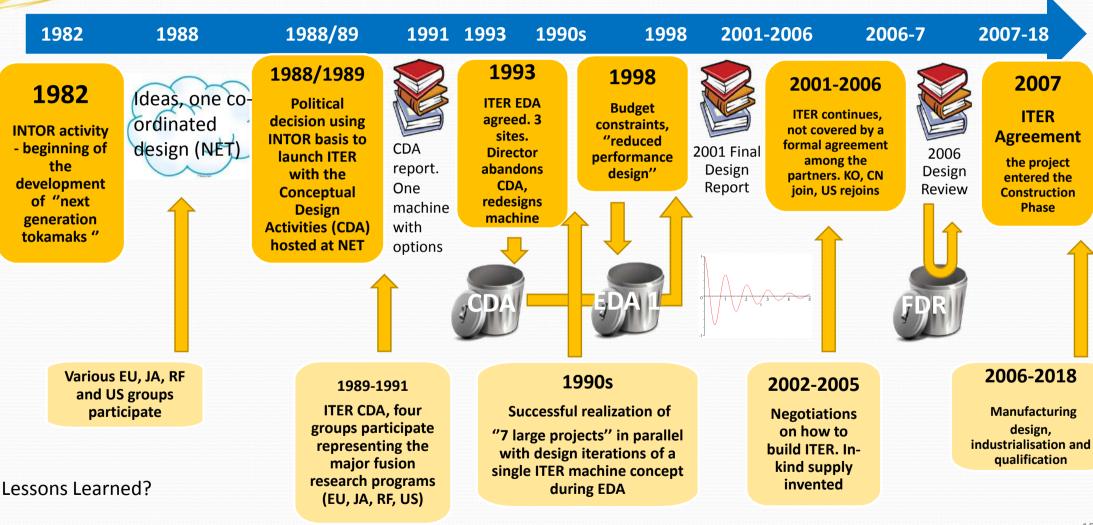
- The design roots go back to 1988, the start of the CDA and the NET machine. Present design mostly from 2001 which itself was based on the CDA final design report (1992) which had commonality with the NET project 1988 report (Fusion Technology July 1988--right)
- Changes, sometimes significant, to surroundings and requirements have created something of a random walk over the last 30 years. We have a design that meets our needs but cannot be said to be optimised. We are where we are.....
- □ The magnet parameters (field & volume) act as the primary drivers for the overall machine size. One of the lessons learned from the history of ITER is that giant oscillations can be created between adventurous (but perhaps unrealistic) innovations that produce large promised cost reductions and more sober (but on-paper more expensive) design realism. <u>Key is to get the right balance</u>





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ITER Project Timeline



Magnet Design: Challenges

Having worked out what the magnets had to do, and argued about the basic components/concepts, we then had to design them

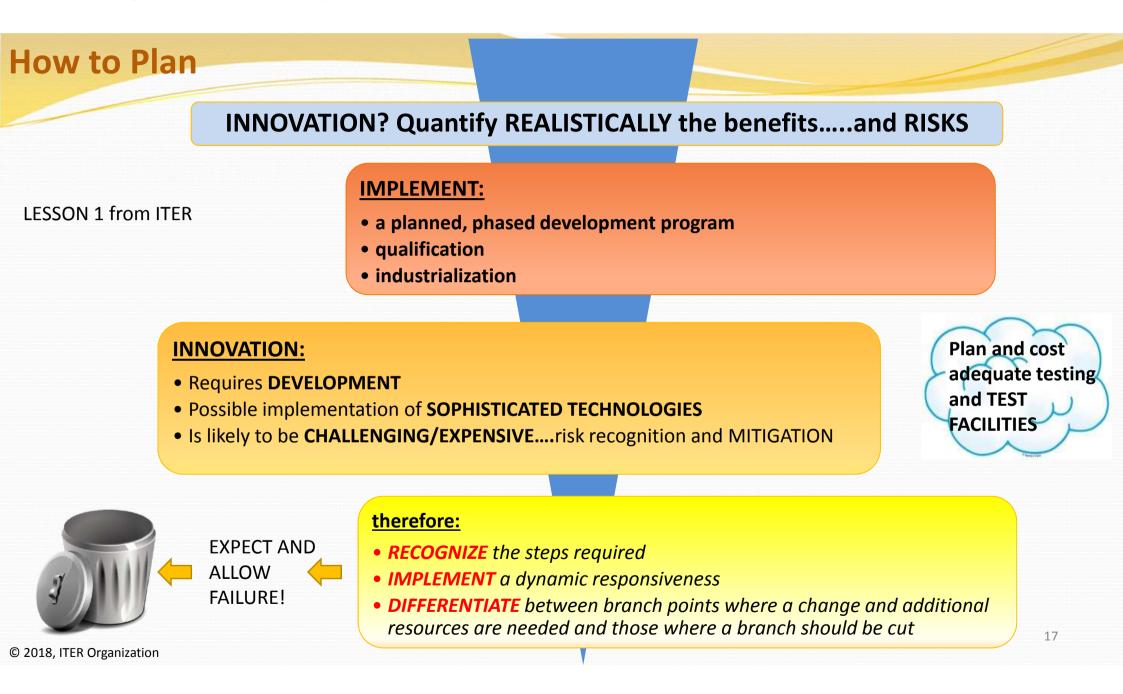
The top engineering innovation issues were (in 1991)

- high fields (12-13T) and current densities for industrial scale superconductors
- tight manufacturing tolerances
- very high voltages for a cryogenic environment
- severe multidirectional loading requirements
- high frequency AC operation
- spectacularly complicated interfaces

Issues with magnets in fusion are the familiar engineering ones that arise when components move out of the research field:

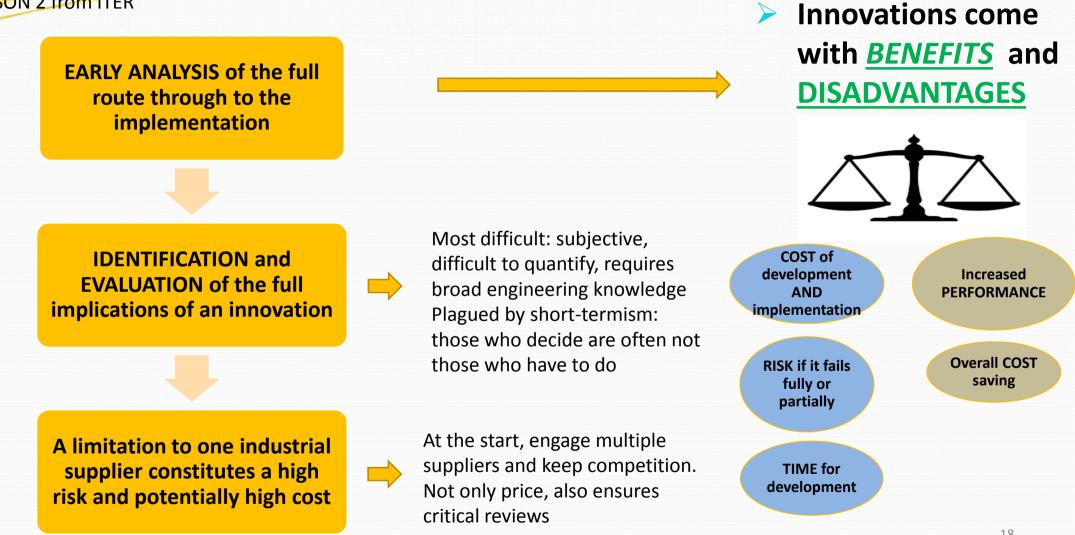
structural and electrical fatigue considerations imposed by the lifetime usage
 focus on reliability and repairability.





