

Welcome!

Cockcroft Institute Lectures – Register Attendance

CI-ACC-221: Ion Sources and Secondary Beams

Dan Faircloth (DF) RAL/STFC

CI-RF-222: RF Linear Accelerators

Graeme Burt (GB) CI/Lancaster University

CI-ACC-225: Electron Sources

Boris Militsyn (BM) CI/ASTeC

CI-ACC-226: Machine Learning Methods for Particle Accelerators

Andrea Santamaria Garcia (ASG) CI/University of Liverpool

Date/time	10:30	11:45	14.00
9 Feb 2026	Ion Sources	Penning Magnetron	
16 Feb 2026	High Voltage		Secondary Beams



QR code will take you to a Google form

Record attendance for each day of lectures

Technological Aspects: High Voltage

Dan Faircloth

ISIS Low Energy Beams Group Leader

Rutherford Appleton Laboratory

STFC-UKRI

Uses of high voltage in particle accelerators

- Extracting beams (up to 50 kV)
- Accelerating beams (up to 28000 kV)
- Initiating discharges / pre-ionising gases (up to 20 kV)
- Focusing and deflecting beams (up to 50 kV)
- Suppressing unwanted particles (up to 5 kV)

Ion sources are particularly challenging for HV design

Explosive gasses (hydrogen)

High temperatures

Other contaminants (e.g. Cs)

Magnetic fields

Large amounts of charge carriers

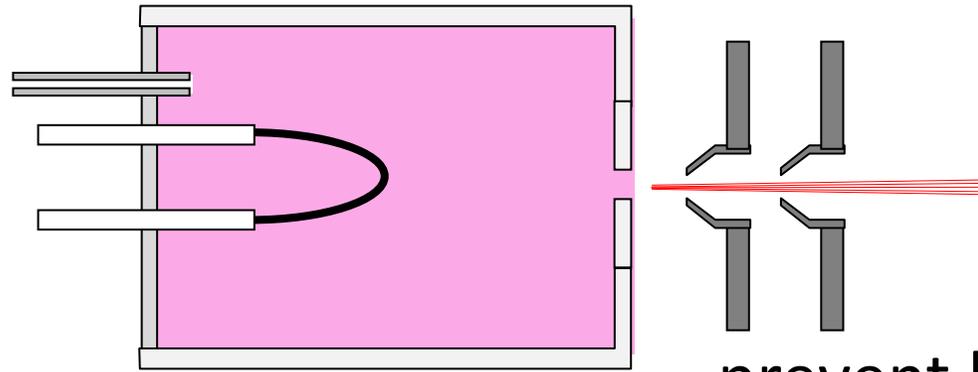
Stray beams: electrons and ions

X-rays

Compact design

Main aim of high voltage design:

Produce reliable breakdown
... where we want it



prevent breakdown

...where we don't want it

Electrical Breakdown

- Global Breakdown
 - Complete rupture or failure of the insulation between two electrodes
- Local Breakdown
 - Partial breakdown of part of the insulation between two electrodes

This may instantaneously cause permanent damage,
or damage might slowly occur,
or the system may come to no harm.

Electrical Breakdown

- Electric field strength is the primary factor
- In general electrical breakdown is most likely to occur where the electric field is highest, but this depends on:
 - Materials and gasses
 - Pressures
 - Temperatures
 - Surfaces
 - Magnetic fields
 - Stray beams
 - Charges
 - Photons

Electric Field

- Potential gradient, electric field strength, electric field intensity, stress, E
- Units of Vm^{-1} , kVm^{-1} , kVmm^{-1} , kVcm^{-1}
- Equations, Analytical , Empirical, Numerical

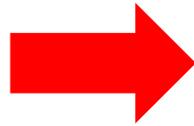
$$E = \frac{V}{d}$$

Maxwell's Equations

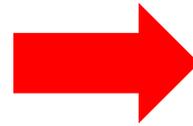
$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$$

For electrostatic fields:

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$



$$\nabla \times \mathbf{E} = 0$$



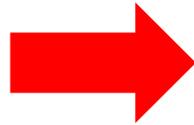
$$\mathbf{E} = -\text{grad}\phi$$

$$\nabla \cdot \mathbf{B} = 0$$

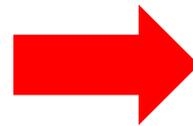


$$\mathbf{D} = \epsilon \mathbf{E}$$

$$\nabla \cdot \mathbf{D} = \rho$$



$$\nabla \cdot \mathbf{D} = \rho$$



$$\nabla^2 \phi = \frac{\rho}{\epsilon}$$

or

Poisson's Equation

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial z^2} = \frac{\rho}{\epsilon}$$

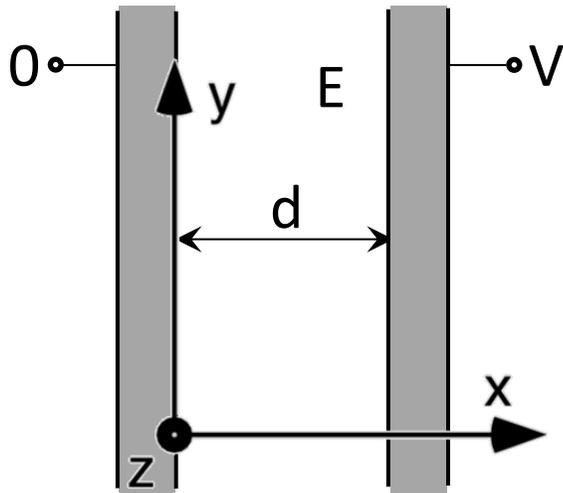
if $\rho = 0$:

Laplace's Equation

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial z^2} = 0$$

Using Laplace's Equation

Infinite parallel plates:



$$\mathbf{E} = -\text{grad}\phi$$

$$\therefore \mathbf{E} = -\frac{V}{d}$$

$$\Rightarrow |\mathbf{E}| = \frac{V}{d}$$

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial z^2} = 0$$

ϕ does not vary with y or z : $\frac{\partial \phi}{\partial y} + \frac{\partial \phi}{\partial z} = 0$

$$\therefore \frac{\partial^2 \phi}{\partial x^2} = 0$$

$$\Rightarrow \frac{\partial \phi}{\partial x} = c_1$$

$$\Rightarrow \phi(x) = c_1 x + c_2$$

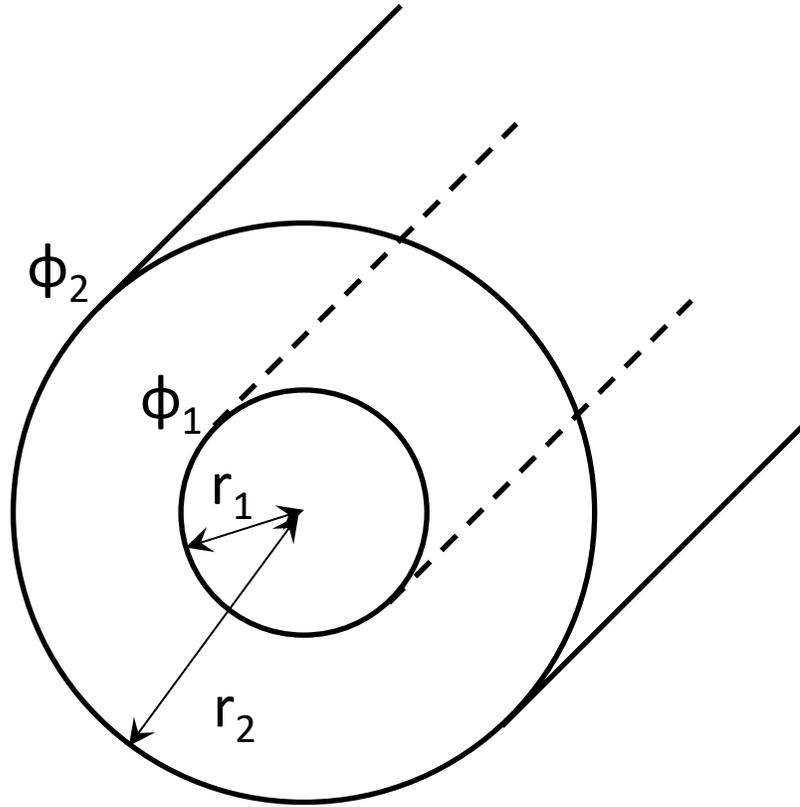
At $x = 0$, $\phi = 0$ and at $x = d$, $\phi = V$

$$\therefore c_1 = \frac{V}{d} \quad \text{and} \quad c_2 = 0$$

$$\therefore \phi(x) = \frac{V}{d} x$$

Similarly....

$$\frac{1}{r} \cdot \frac{\partial}{\partial r} \left(r \frac{\partial \phi}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \varphi^2} + \frac{\partial^2 \phi}{\partial z^2} = 0$$



$$\phi(r) = \phi_1 + \frac{\phi_1 - \phi_2}{\ln\left(\frac{r_1}{r_2}\right)} (\ln r - \ln r_1)$$

$$E(r) = \frac{\phi_1 - \phi_2}{r \ln\left(\frac{r_2}{r_1}\right)}$$

$$E_{\max} = \frac{\phi_1 - \phi_2}{r_1 \ln\left(\frac{r_2}{r_1}\right)}$$

Fine for simple geometries...

thankfully we have computers

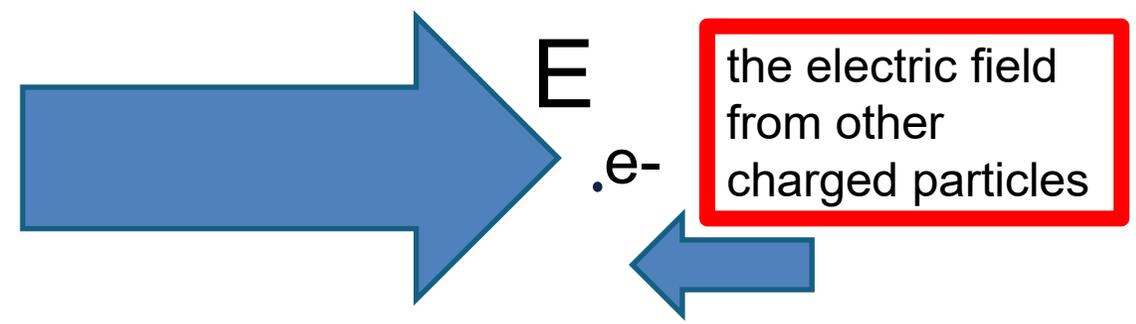


3D Modelling Software- Commercial and Open Source



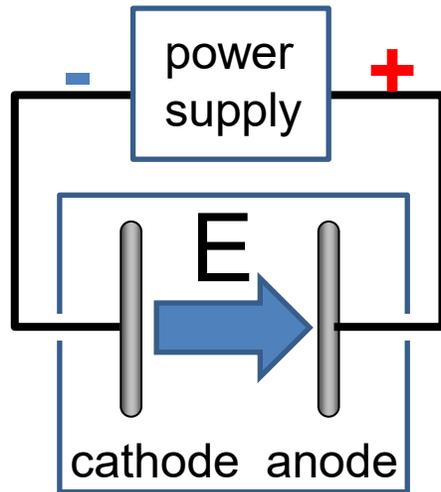
Plus many others...

