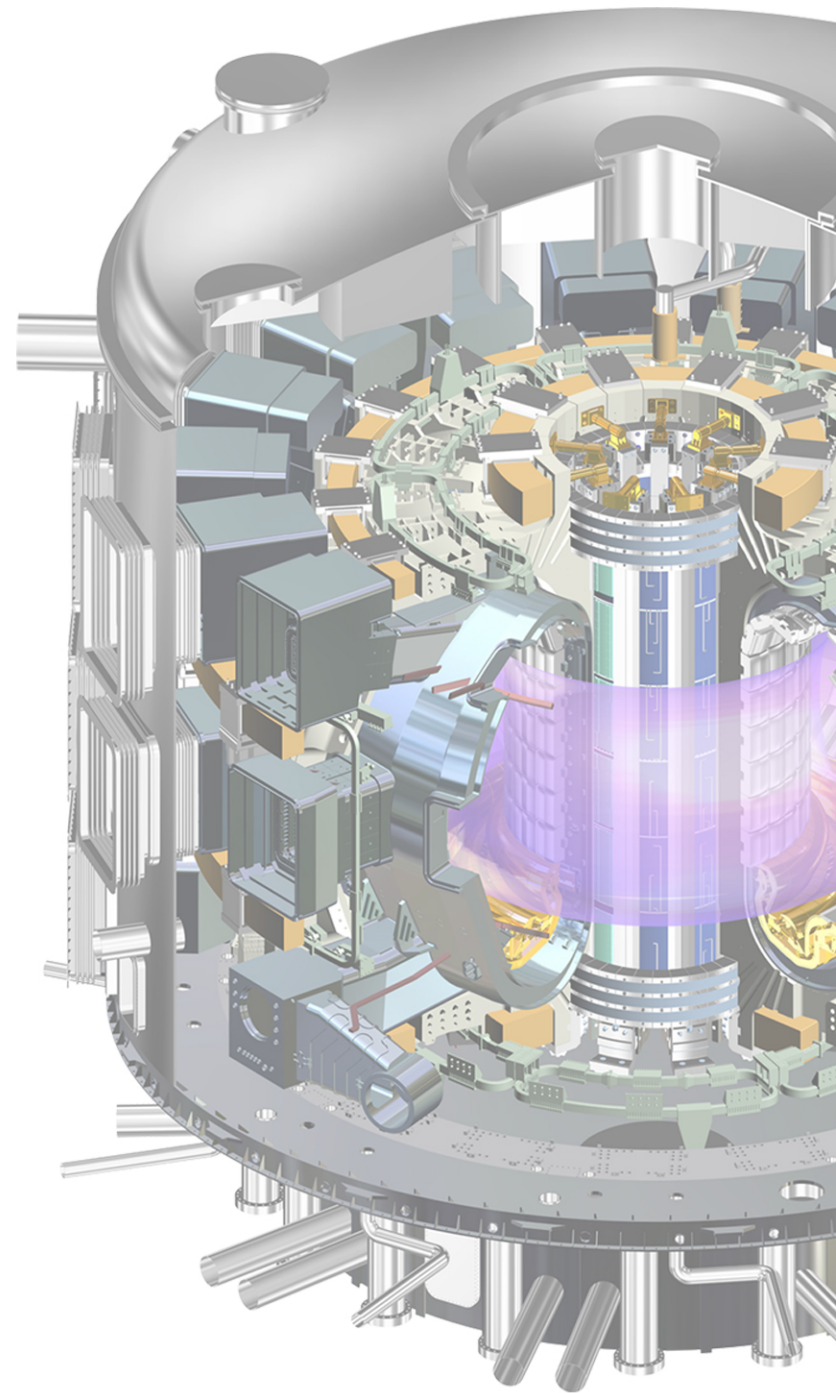


ITER CS Inlet Fatigue Test

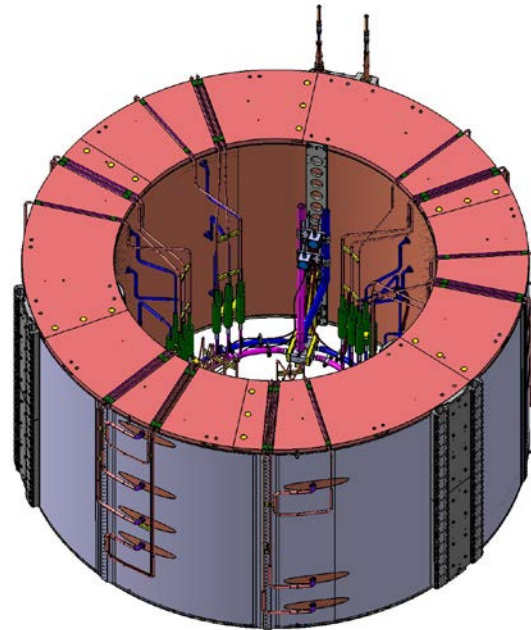
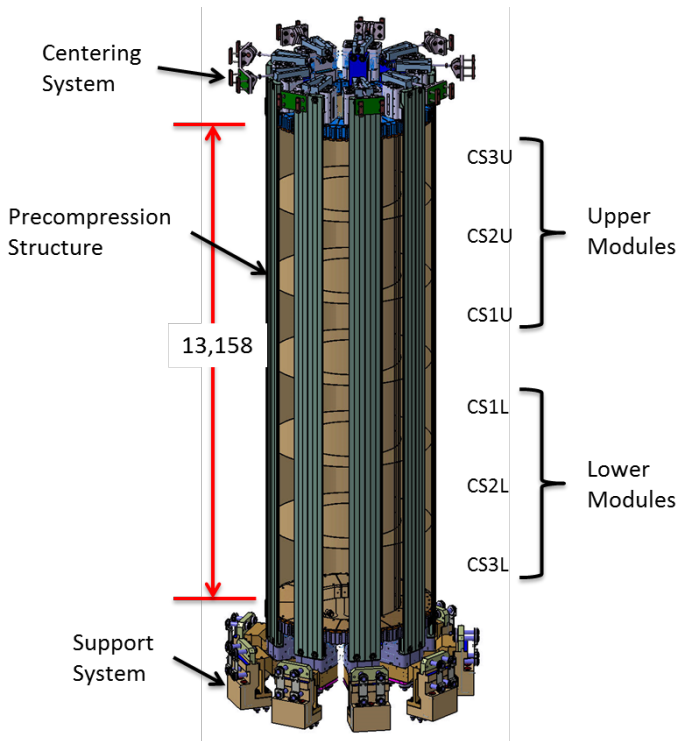
**Nicolai Martovetsky, Robert Walsh,
Kevin Freudenberg, Wayne Reiersen,