The successful implementation of an innovation

LESSON 2 from ITER



3. Industrial Development: Planning & Learning Lessons

Four Key Innovations in ITER Magnets

Insulation Systems (from 1988) Superconductors (from 1987) Structural Metals (from 1991) High Strength Composites (from 1999)

The challenges of these systems had a common theme:

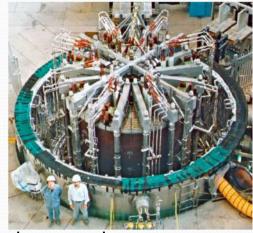
- Significant impact on overall machine size and cost if not implemented
- Early decision to choose what performance requirements to use for the baseline design, difficult to change later because of wide ranging impact on overall design
- □ Need to select the R&D targets at levels that are reasonable, promise a cost effective manufacturing route and maintain the positive advantages for the machine.

For each example we can look back and see how the Innovations were Implemented, using more-or-less successful process of learning lessons (....eventually)

With hindsight, it is possible to develop and trace a logic that was not there at the time

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Key (but not unique) facilities CS and TF model coils





Strategy of Conductor Development

Decide strand concept.......1987 Develop conductor test facilities 1988-1991 (FENIX then SULTAN) Decide strand parameters....1991, more or less fixed for 20 years Nb3Al persisted as R&D activity until 2002, obvious unsuitability after 1996

Consider composite conductor options

Choose conductor concept....more or less fixed for 20 years Argue about conductor concept for first 10 years

Consider conductor details

Strand stability and copper...fixed 2003 Conductor jacket material....fixed 2003 Cable configuration...fixed 2003, iterate 2006, iterated 2010

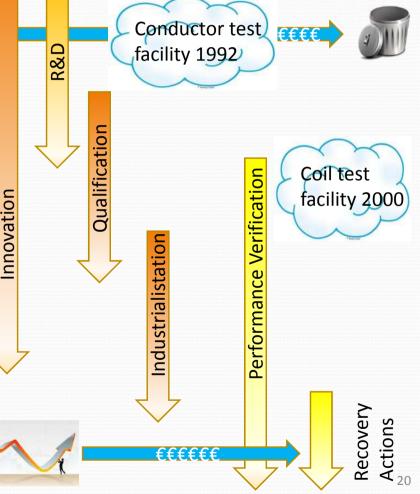
Industrialisation (from 2007)

Engage multiple strand suppliers (limited by ITER politics) Couple strand and cabling (reduce interface), extensive IO support on cabling Special jacketing lines (ITER politics dictated more than needed)

Continuous Performance Checks

CS conductor problems 2009 => solved 2013 (Crash Program 2) TF conductor problems 2006, adjusted 2008 (Crash Program 1), further issues 2017, solved 2018 (Crash Program 3) © 2018, ITER Organization Classic example of successful innovation.

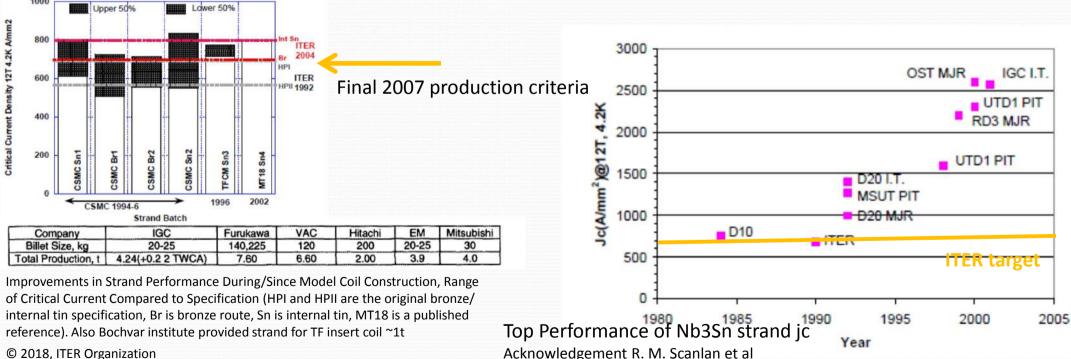
- Overall programme ~600M€
- Sequential activities, stable targets
- Focused recovery actions



Step I: Base Material Development

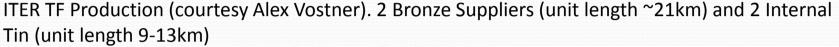
In 1987 even basic Nb3Sn strand fabrication was difficult. Few suppliers, low yield, 'individual' strands not standard material. Launched multiple contracts of ~50kg with common target, 4 production routes (jelly roll, bronze, IT, PIT)

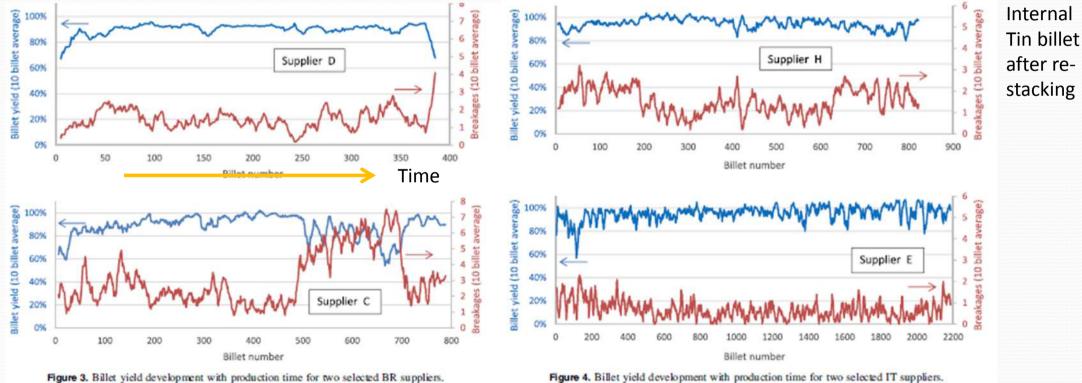
- ITER target kept well below "technology frontier". ITER model coils gave first steps in industrialisation
- T companies produced a few tonnes each by 1998, one (TWCA, jelly roll) dropped out



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Focused on industrial qualities: unit length, wastage, NDT processes and inherent process cost
 Contracts >1988 had incentives to improve usability: Larger billets, lower breakage
 Unit length increased from a few 100m in 1988 to ~1km in 1993 to >5km in 2008
 ITER TF Production (courtesy Alex Vostner). 2 Bronze Suppliers (unit length ~21km) and 2 International context of the second se





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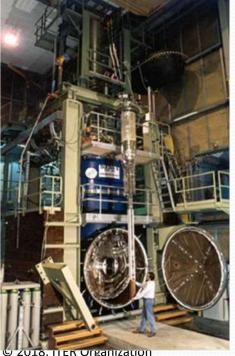
Figure 4. Billet yield development with production time for two selected IT suppliers. Yield is based on piece length wastage (breakage) not billet usability

Step II: Composite Conductor Selection

Differences in use of basic material (strand). Substantial difference in coil manufacturing (react and wind) vs wind and react)

•Key element to choice of conductor was current capacity (reduces voltage and/or copper for protection)

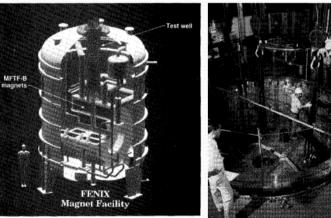
Test facilities for conductor samples were critical: SULTAN was constructed in 1980s and became available as split coil test facility in 1992. Still running 2018