Accelerating electrons



Capacitively Coupled Plasmas (CCP)

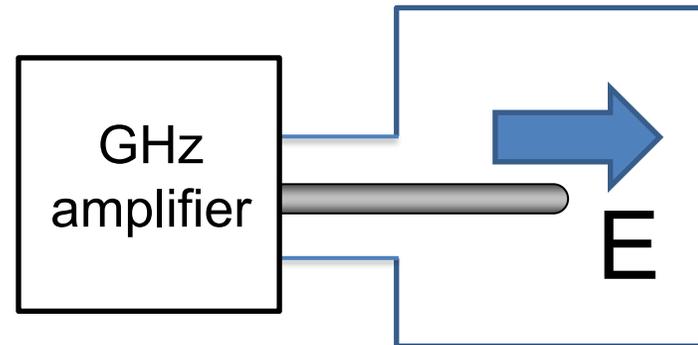
voltage applied to electrodes creates the electric field



many different electrode and magnetic field configurations
DC and AC

Electromagnetic Cavity Plasmas - waveguide or coax coupled

the electric field component of the electromagnetic oscillation in a cavity

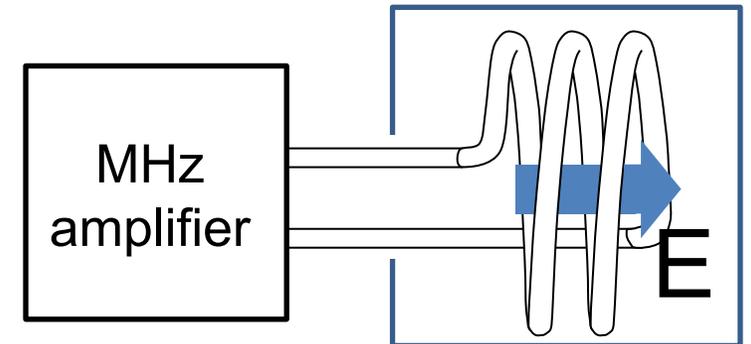


“Microwave sources”
“ECR sources”

Inductively Coupled Plasmas (ICP)

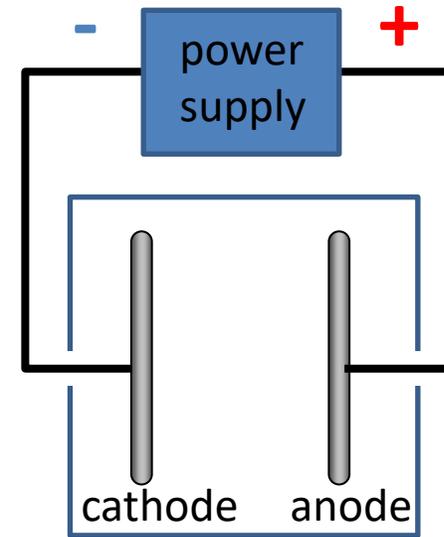
a time varying current in a coil creates a time varying magnetic field that induces a time varying electric field

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

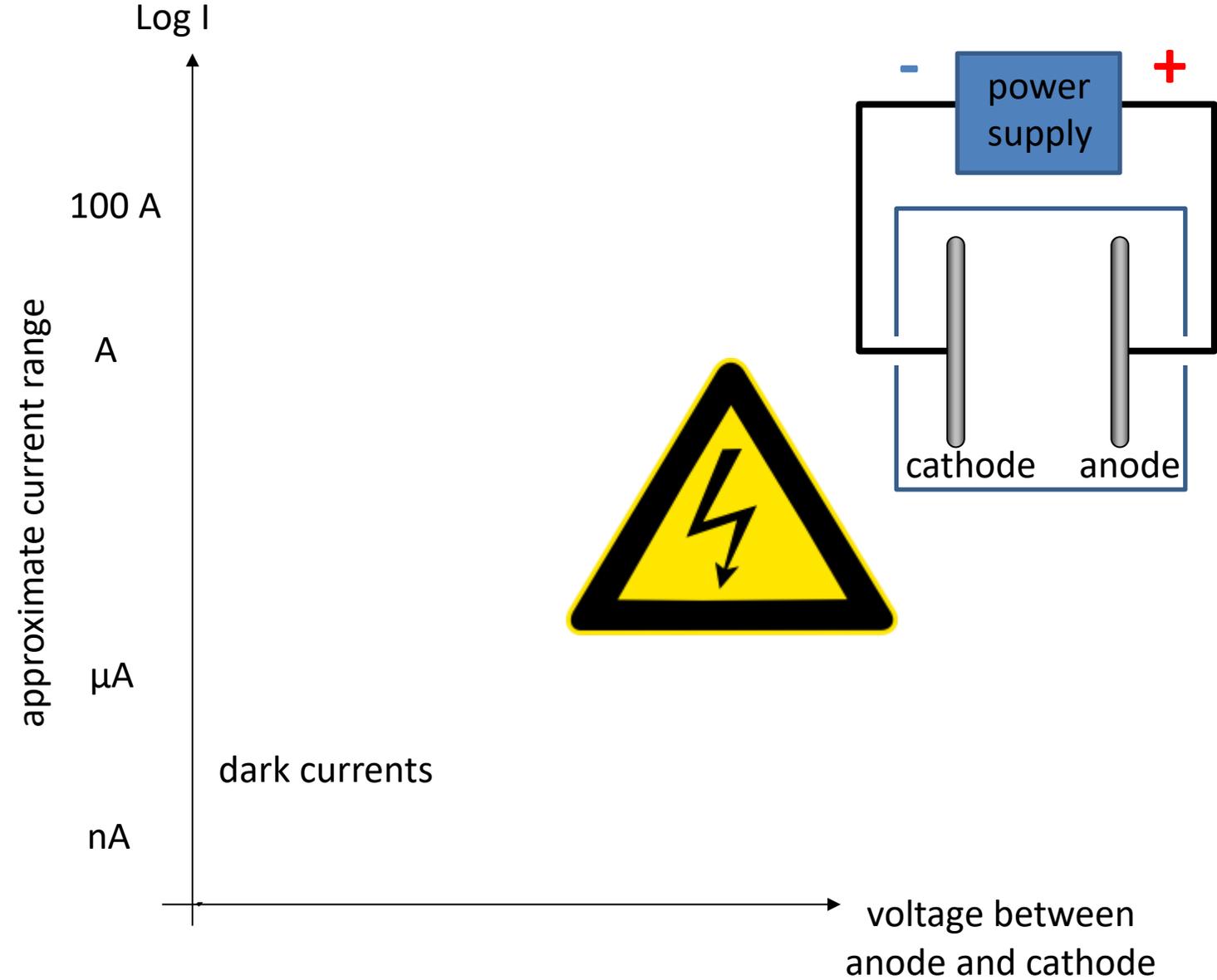


“RF sources”