David Everitt, Dustin McRae, Leonard
Myatt, Kristine Cochran, and Cornelis
Jong**

ICMC

09/02/2018



ITER CS Stack



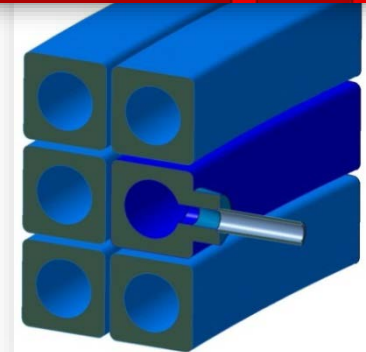
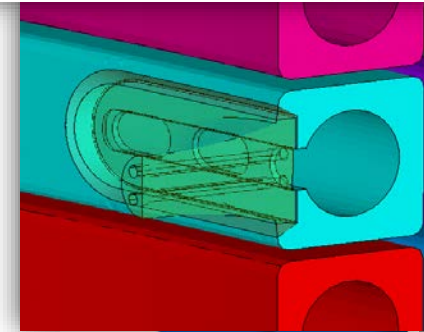
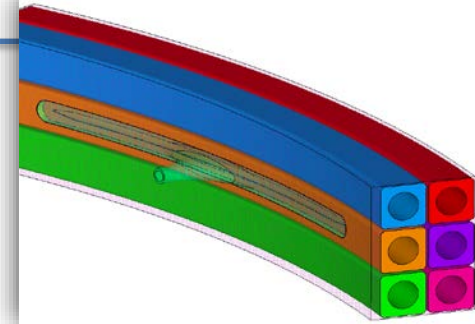
CS Module