Key for testing: SULTAN facility for conductor testina with open end cap showing conductor sample hanging vertically in front, 1990s

FENIX conductor test facility constructed at LLNL 1988-1990

- Used MFTF-B choke coils (Nb3Sn)
- First large test facility
- Very noisy high current power supply limited useful results



ITER TF Conductor Concept selected (by decree) 1993 Significant iterations on the details (Nb3Sn strand quantity, void fraction, twist pitch). For example Nb3Sn strand weight for the TF with temperature margin, standardised to a strain of -0.5%

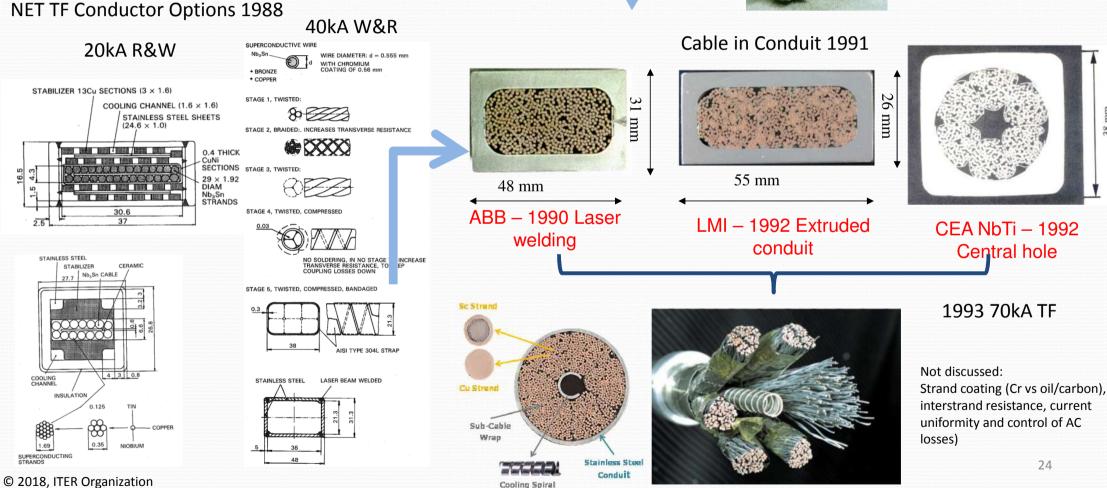
1998	822t	1K	
2001	351t	1K	
2004	369t	2.25K	

In 2003-4 recovery for degradation implemented Key to 2003-4 changesCu:nonCu ratio

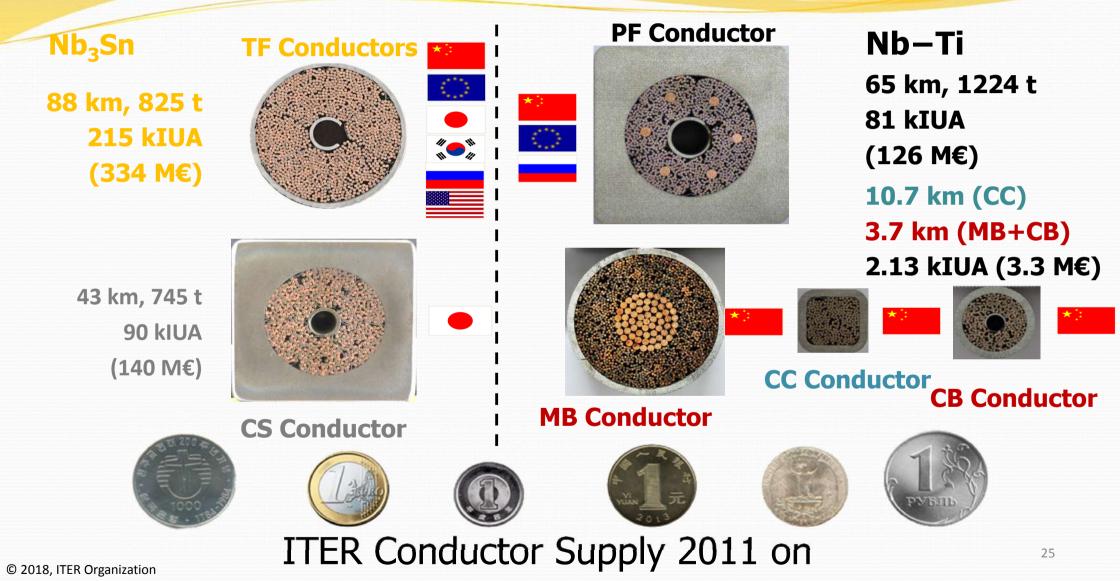
Ancestry of ITER Composite Conductors



DPC Nb3Sn cable in conduit 1985







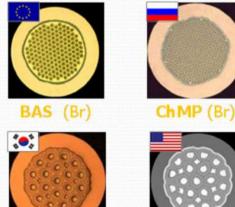
Step III: Industrial Base for strand

Even by 2007, minimal industrial base when we started (ITER) scale up was about 1 order of magnitude over 4 years in world production)

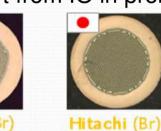
Raw material supply (Nb alloys, barriers) an early concern, eventually no issue

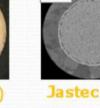
ITER procurement specification set to encourage multiple suppliers; staged ramp up, repeated gates to demonstrate performance. Support from IO in problem resolution in 2-3 cases

OST (IT



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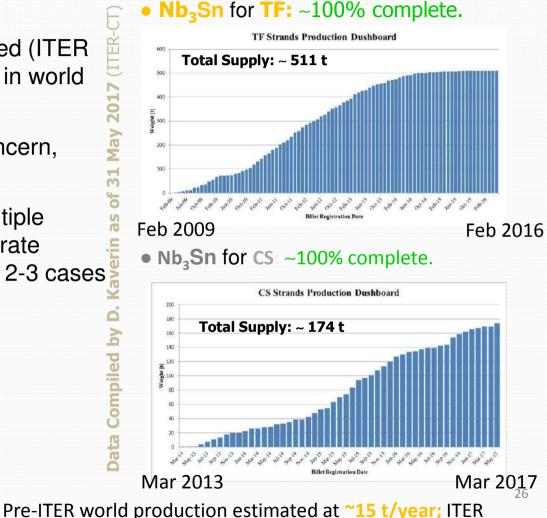






Jastec (Br)