Electrical Discharges



Electrical Discharges



Avalanche

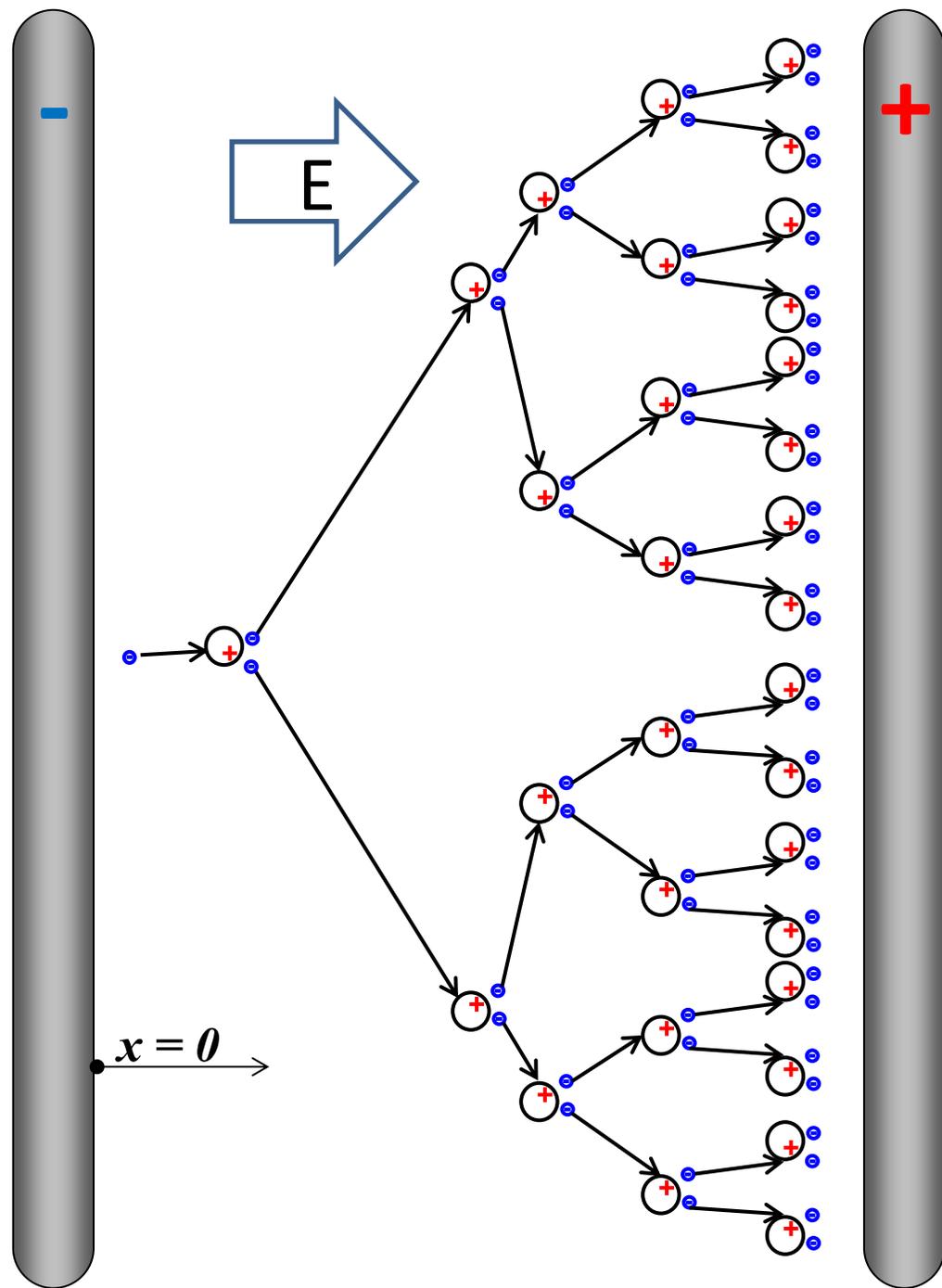


John Townsend
"Townsend discharge"
1897

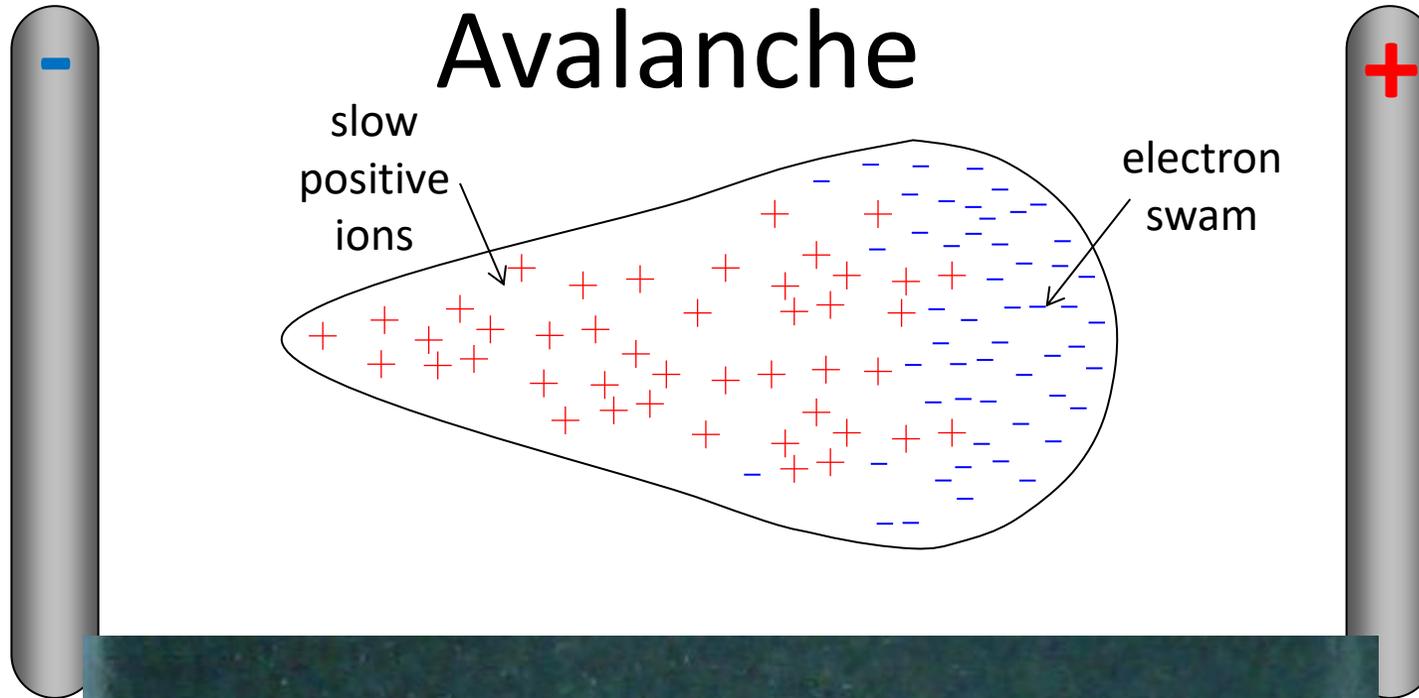
$$dn_x = n_x \alpha dx$$

By integration and $n_x = n_0$ at $x = 0$

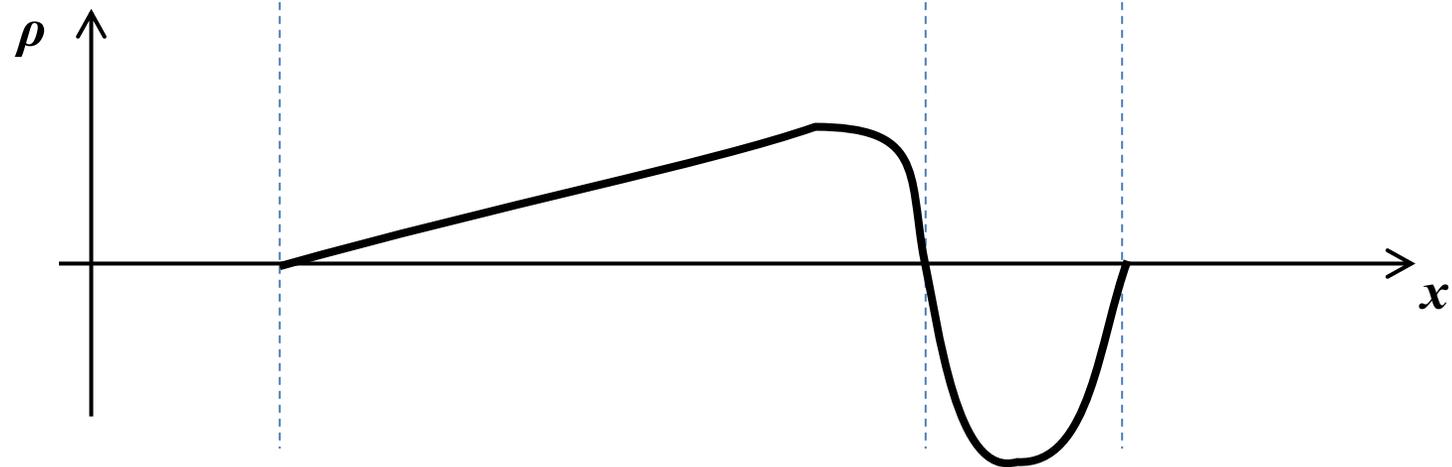
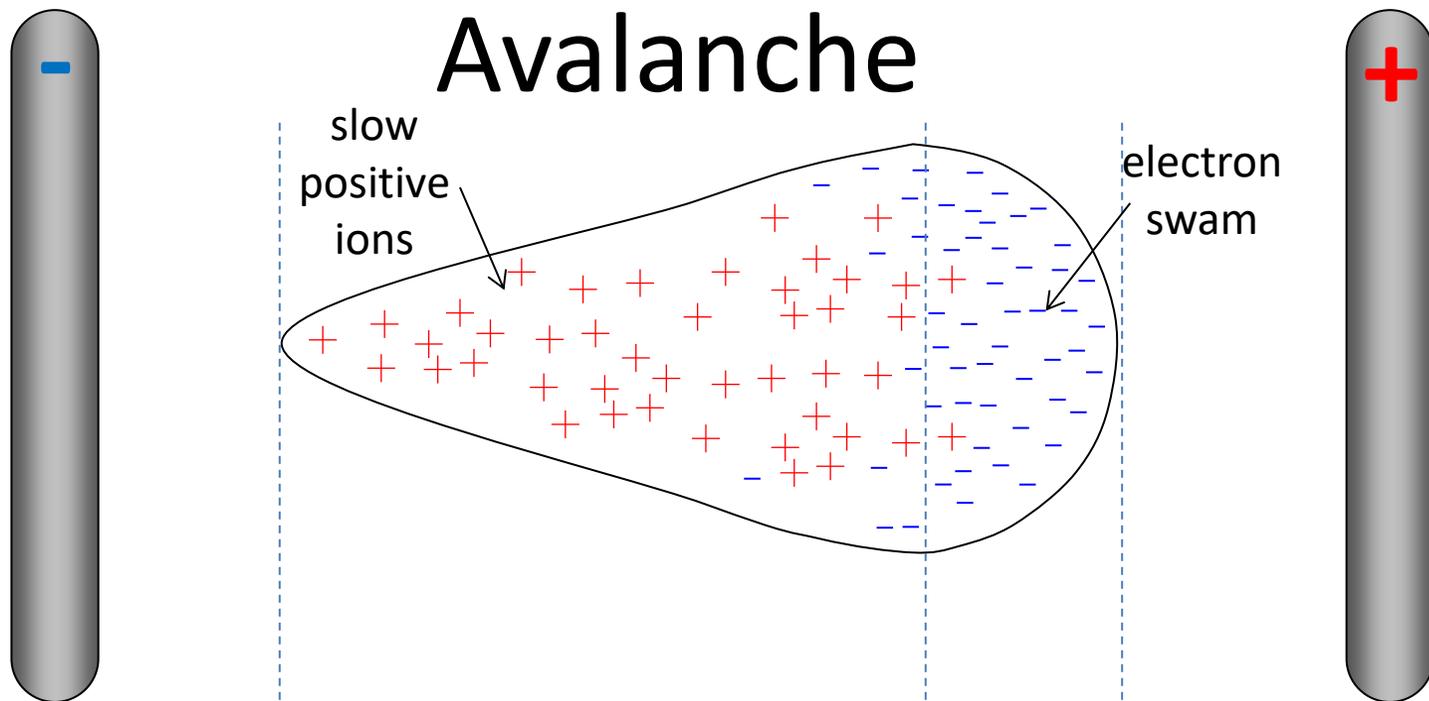
$$n_x = n_0 e^{\alpha x}$$