Helium is injected at the ID



CS Helium Inlet

Introduction



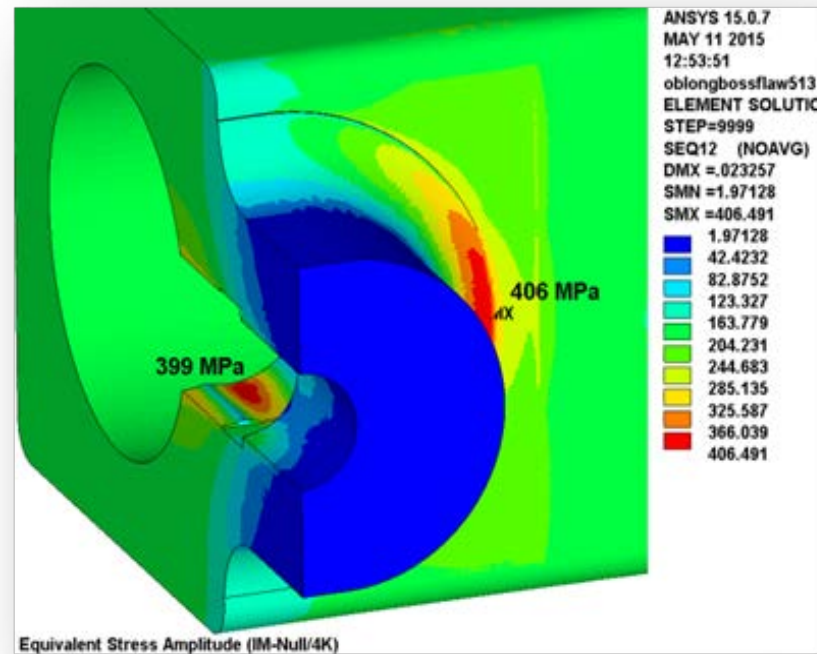
- Since CS CDR (2009), numerous variations of He inlet design have been explored
- Motivation (as listed here, but ultimately based on reliability & cost):
 - Minimize structural impact on highly stressed WP region
 - Simplify manufacturing processes
 - Conduit machining
 - Weldment shape & size
 - Length of closure weld and proximity to conductor
- One design has emerged as simple, robust and meeting design requirements:
 - “Heavy-wall boss” similar to traditional fitting used in ASME Class I nuclear power industry
- Advantages of this particular design:
 - Circumferentially much shorter than the reference design
 - Reduces structural impact on the ID turn
 - Reduces risk of damaging conductor during machining and welding operations
 - Allows toroidal location to float enough to avoid compounding stress fields with conduit butt-welds
 - Simplifies manufacturing issues
 - Easier tooling
 - Faster machining operations
 - Smaller machined region
 - Weld surfaces are accessible for inspection, cleanup/grinding (improved fatigue)
- Structural and hydraulic performance were evaluated