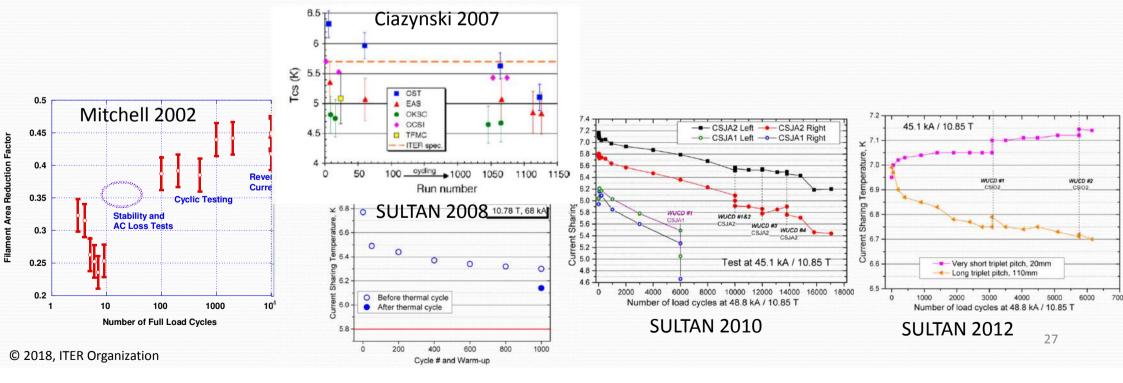


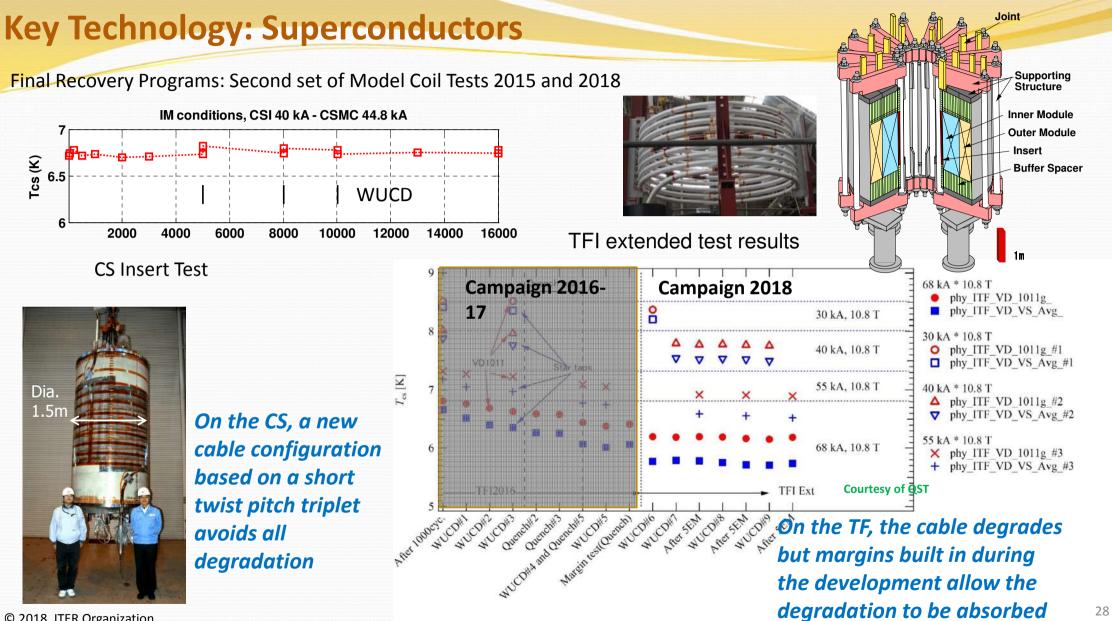
achieved ~100 t/year for ~5yrs.

Step IV: Recovery Programmes

By necessity (budget, schedule) industrial qualification went in parallel with full integrated performance testing. Result was unexpected issue with filament fracture that had to be addressed three times

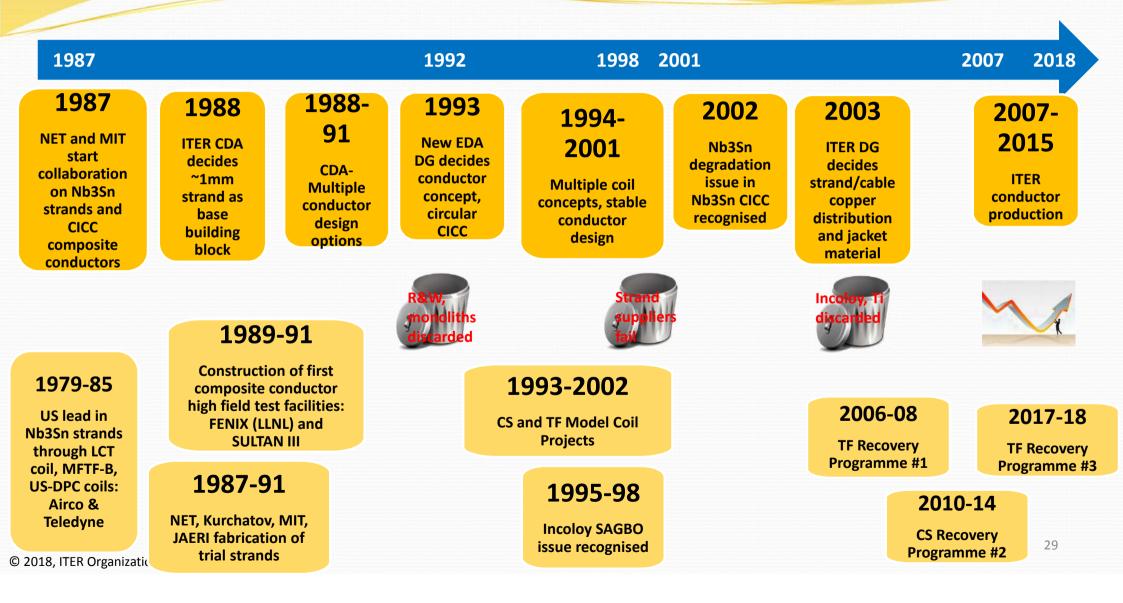
- I. Degradation discovered 2002-3. Details of cable design adjust 2003, then 2006-7, issue thought to be solved
- II. Testing of CS conductor 2010 showed issue not solved, cable redesign for CS, too late for TF
- III. Thermal-mechanical coupled degradation found in TF, testing showed stabilisation within margins





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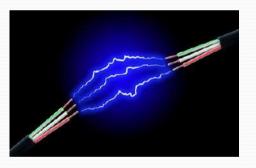
Development of Nb3Sn Superconductors for ITER



Copper coiled tokamaks built to high voltage requirements on PF system since 1970s Solid (VPI) glass-epoxy with kapton insulation as standard For example JET ground voltage is 20kV, test voltages about 40kV

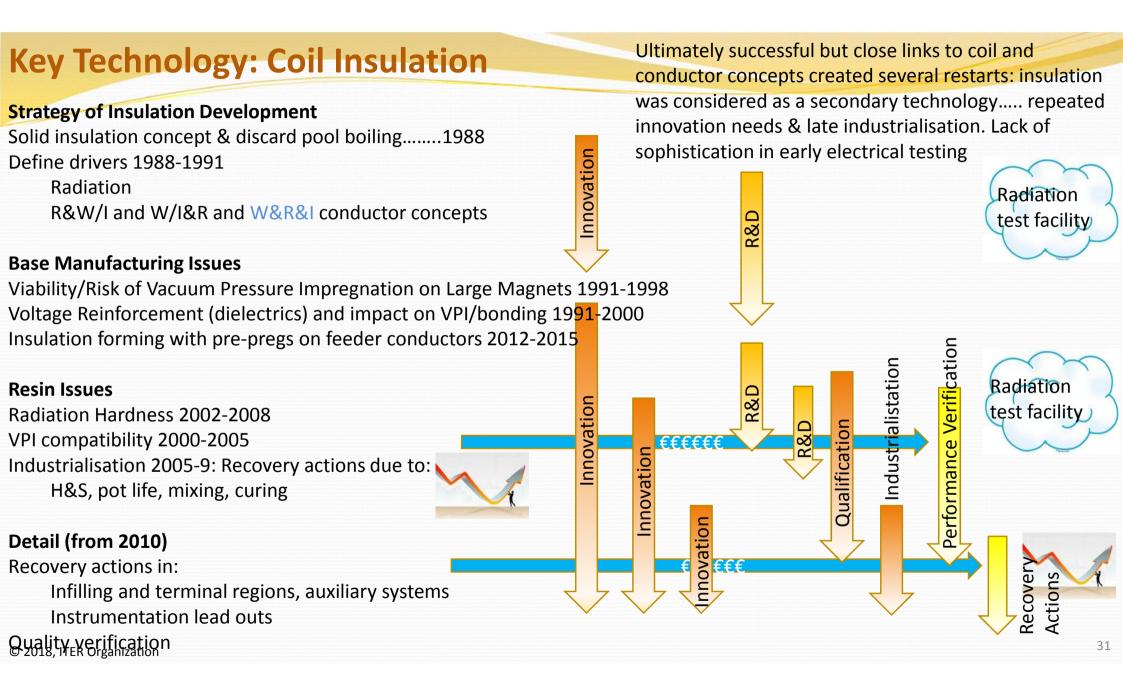
Early s/c tokamaks low energy & did not need to address high voltage issue, generally copper coils for pulsed CS/PF and steady s/c for TF (Tore Supra, T-7, T-15).