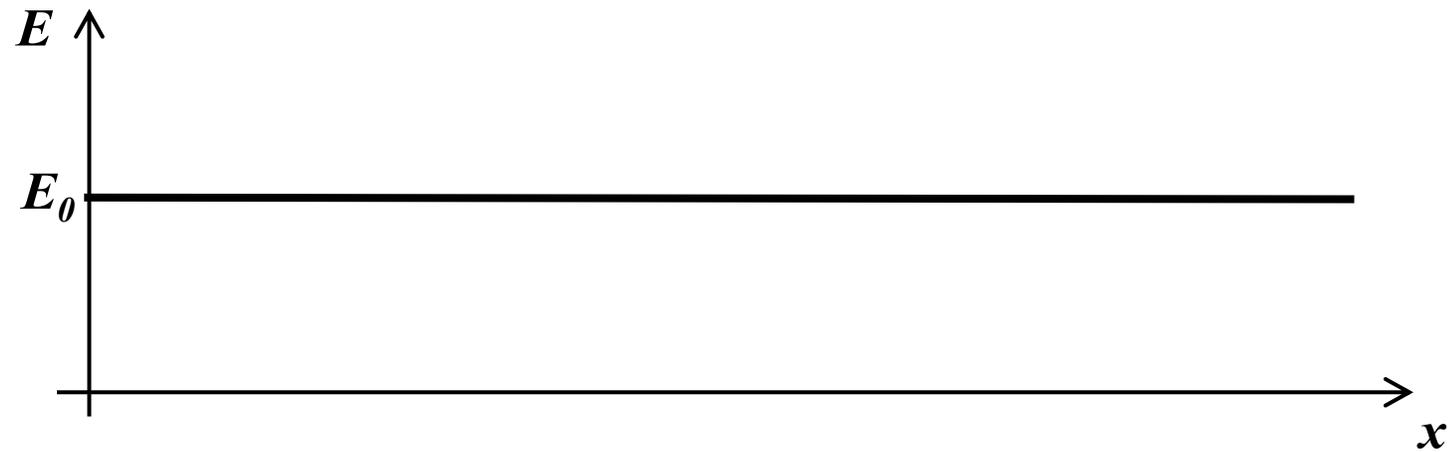
Avalanche



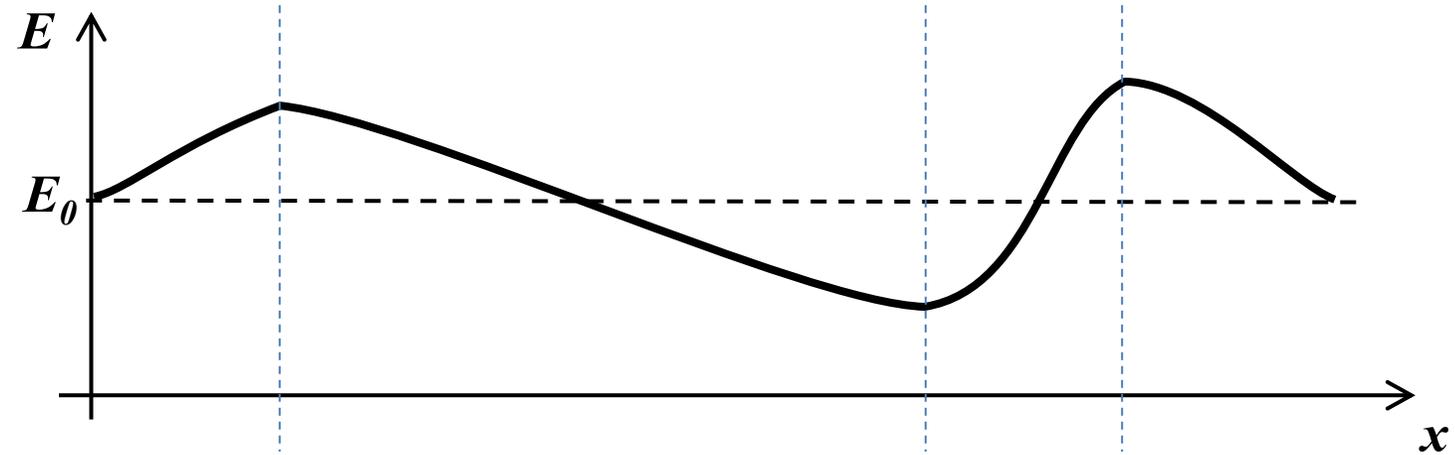
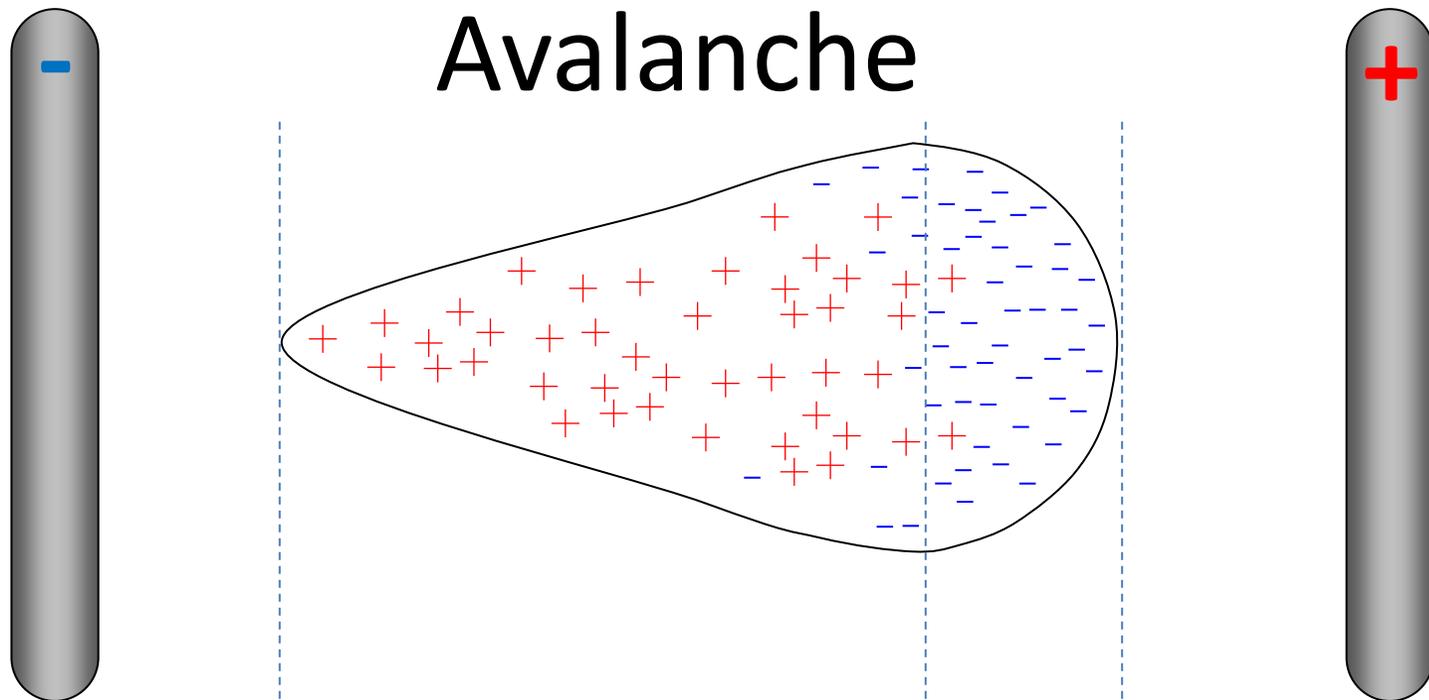
Avalanche



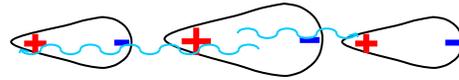
Avalanche



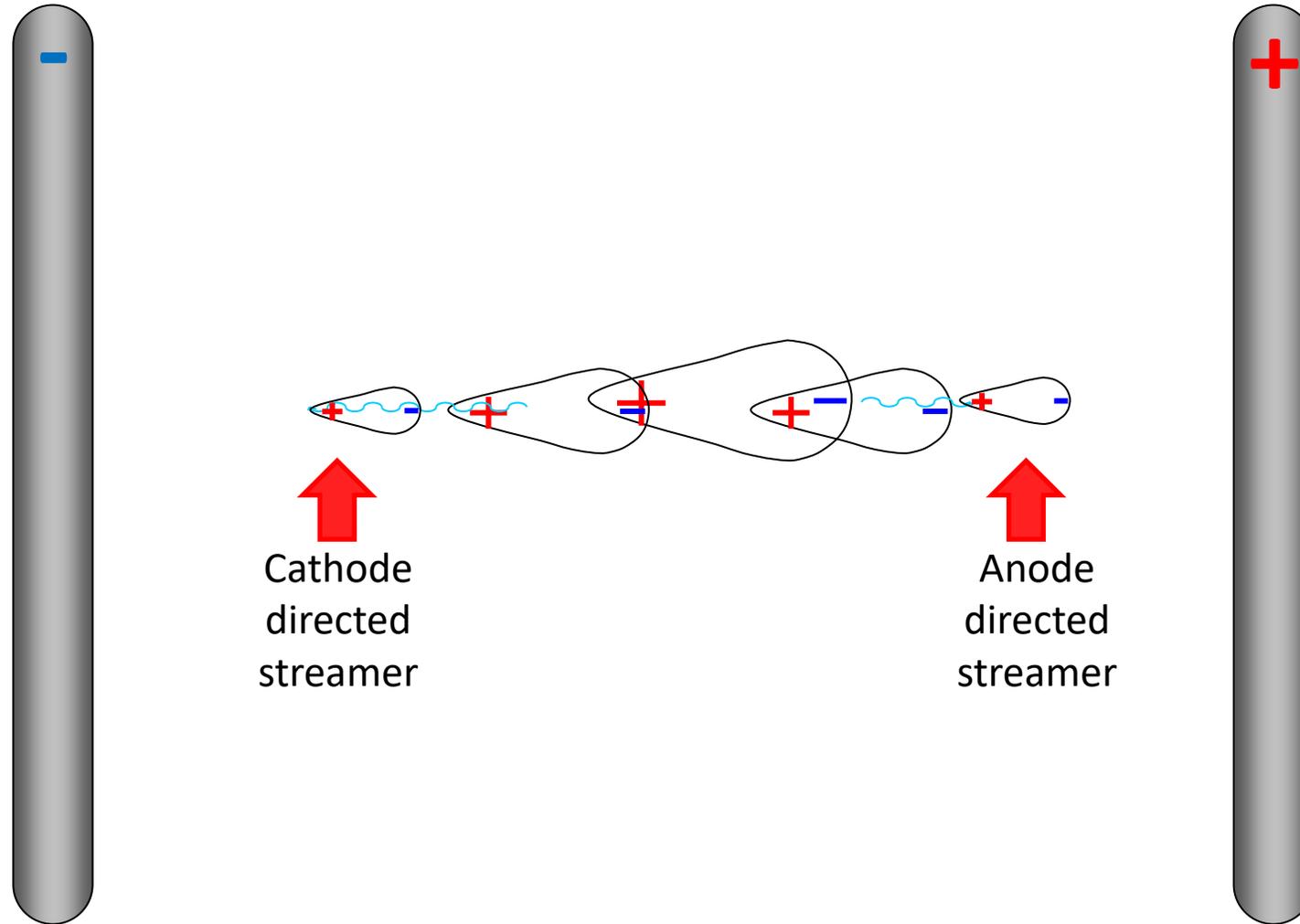
Avalanche



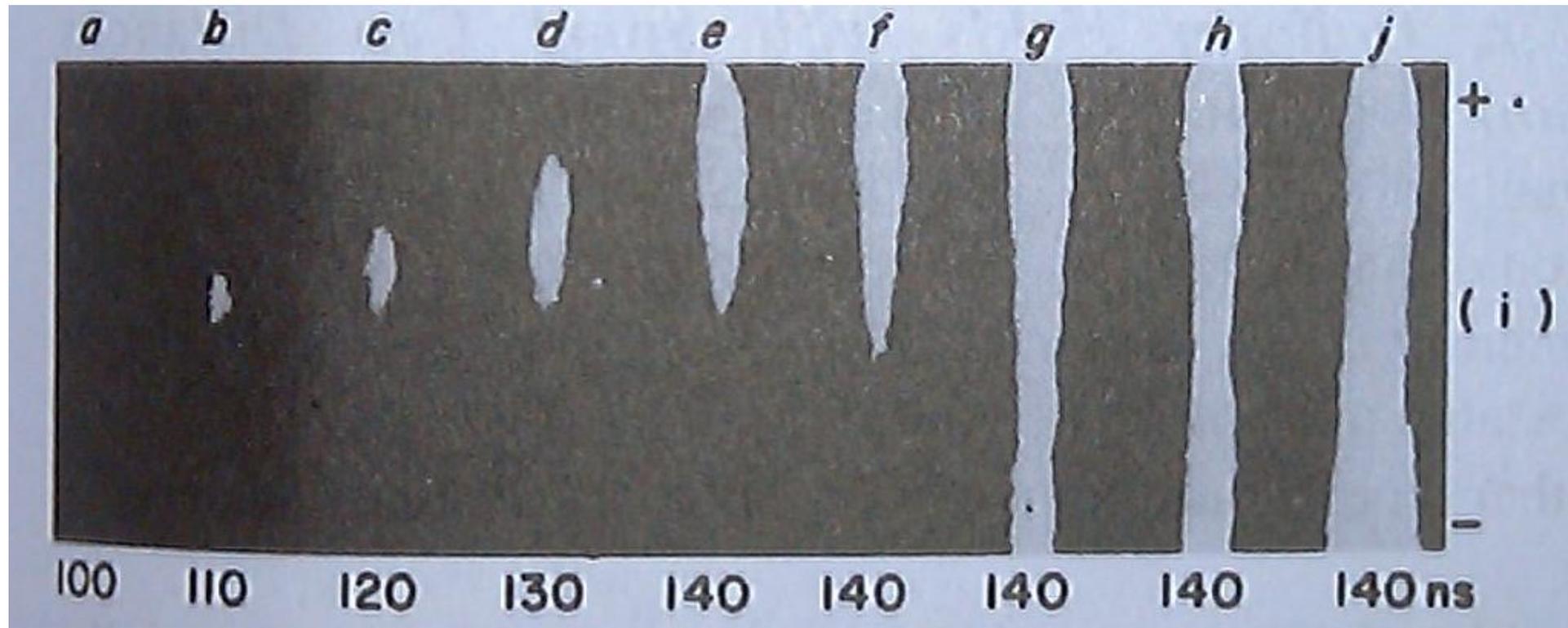
Streamer



Streamer



Streamer



Townsend Secondary Ionisation Coefficient, γ



John Townsend
"Townsend discharge"
1897

$$dn_x = n_x \alpha dx$$

$$n_x = n_0 e^{\alpha x}$$

γ is the number of secondary electrons produced per electron in the primary avalanche