Inlet features



The oblong hole is made by three overlapping round holes

The highest stress and highest B – lowest Tcs
60 kcycles in operation



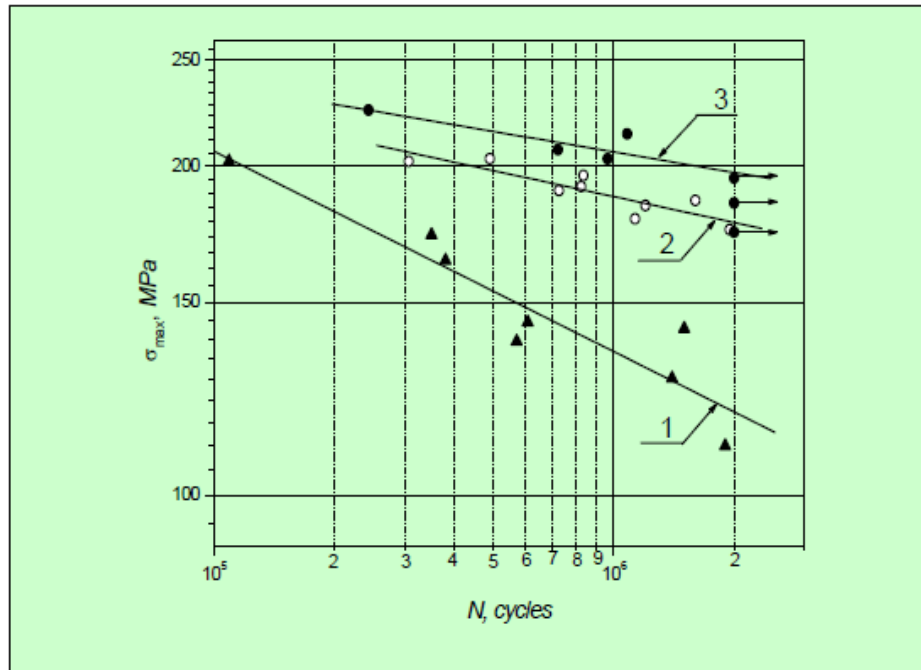
Two peaks of the equivalent stress amplitude –
pretty high: Cumulative Usage Factor is close to
1.0

- Qualification by analysis: too close to allowable
- Recommended Ultrasound Peening to increase fatigue endurance