Now s/c voltage gradually increase >ITER CS model coil factory tested at 30kV >KSTAR tested at 15kV after installation >EAST tested at 6kV after installation



Now glass-kapton-epoxy is standard, ITER developed and uses glass-kapton-cyanate ester blend to give improved bonding and radiation resistance

INSULATION TECHNOLOGY AS CRITICAL AS SUPERCONDUCTING



Impact on Insulation of R&W/I and W/I&R and W&R&I conductor concepts

- Early insulation systems <1994 did not integrate dielectric barrier within winding (only as ground reinforcement)
- Relied on stand-off produced by glass filled with epoxy....as long as no cracks
- Glass wrap was compatible with W/I&R coil winding process where the glass went through the Nb3Sn heat treatment
- Despite this from 1988 on TF coil voltages of 20kV to ground and 10kV on terminals were regularly chosen

Present experience that these insulation systems would not have worked. Fortunately we did not build them

From 1993 multilayer insulation (familiar in copper coils) was standard CONDUCTOR INSULATION SHEME



POLYIMIDE

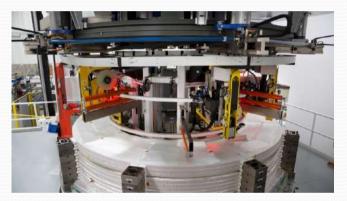
FIBERGLASS Issues to be addressed are well known and include outgasing of glass to avoid bubbles, resin penetration and cracking. Much more significant in cryogenic coils with thermal cycles and vacuum © 2018, ITER Organization



Demonstrated on TF MC 1998

R=react W=wind I= insulate

Final selection of W&R&I from 1995





Implemented in ITER 2012=> Top: CS, Below: TF Requires controlled handling of (delicate) Nb3Sn reacted conductor

Test Facilities for Irradiation

Garching

Required shielding for coil insulation is a key parameter driving the machine build. Establishing limits is difficult

- Irradiation in test reactor is not same spectrum as tokamak
- Big variations in resistance with minor changes in composition
- Impact of degradation difficult to quantify

First facility at Garching (up to mid 1990s)

- Small samples
- Succeeded to carry out irradiation and testing <80K by installing a special facility above the reactor
- Ended when reactor shut down

Second facility at Atom Institute Wien ATI (2001 to 2010) Triga

- Larger samples
- Room temperature only

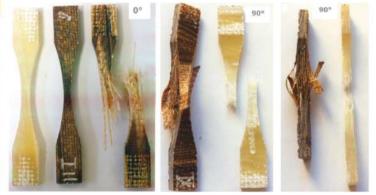


ATI

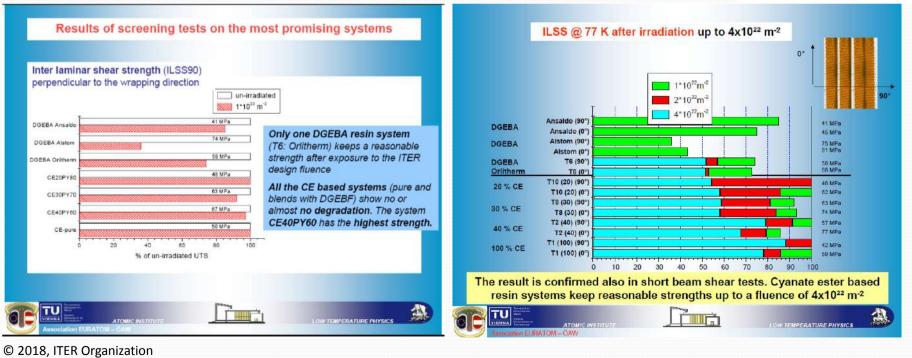
Insulation Irradiation Results

- Up to 2003 all coils impregnated with epoxy resin typically DGEBA
- At ITER fluence level (10MGy or 1*10²² neutrons/m²) marginal
- Cynate ester proposed in 2002 (CDT/TU Wien) as possible improvement
- Due to cost Cynate Ester Epoxy blend investigated, 40% CE identified as acceptabl up to 4*10²² neutrons/m²

Tensile Tests of Unirradiated and Irradiated ALSTOM ITER Samples



Fracture at 77 K before and after irradiation to fast neutron fluence of 1x 10²² m⁻² (E>0.1 MeV)



Resin Systems

- □ Initially (too) focused on radiation resistance
- Used industrial standard resins and until 2005=> did not look properly at electrical issues
- Only from 2009 addressed issues of
- Pot life (time to impregnate large winding at low viscosity before glassification)
- Exothermic curing
- Health issues (and regulation of perceived health risks) on composite chemicals (especially catalysts)
- Mixing and outgassing

EXAMPLE: Industrialisation of Cyanate Ester blend produced

several recovery actions

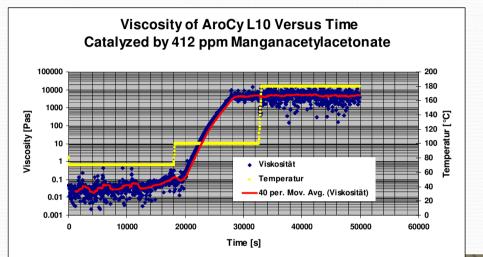
Cyanate Esters Polymerization Catalysts

- Pot life / speed of reaction strongly depends on catalyst type / concentration
- Catalysts must be added as homogeneous (filtered) solution to avoid any local high catalyst concentrations that could lead to uncontrollable reactions
- Polymerization is a highly exothermic reaction. Safety precautions!
 - □ Metal catalysts (typical concentrations 20-300 ppm)
 - 🖵 Co, Zn, Mn, Cu ...
 - Soluble organic salts/complexes are used e.g. acetylacetonates, octoates, naphtenates
 - Solutions in liquid alkyl phenols

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Lab-scale thermal runaway of cyanate ester

Pot-life extended in 2009 to more than 100h by exchanging the Mn-catalyst by a Co-catalyst.