$$\gamma = \gamma_{ion} + \gamma_p + \gamma_m$$

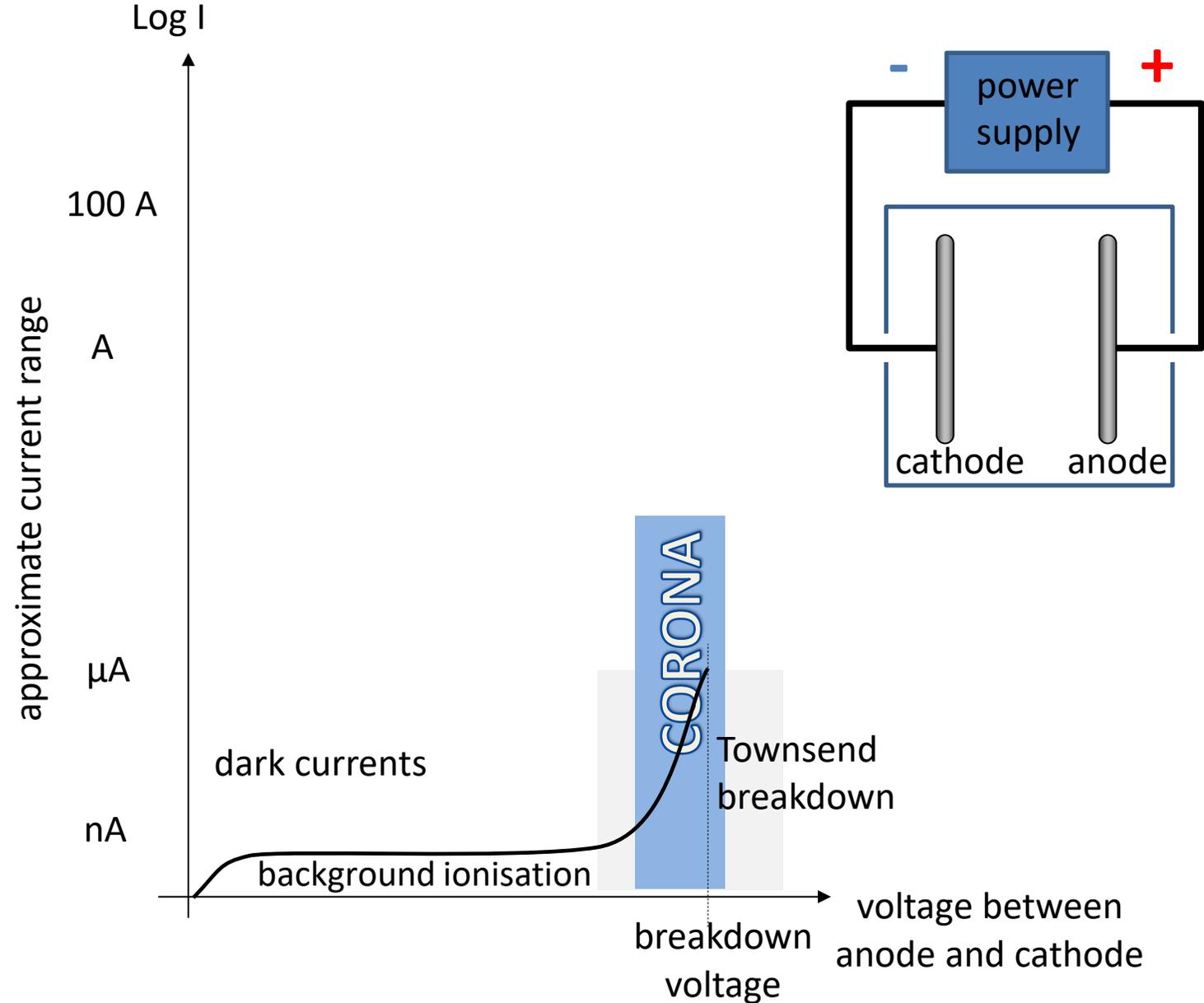
$$I = \frac{I_0 e^{\alpha d}}{1 - \lambda(e^{\alpha d} - 1)}$$

Self sustaining discharge resulting in breakdown when:

$$\gamma e^{\alpha d} = 1$$

Townsend Criterion for Breakdown

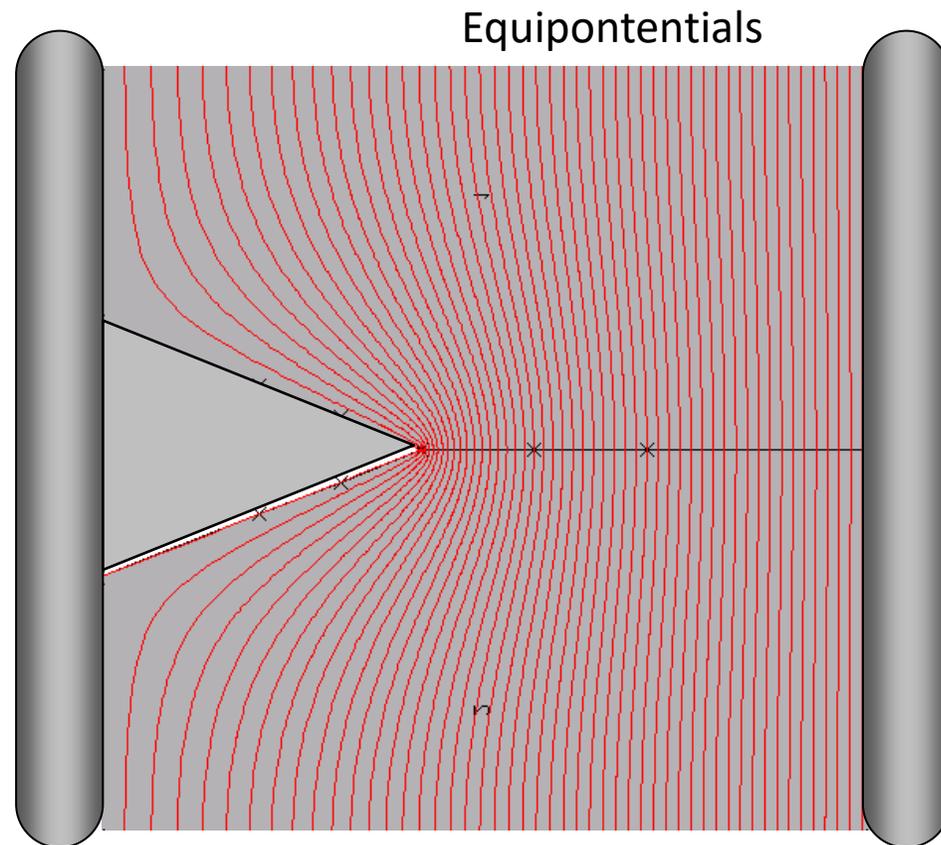
Electrical Discharges





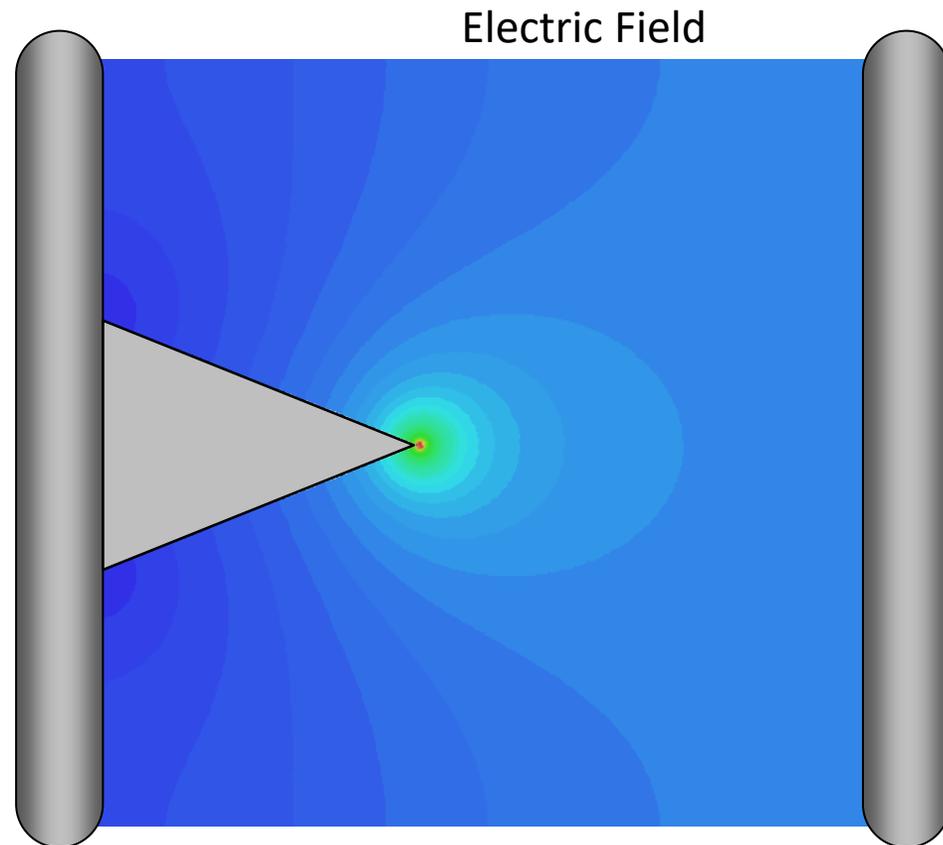
Corona

- Corona is a type of partial discharge occurring in divergent fields
- Divergent fields are caused by sharp points