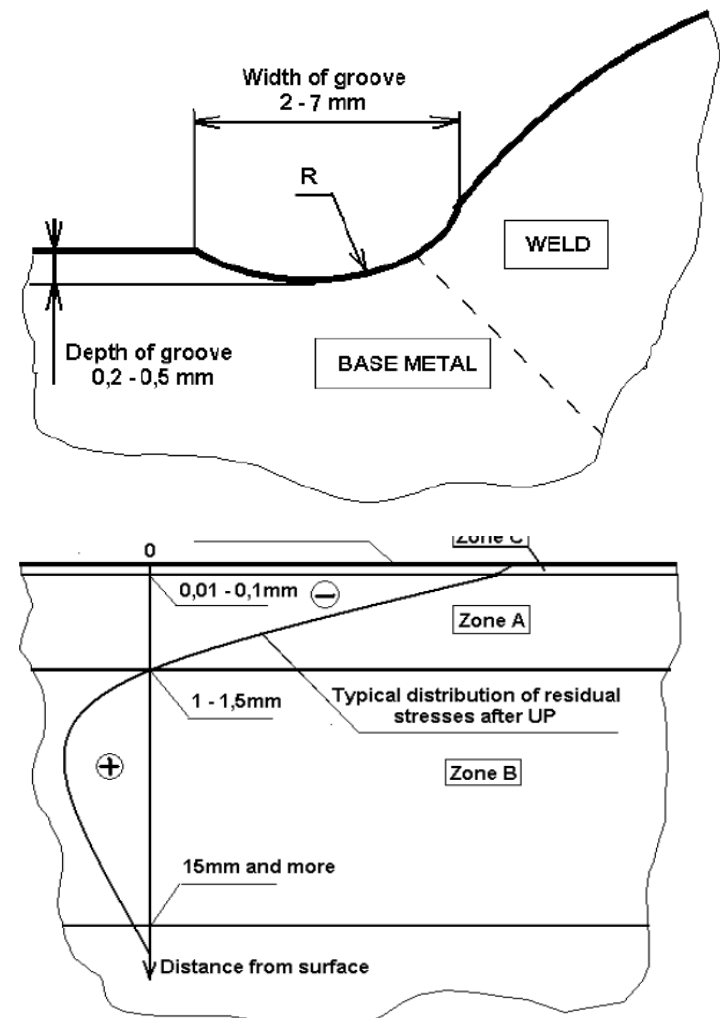


Basic UP system for fatigue life improvement of parts and welded elements

Ultrasound peening extends life of welded joints

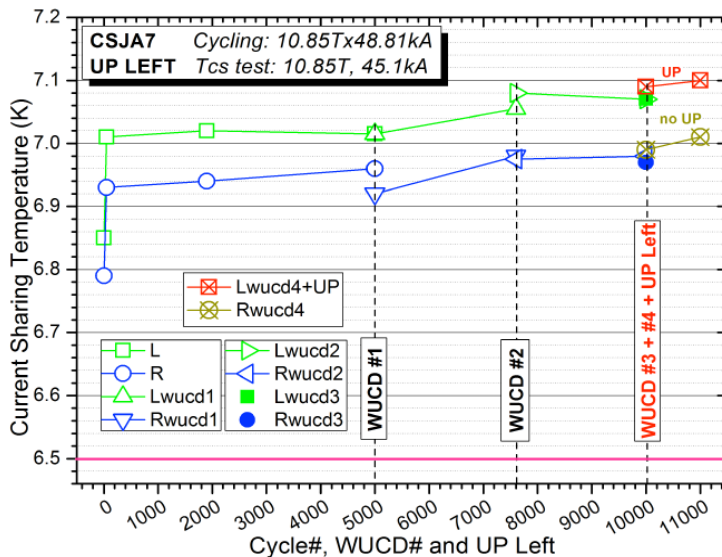
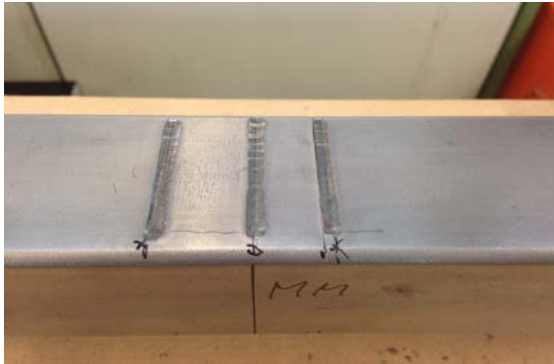


Fatigue curves of large-scale welded samples (transverse non-load-carrying attachment, $R=0$):
 1 – in as-welded condition, 2 – UP was applied before fatigue testing,
 3 – UP was applied after fatigue loading with the number of cycles corresponding to 50% of expected fatigue life of samples in as-welded condition



UP – before or after HT?

Concern will UP damage the superconductor?