Auxiliary Insulation Systems

•Insulation specimens manufactured with pre-preg from different suppliers. Processing conditions optimised. Many iterations to achieve quality

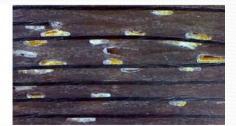
- •Pre-preg surface conditions important for bonding and voids
- •Pressure/vacuum bag important to reduce void fraction to 2-3%





Some material / process combinations result in insulation with significant voids, leading to poor electrical performance (left)





The final selected materials produce largely void-free specimens (right)

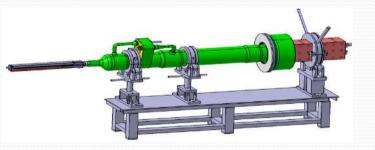


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Key Technology: Coil Insulation

Art of applying polyimide

- Inflexible and therefore curved surfaces have to be smoothed
- Complicated patterns of lay-up



- The HTS current leads offer a challenging geometry to wrap due to changes in section and presence of helium pipes at right angles.
- Strategy is to lay up the GK tapes on the cone section.
- Root area of the pipes is first smoothed with green putty before application of the GK tapes.



Feeder Wrapping

TF coil terminal region







Principles well known but in ITER (with vacuum) failure to overlap adequately (and cure without resin rich areas) leads to cracks and Paschen failures

Origami style cutting of sheets to fit curves

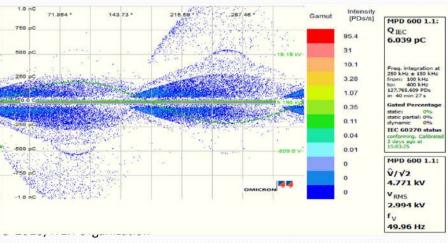


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Key Technology: Coil Insulation

Quality Testing

- □ Up to 2008, only HV DC testing
- From 2008, IO introduced Partial Discharge characterisation and Paschen breakdown testing. Now by far most critical tests, and used for development as well as qualification and production
- Void fraction measurements also improved
 - Insulation test of current lead
 - PD test results show stable but relatively high absolute values.
 - Ground screen termination was improved on next prototype.



Paschen Tests on TF Terminal Region (first production coil): yellow arc indicates the breakdown



Acknowledgement F4E/ASG and Sandro Bonito-Oliva and US-IPO/GA Wayne Reiersen and John Smith



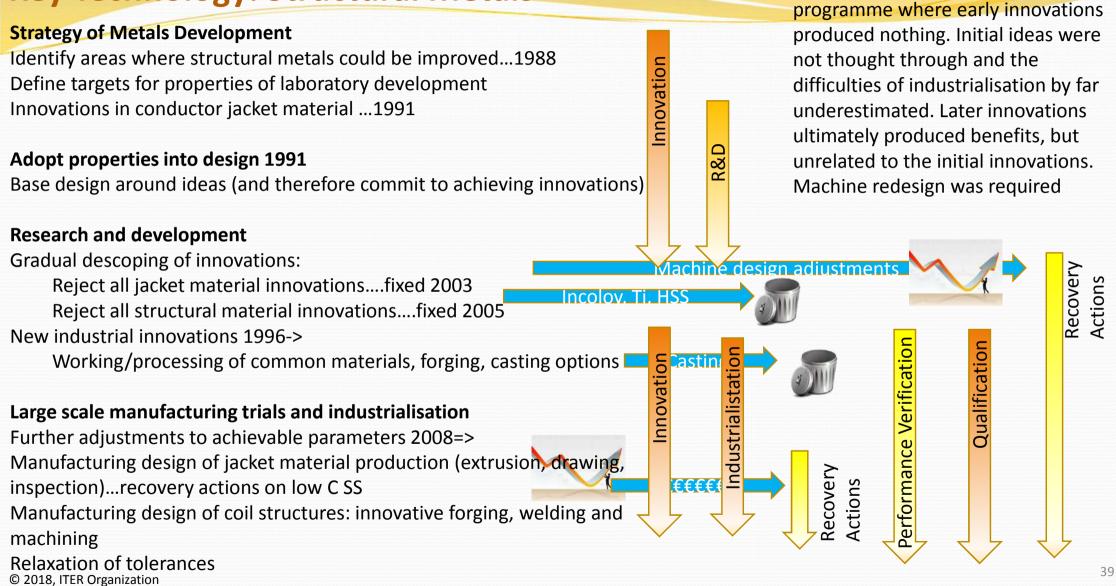






CS Lead Breakout (mock-up) before discharge (left) and during discharge (right), breakdown at <5kV, 10 mbar





Almost classic example of a

- Accuracy and adjustability of magnetic fields critical to plasma performance
- Coil set built for one function must minimise fields that affect other functions
- Impossible to build and fit everything in ITER magnets to <1mm tolerances. Difficult & expensive to achieve <5mm overall</p>
- Difficult to establish coil tolerances (or field accuracy) on many existing tokamaks
- Generally 'a few mm'....regardless of size
- ■Only recently (last 10 years) is field quality (→ tolerances) a design issue

Major effort with ITER coils to identify and minimise <u>critical</u> manufacturing manufacturing/assembly tolerances but NOT to demand unnecessary accuracy

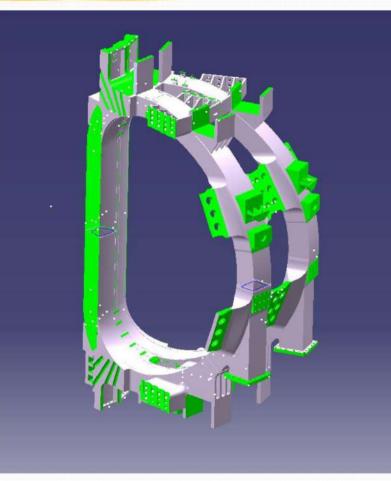
Example of Tolerances: Structures

Where dimensional errors have an impact

- Fitting of components during assembly so that load paths still match design intention
- Inability to place component in available space
- Field errors

What drives tolerances

- Manufacturing requirements/capability typically +/- 1-2mm locally +/-0.5mm
- Installation requirements/capability typically +/- 2mm
- Measurement errors and component deformations under gravity
- Cumulative build up during manufacturing & assembly.... tolerances depend on other components
- For some interfaces we can adapt to +/-10mm



Multiple TF coil interfaces (green)

TF coils & structures are the core which drive the rest

Base Materials for Structures

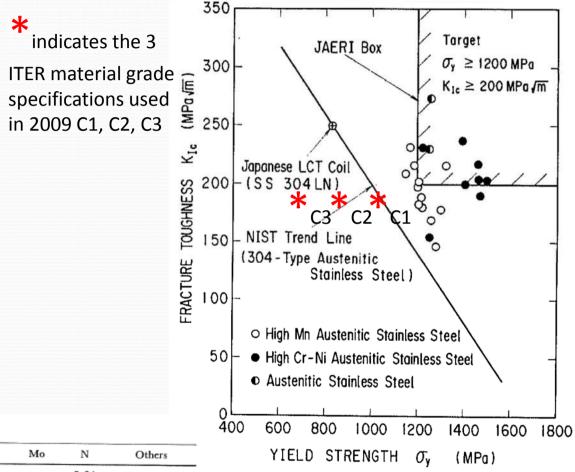
- Basic material research launched in 1988 as perception that higher structural metal properties could bring saving in overall machine cost
- Programme launched in JA, EU, RF
- Success claimed in laboratory scale research but universal failure on industrial scale.
- Problems of production of highly compositon specific alloys underestimated
- Issues such as welding, forging, corrosion neglected
- By 2008 only JJ1 remains (TF coil nose) at C1 level and steel properties at same level as obtainable industrially in 1980s

Table 1. Chemical compositions of the JCS.