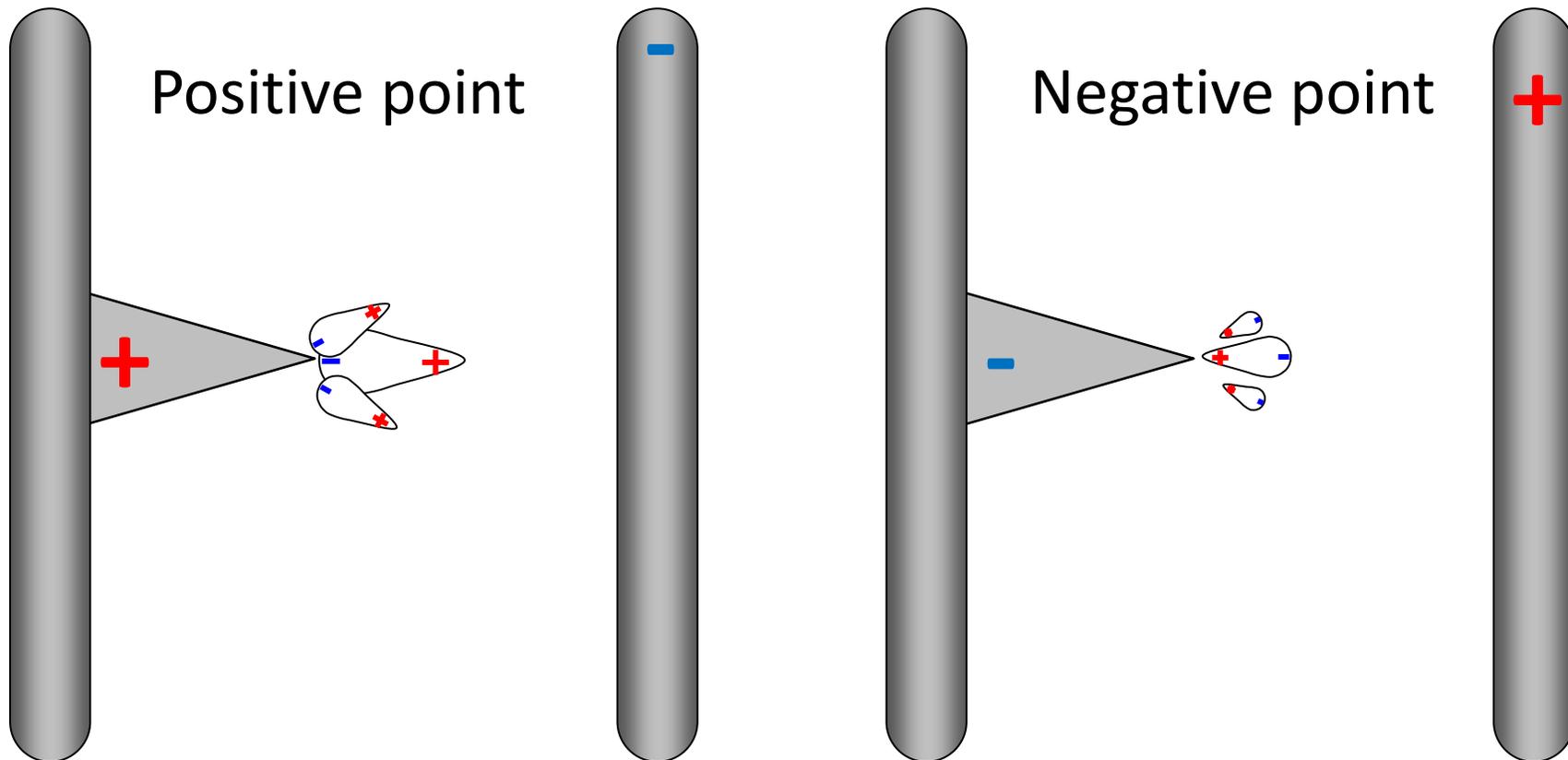
Corona

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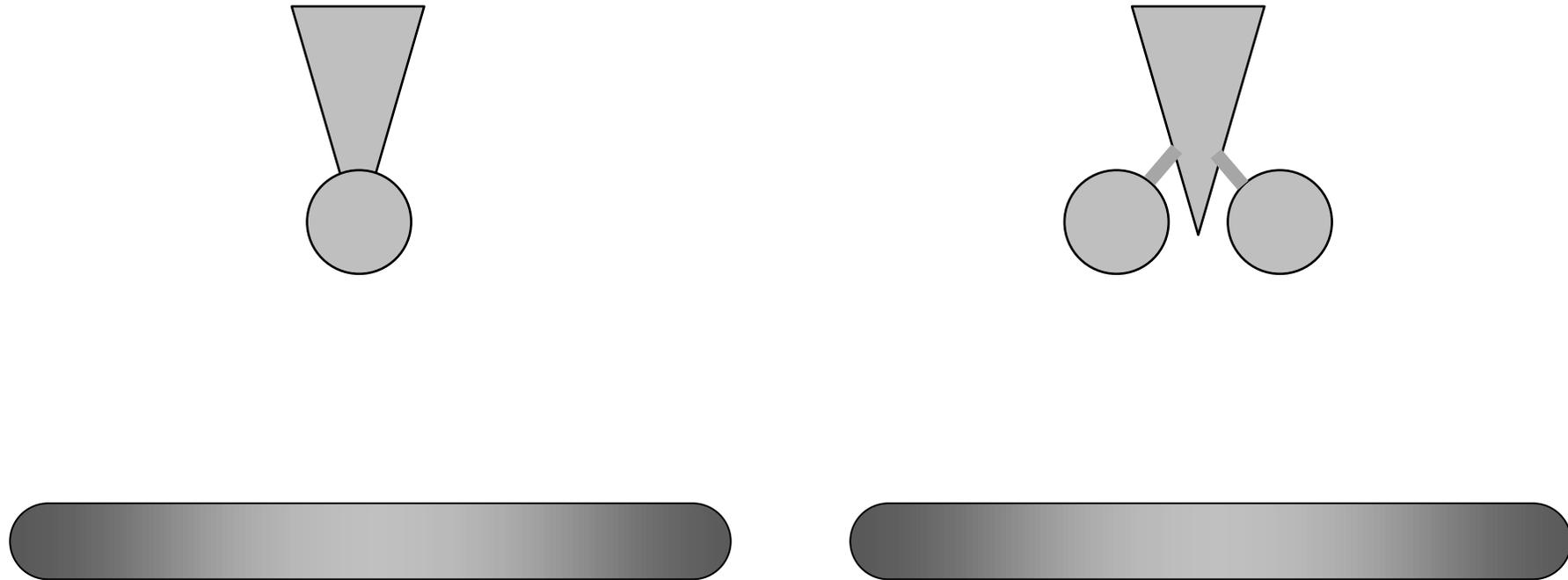
Corona

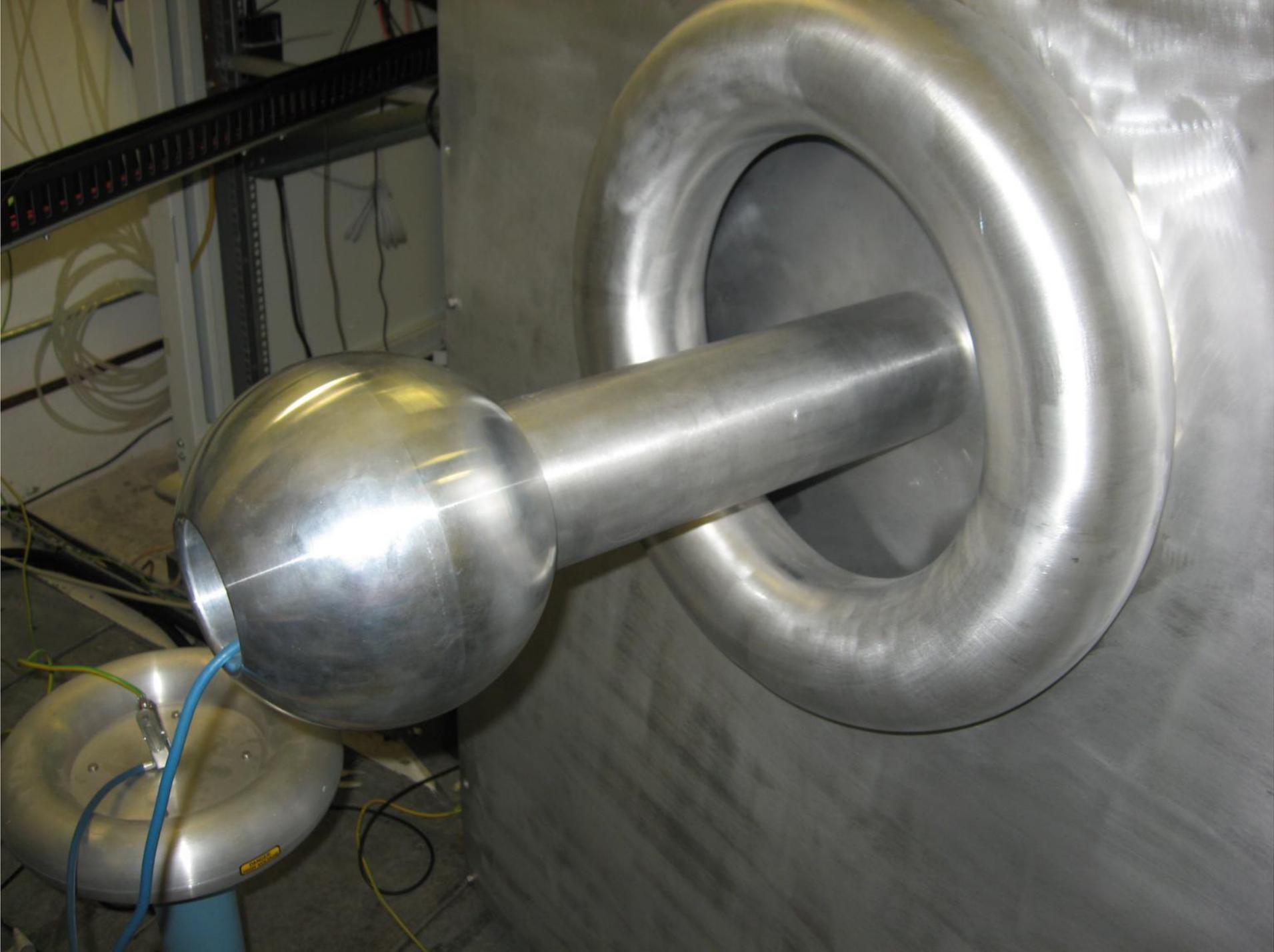
- Corona is a type of partial discharge occurring in divergent fields
- Divergent fields are caused by sharp points
- Discharge behaviour is dependant on polarity



Electrode Design

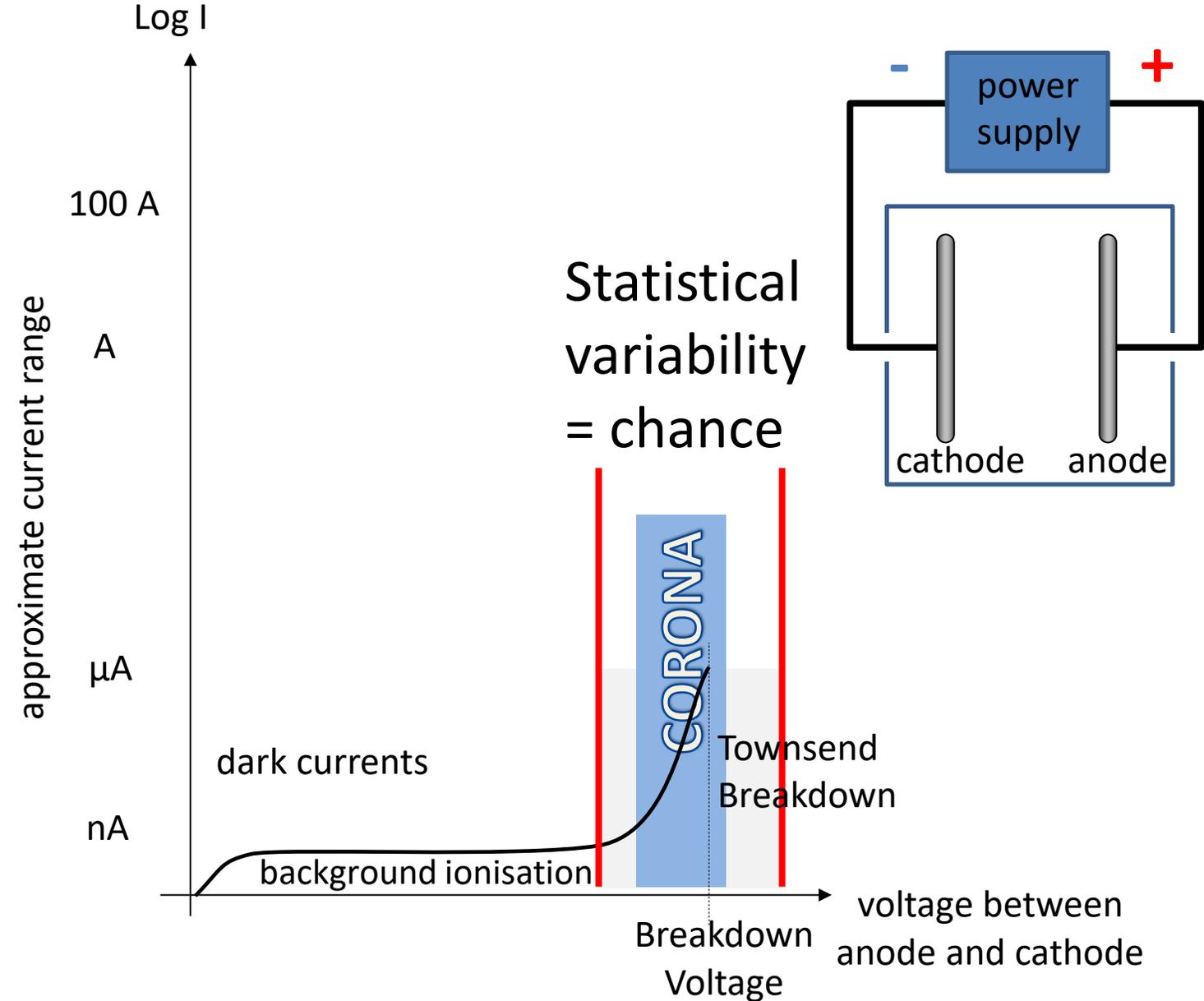
- Minimise electric field by making smooth rounded electrodes
- Shield any sharp points with corona shields