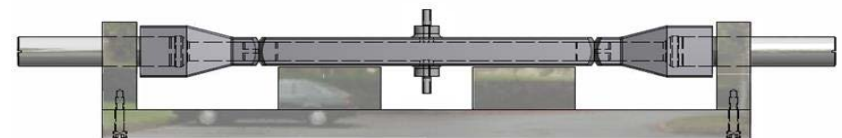


Study showed – UP does not damage the superconducting properties

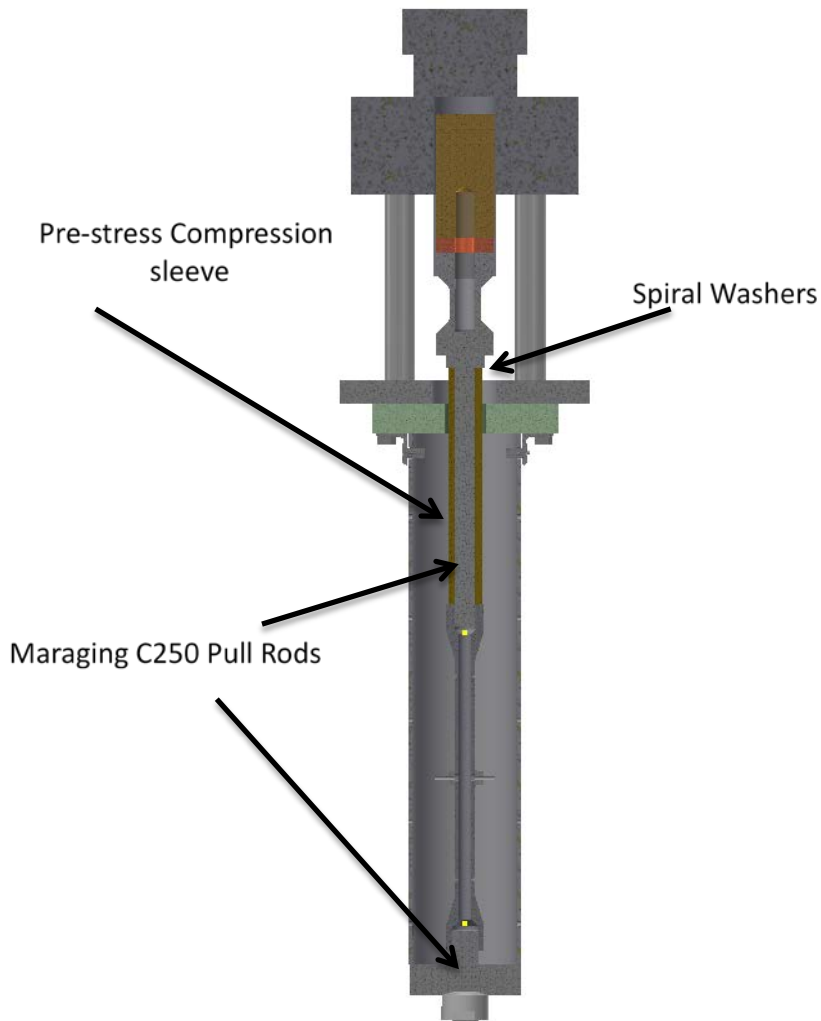
Qualification by testing

| | |
|---|-----------------------------------|
| Total number of specimens | 6 |
| Number of UP treated specimens | 5 (10 with two inlets per sample) |
| Stress | As in operation |
| Cycles in operation | 60 000 |
| Minimum number of test cycles required* | 540 000 |

*code EN 13445 – geometrically mean



Inlet testing

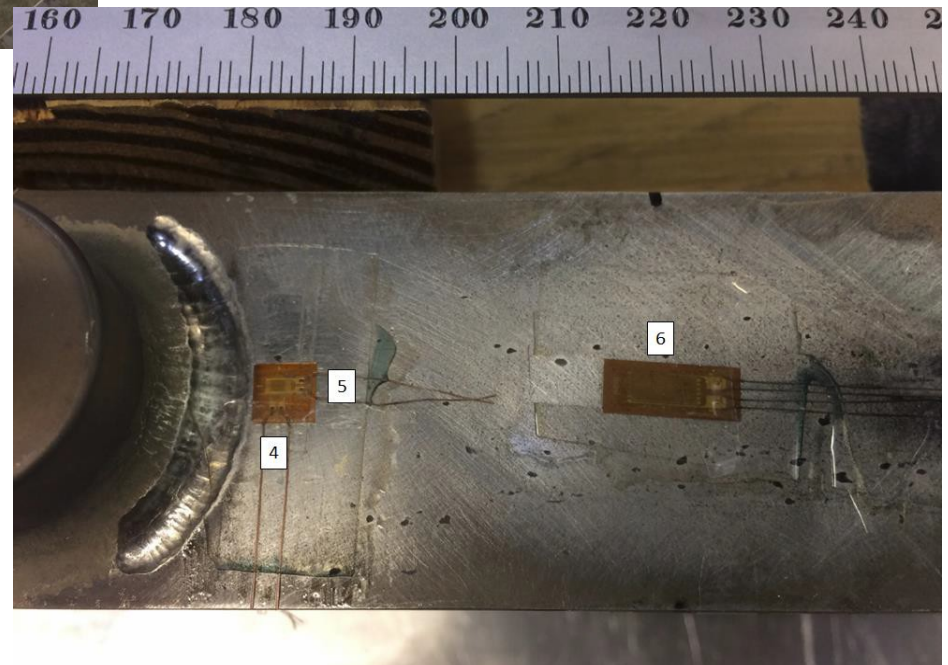
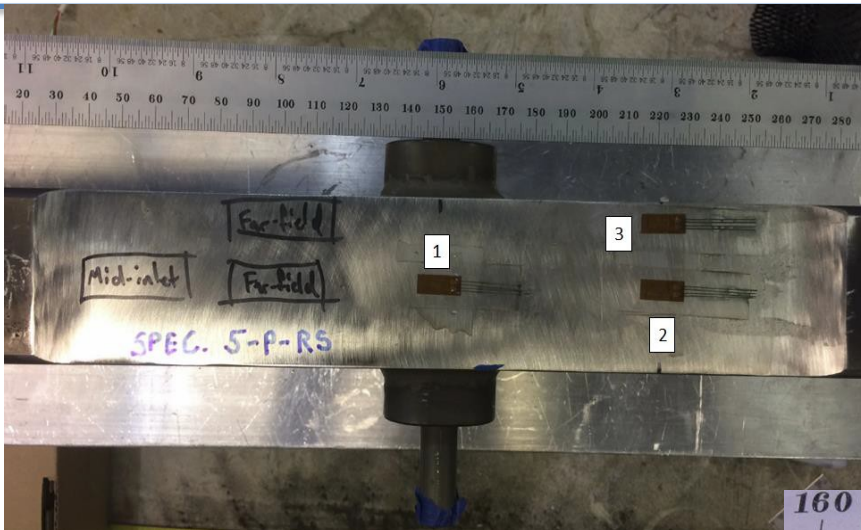