indicates the 3

JCS	С	Si	Mn	Р	s	Ni	\mathbf{Cr}	Mo	N	Others
CSUS-JN1	0.026	0.99	4.2	0.026	0,002	14.74	24.2	_	0.34	
CSUS-JKAI	0.023	0.42	0.49	0.006	0.001	14.0	25.0	0,68	0.268	
CSUS-JN2	0.050	0.34	22.4	0,010	0.002	3,22	13.4	0,70	0.24	V: 0.30
CSUS-JK2	0,05	0.36	21.79	0.013	0.005	4.94	12.82		0.212	Cu: 0,70
CSUS-JJ1	0.046	0.44	9.74	0,020	0.002	11.92	12.21	4.89	0,203	

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The relation between fracture toughness and yield trength of the JCS at 4 K. 1988

Base Materials for Conductor Jackets I

"Exotics"

Considerations on requirements (in 1991)

- Perception that metal contraction coefficient from 600C to 4K should match that of Nb3Sn to avoid critical current degradation
- The thermal contraction significance in CICC optimisation vastly over-estimated (still seen in new cable development in 2018) *leading to incorrect cost impact* assessment
- Many other issues drive cable in jacket performance (In particular degradation)
- Environmental issues ignored: corrosion
- Production issues vastly under-estimated but became obvious in period 1998-2002

Candidates Incoloy 908 and Ti. SS was neglected

CS JK2LB conductor samples 2012-13 - corrosion leaks originating from halides present in solder flux accidently contaminating the metal surface

Corrosion 1

Typical SAGBO cracking in Incoloy 908, in CS Model Coil jacket sections (K. Hamada and JAERI)









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Corrosion 2

Base Materials for Conductor Jackets

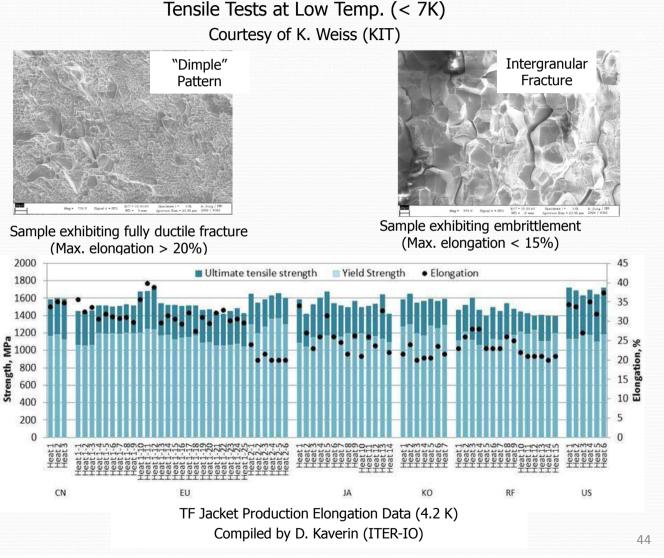
"Conventional"

Late development of SS jackets

- Nb3Sn heat treatment leads to carbon precipitation and embrittlement of SS enhanced by cold work of jacket
- For TF needed to develop low carbon steel.
 Worked with industrial partners to optimise production process and control cold working
- For CS JADA continued with JK2LB and eventually achieved success after several material composition adjustments
- JK2LB remains highly sensitive to halogen stress corrosion



4 TF jacket suppliers (1 in EU SMST, 1 in JA KSST, 1 in KO POSCOSS and 1 in CN JIULI) have been qualified and produced tubes for all 6 DAs.
Tubes extruded in ~12m lengths and butt welded



1996-2000 Various forged sub-sections of the ITER TF coil case, showing the complexity of the forged forms. Top: seamless TF case, bottom, seamless radial plate for TFMC



Forging Challenges: Size (for CS tie plate, longer than reheat furnace), shape complexity to reduce machining, narrow temperature window for forging high strength steel



2015-16 Offset forging of a 12m CS tie plate

Trials on TF Structures: curved hollow section of coil case. Ultimately too complex but the know-how obtained by the company (Kind) was used to produce almost all the forgings for the TF coil cases and VV under contracts with EU, KO and JA © 2018, ITER Organization

Trial Casting of Components: rejected because of poor properties (low modulus, low strength)





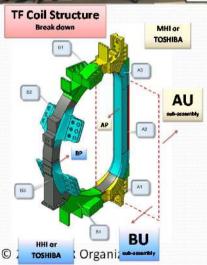








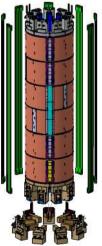




Various forged sub-sections of the ITER TF coil case in 2016-17, showing the complexity of the forged forms.

CS tie plate 2017

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Strategy of Use

Decide on Pre-compression ring concept......2000...too vague Decide performance parameters....overestimate

Consider options

Choose winding concept.....wet winding of monofilament glass...2002 No industrial input, attractive as subsize tests can be performed

R&D and qualification

Change winding concept...VPI of monofilament glass...2004-5 Construct 1/5 scale test facility 2005-6 Wind 1/5 scale samples in laboratory, successful test 2006-7

Industrialisation (from 2009)

No industrial suppliers prepared to offer full scale monofilament ring 2011 Change concept to AFP, new process, 2012 Process not down-scalable to 1/5 test facility, go to full scale AFP manufacturing issues 2015 Change main line concept to pultruded process, 2017 Construct full scale test facility 2017 Full size pultruded ring test end 2018 (?)

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implementation of innovation Industrialisation too late Cost saving on test facilities nnovation Everything ended up in parallel Ultimately seems successful R&D Subsize test **Verification** facility Qualification mance Recovery Actions Industrialistatio Sample testing Pert Full size test facility 47

Classic case of poor

Critical component introduced in ITER in 1999-2001 to preload TF coils and compress shear keys

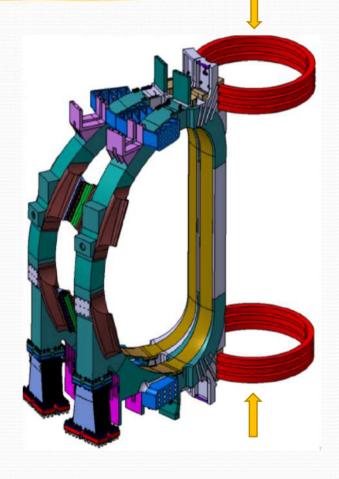
Relies on specific properties of strength, modulus and thermal contraction.

Practically only one solution: structure made with glass fibre

Classic example of a high risk innovation: limited opportunity for risk mitigation if it does not work, limited possibilities to find alternatives

Cost saving did not allow proper risk mitigation. Too small testing, very late industrial involvement. In the end cost more than a structured programme from the start

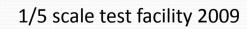
Classic example of a (too) late recovery plan based on R&D to produce a 'Plan B' that seems successful linked to implementation of full testing



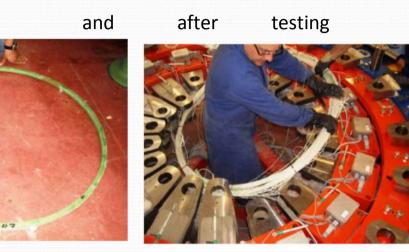
Wet Winding







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1/5 scale test facility

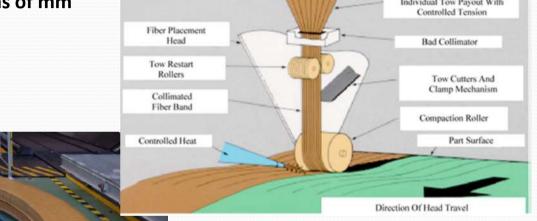
Ring before



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AFP Automated Filament Placement Method