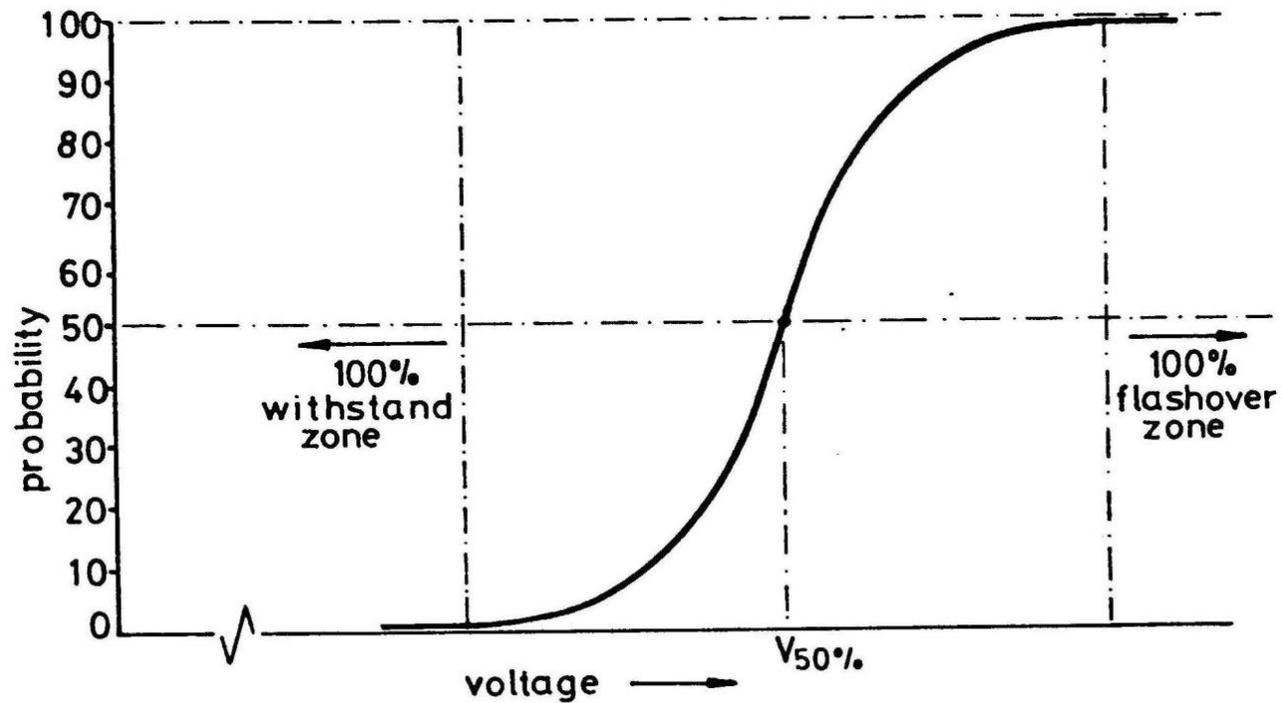
Electrical Discharges

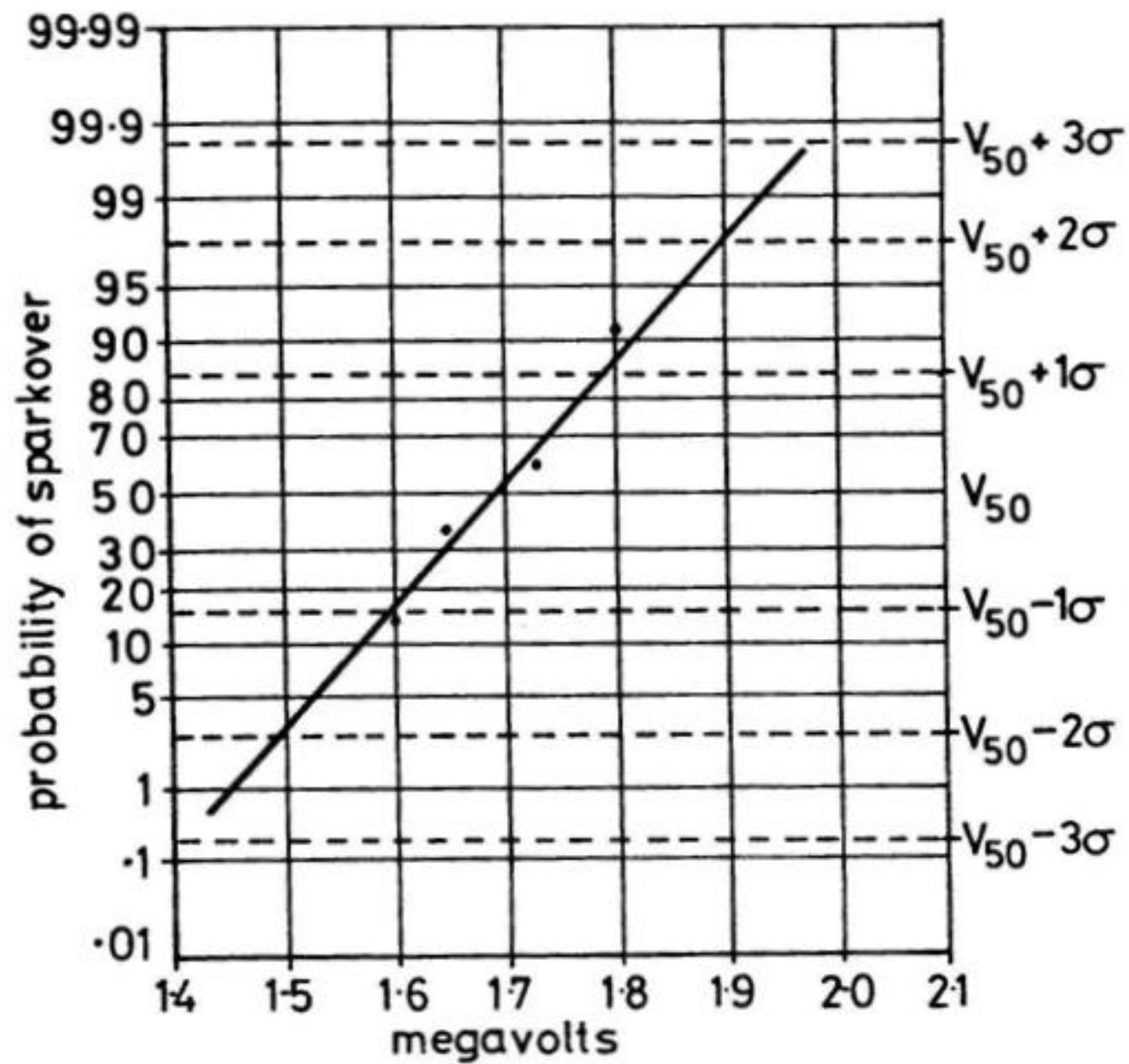


Statistical Variability

Even with identical conditions the same electrode gap will breakdown at different voltages each time the voltage is applied.

This is because of the statistical nature of high voltage breakdown: no two sparks are ever the same.





Environmental conditions

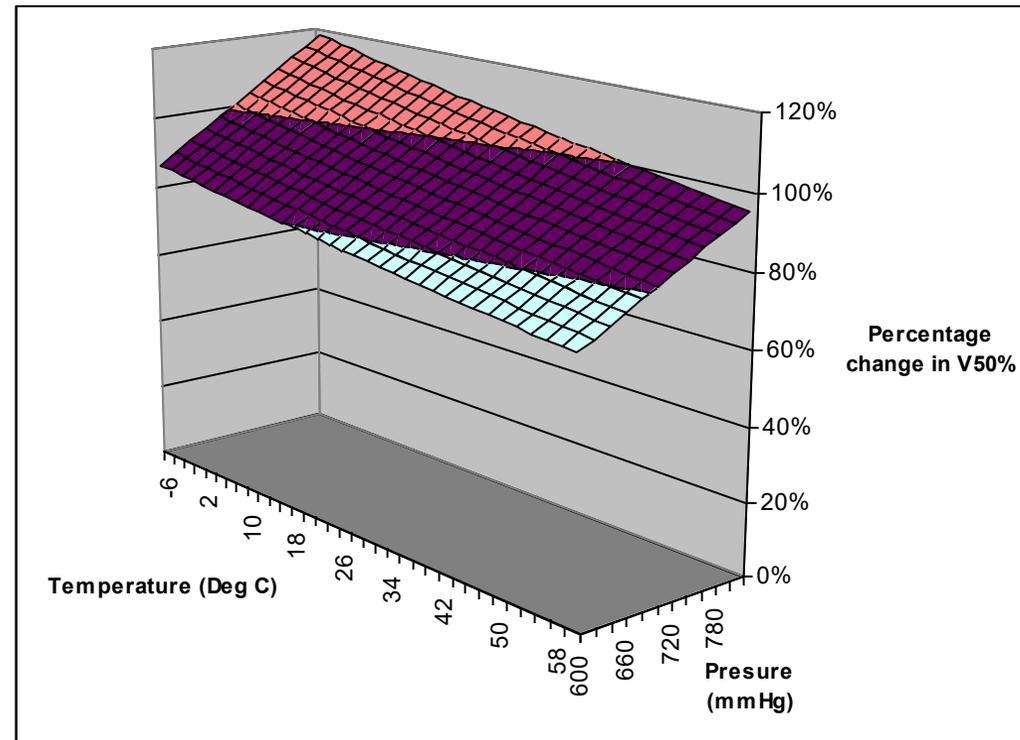
Higher temperatures and lower pressures lead to lower flashover voltages.