Schematic of test specimen and fixture, liquid nitrogen bucket dewar is not shown.

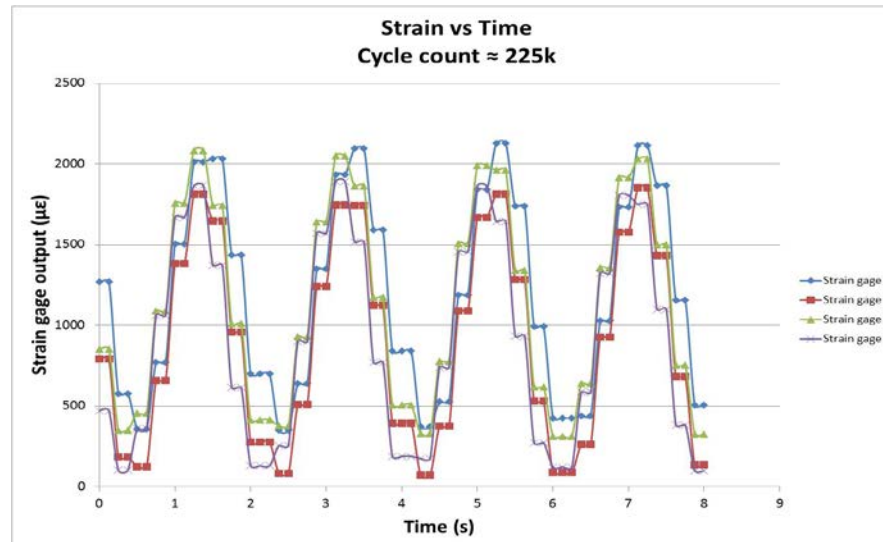
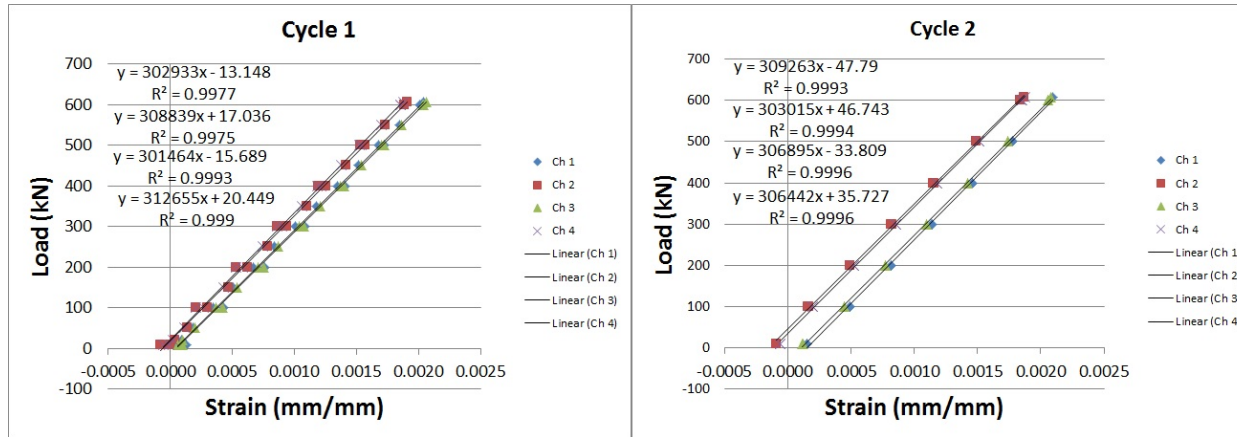
Testing arrangement