Fibers' Wrinkles: waves on fibers with pitch of few mm
Fibers' Undulations: waves slightly taller and with pitch of tens of mm

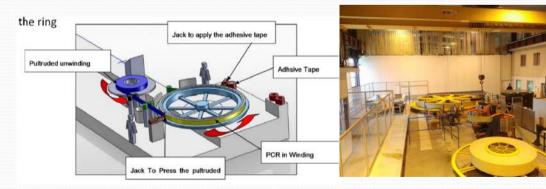


Pultruded Route

Full size 1/3 thickness prototype July 2018



Winding line completed



Full diameter prototype ring after curing, showing wrinkles

Acknowledgement F4E, A. Bonito-Oliva, T. Boutboule, CASA and CNIM

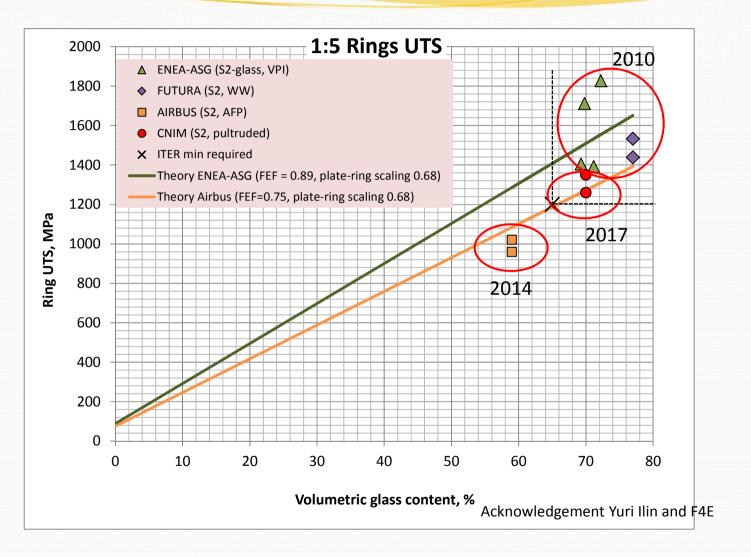
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Summary of recovery actions

Tests of 1/5 scale rings to failure

UTS= ultimate tensile strength



What Lessons were learned?

Innovation will happen at many levels in a project....great ideas everywhere ITER top level: Series of innovations in tokamak concepts provoked big oscillations in the technological development Medium level: 4 innovations were ultimately successful but followed paths of highly variable roughness

What Lessons do we expect to learn from all this? We are not going to repeat exactly the ITER experience

Generalise the specific examples to write rules/guidelines on how to start a basic research project in an international environment (which in the present world is omnipresent)...essentially try to carry out a root cause analysis

- 1. Always carry out a FMEA assessment based on the full, partial or complete failure of a great idea. A risk analysis is not the same....failure is black and white, risk is shades of grey. A FMEA should identify the necessary escape routes...
- 2. When assessing a proposed innovation, confirm that the innovation is really the key issue in the area it affects. Good example here is the structural materials....laboratory scale R&D created a series of red herrings that took years to straighten out. If it is not, what is? And can it be improved?
- 3. Successful engineering implementation is much more difficult than a small R&D programme. If an innovation is selected, plan, plan, plan! You need industrial suppliers and (while recognising the key part industrial collaboration can play) never ever create a monopoly supplier situation
- 4. Successful innovation is a long grind, with many forks. You cannot follow them all, but nor can you cut off the branches too early. Plan frequent reviews, adapt, ensure wide input, get in early with recovery plans, and ruthlessly discard when the end of the road seems to be reached.

3. Brief Status of the ITER Magnets

Manufacturing Status (July 2018)

Very approximate overview

Conductors: 99% complete

TF Coil Windings: 60% complete

TF Structures: 50% complete

PF Coils: 25% complete

Feeders: 25% complete

Supports: 60% complete

CS coils: 50% complete

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Worksite Progress: Feb. 2015 – July 2018

Feb 15







© 20 More sthan halfway to First Plasma:

April 18



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Assembly Hall





Before being integrated in the machine, the components will be prepared and pre-assembled in this 6,000 m2, 60-metre high building.

The Assembly Hall is equipped with a double overhead travelling crane with a total lifting capacity of 1,500 tons.

To the right, the installation of the first sub-assembly tool (SSAT-1) is nearing completion

JA TF coils – Manufacturing progress at MHI Kobe



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TF13 WP in VPI mould

Acknowledgement: N. Koizumi, QST team and MHI



assembly

EU TF coils – Progress at ASG La Spezia



 $_{\odot}$ WP instrumentation under test

Acknowledgement F4E and ASG

TF Coil Structure BU-AU fitting tests at MHI Japan & HHI Korea





Fitting achieved to better than 0.5mm at interfaces Left: TF09 fitting, HHI, January 2018 Right: TF12 fitting, MHI, Aug 2018

Acknowledgement QST, MHI & HHI

Case-WP Insertion Assembly Rig at SIMIC

- The 1st Assembly Rig has been tested and commissioned in 2017
- Results showed that the parts can be moved with a precision better that 0.2mm
- First set of structures has undergone a trial fitting in July 2018
- First winding pack insertion starts in September 2018



Acknowledgement F4E & SIMIC

Supports at various locations in China

- Lots of PF clamps in various stages of completion at HTXL China
- TF GS complete and components for 3-4 more near completion



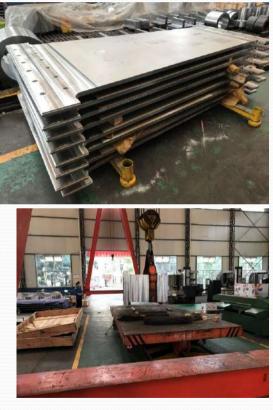


Water jet TF GS plates machining PF5 clamps

PF clamps rough forgings



Behind: PF clamps (left), TF GS plates (right), PF6 plates and blanket shielding blocks (front)



Balancing a PF5 clamp



First complete TF Gravity Support (July 2017)

Acknowledgement CNDA, SWIP & HTXL

PF5 Status (ITER Site)

- Five PF5 real Double Pancakes (DPs) windings have been completed. The third • series production DP6 has been started.
- First VPI on DP7 finished. VPI on DP8 and DP6 is on-going.



PF5: 2nd DP(DP8) Winding Completed



PF5: Dummy DP VPI Under Preparation

Acknowledgement F4E

PF6 Status in Hefei, China

- All DPs windings have been completed.
- Completed resin impregnation (VPI) for six DPs.
- Coil stacking underway



Acknowledgement F4E & ASIPP © 2018, ITER Organization



PF6 DP stacking, July 2018

CS Coil at GA San Diego

Modules 1, 2 & 3 are heat treated

- Left: CS module 1 on turn insulation station after heat treatment. Right: Module 1 entering mold (Aug 18). Resin impregnation in September 2018
- Winding of 4nd module is completed; winding of 5th module has started.

Acknowledgement US-IPO, GA)



Striking the right balance between potential advantage and risk in the pursuit of innovation is challenging, especially as innovations are often associated with substantial potential cost advantages – and, of course, large scale scientific projects such as ITER are invariably subject to cost pressures

Long development, first with R&D then with industry to produce the functionality and quality needed ITER provides 4 examples of extended and ultimately successful innovation & industrialisation, but with clear lessons on how a more effecrive innovation could have been achieved more quickly and cheaply

Machine and Magnet Construction passed the 50% mark