Strain gauge instrumentation



Typical stress-strain curve

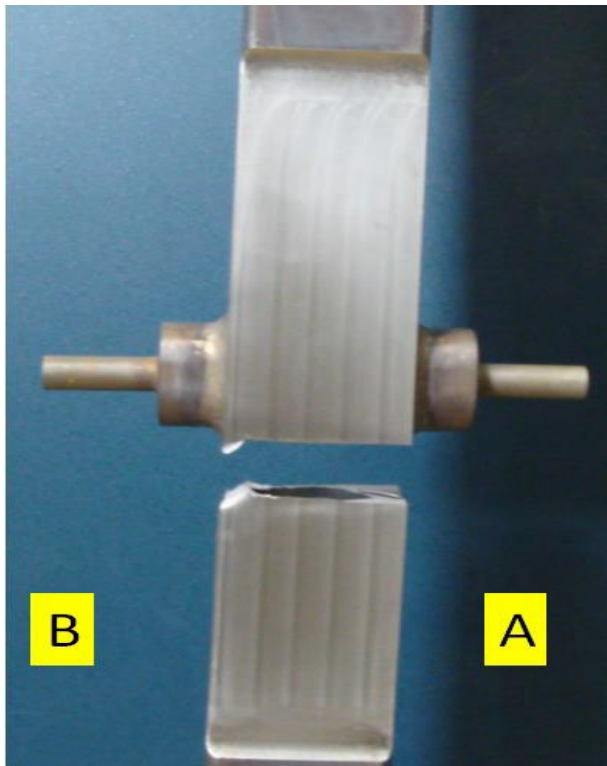


CS inlets testing summary



| Condition | Sample ID | Max force, kN | Max fatigue stress, MPa | Nominal fatigue stress range, MPa | Cycles to failure | Comments |
|---------------------|-----------|---------------|-------------------------|-----------------------------------|-------------------|--|
| As welded + HT | 1-AW-RS | 434 | 336 | 303 | 158,451 | Crack originated at the weld toe |
| As welded + HT + UP | 1-P-RS | 434 | 336 | 303 | 337,491 | Crack originated at the hole in the jacket |
| | 2-P | 607 | 387 | 348 | > 540,000 | Did not fail and reached designed number of cycles |
| | 3-P-RS | 434 | 336 | 303 | > 850,660 | The inlet did not fail, but the grip failed |
| | 4-P-RS | 434 | 336 | 303 | 723,317 | Crack originated at the hole in the jacket |
| | 5-P-RS | 434 | 336 | 303 | 534,518 | Crack originated at the hole in the jacket |

Fractures in UP and not UP treated specimens



As welded – not UP
treated failed after 158.5
kcycles at the weld toe



UP treated failed after
534.5 kcycles at the
drilled hole

- The ITER CS inlets meet requirements for fatigue testing presented in national and international structural codes
- Ultrasonic peening is a necessary condition for fabrication of the inlets with sufficiently long life for ITER CS. Ultrasonic peening extends life of the inlets by a factor of 3.5–5 or higher.
- All failures in the peened specimens were initiated in the second-highest stress location—the area where the cable space meets the drilled hole of the inlet. This agrees with the FEA and fracture mechanics predictions.