A correction factor for V50% can be found from this equation:

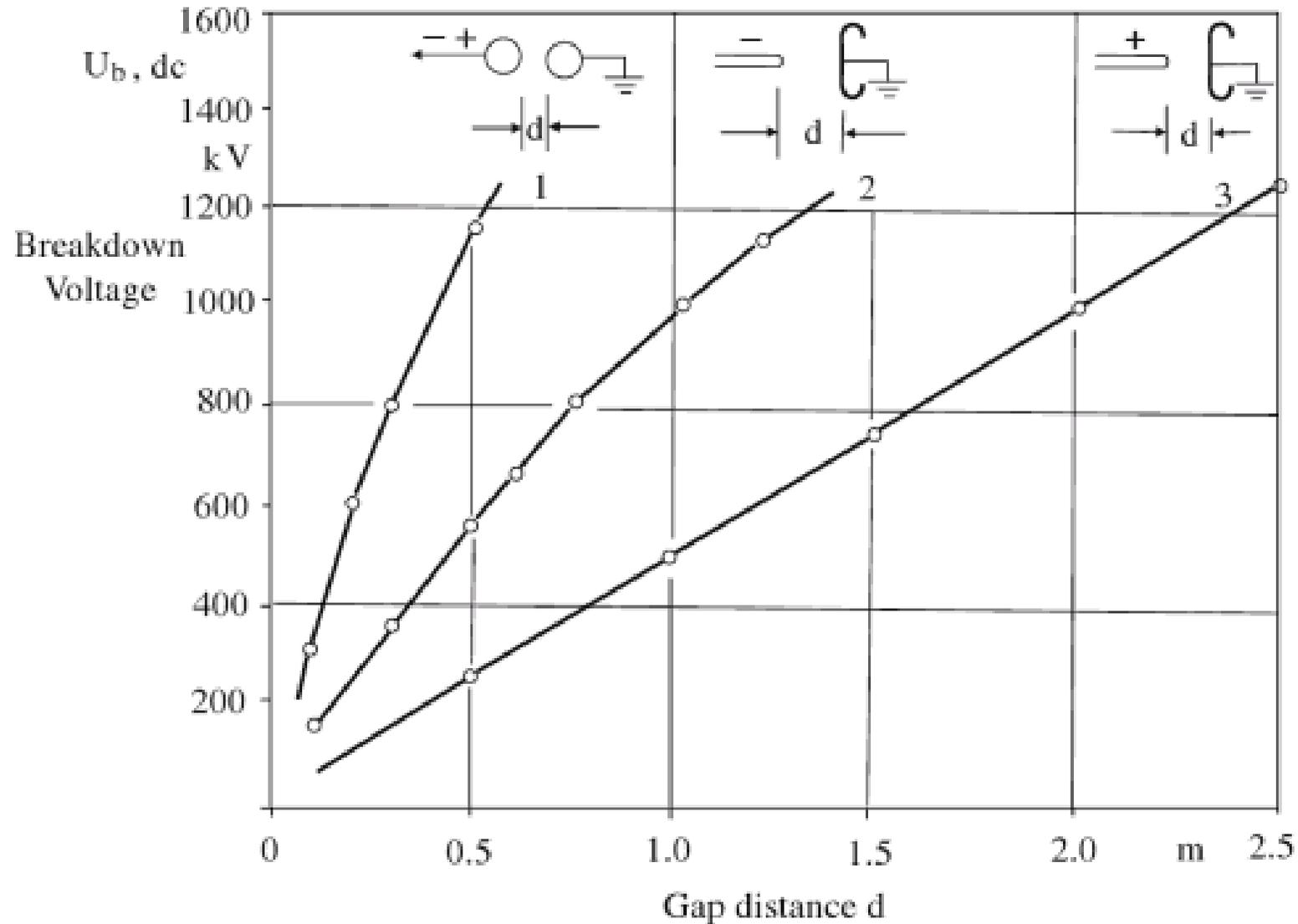
$$\frac{0.386 \times P}{273 + t}$$

where P is in mmHg and t is in degrees centigrade.

Humidity can also affect breakdown voltage



Polarity is very important in non-uniform asymmetrical gaps

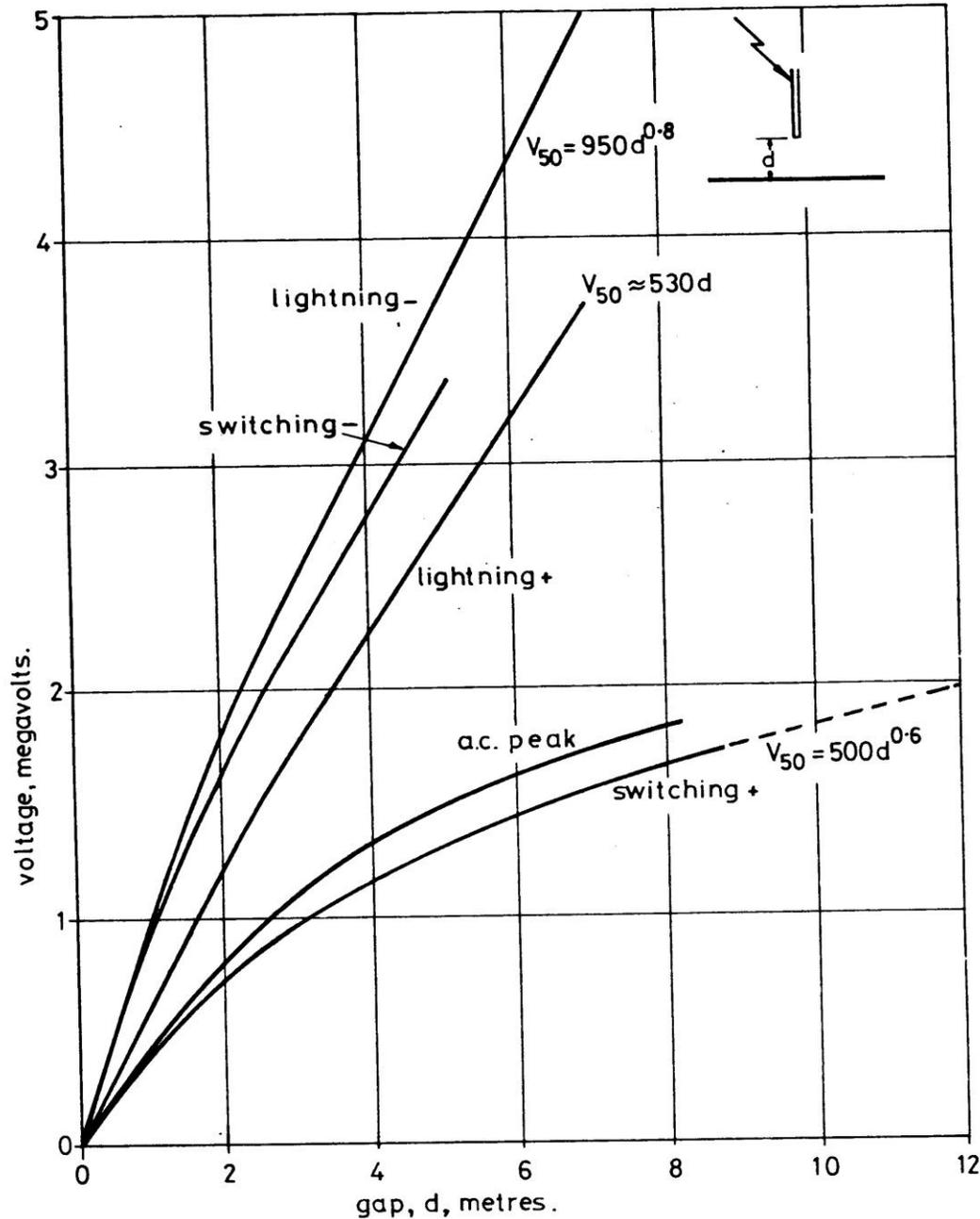


	Gap.		kg
1.	Rod-plane.		1.00
2.	Rod-structure.		1.05
3.	Conductor-plane.		1.15
4.	Conductor-window.		1.20
5.	Conductor-structure.		1.30
6.	Rod-rod (h=3m; under)		1.30
7.	Rod-rod (h=6m; under)		1.40
8.	Conductor-structure, (over & laterally)		1.39
9.	Conductor-crossarm end		1.55
10.	Conductor-rod (h=3m; under)		1.65
11.	Conductor-rod (h=6m; under)		1.90
12.	Conductor-rod (over)		1.90
13.	Conductor rod		1.40

“Rule of thumb”
breakdown voltage scaling
factors (K) for different
asymmetrical gap geometries

In asymmetric gaps the type of applied voltage is important:

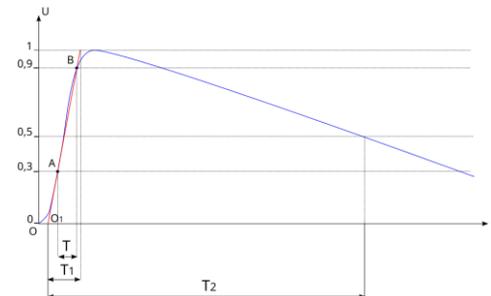
- Polarity
- DC
- AC (frequency)
- Pulsed (length)



“Standard impulses”

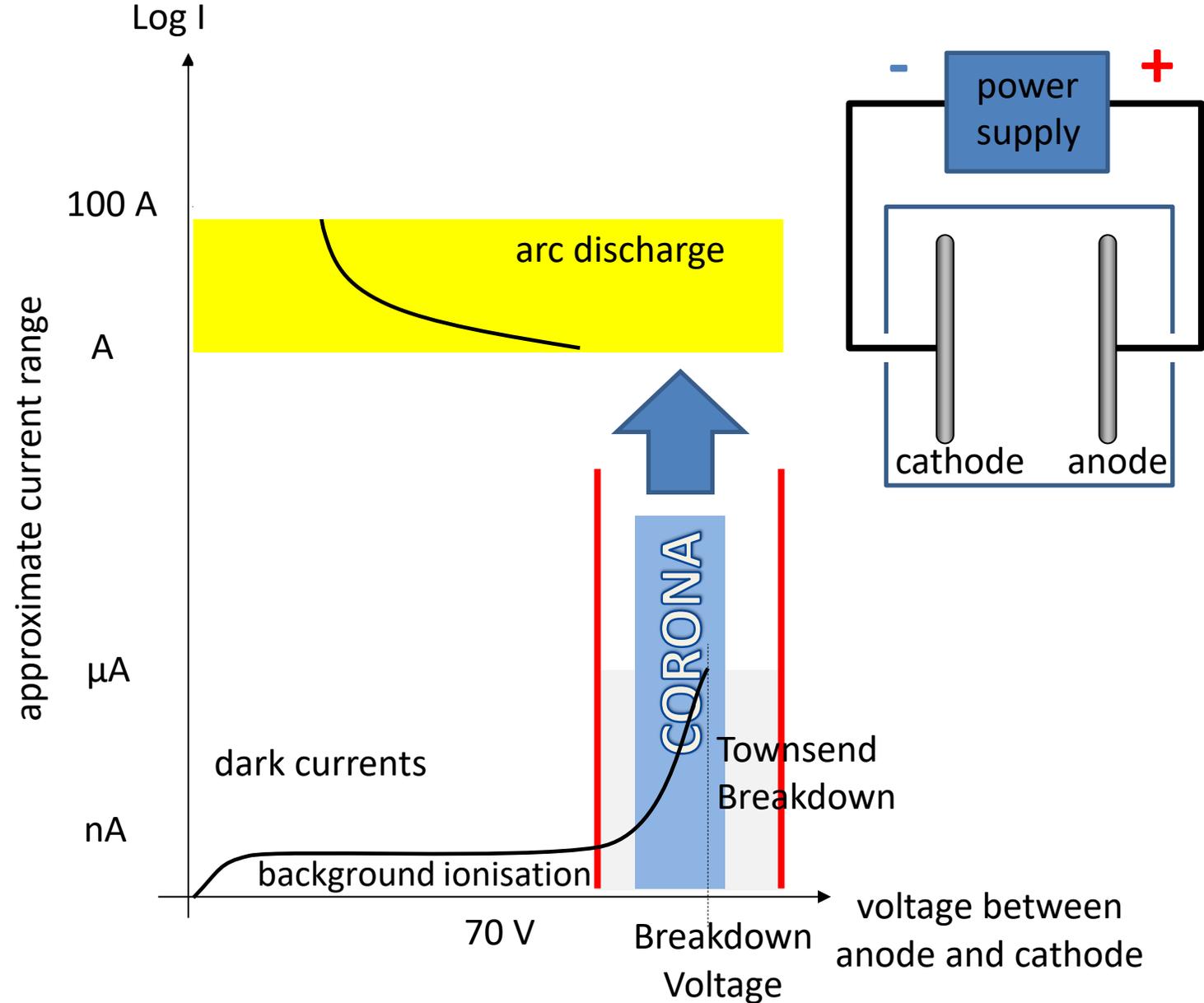
Lightning: 1.2/50 μ s

Switching: 250/2500 μ s



Electrical Discharges

Dependant on power supply and what is between electrodes



Arcs



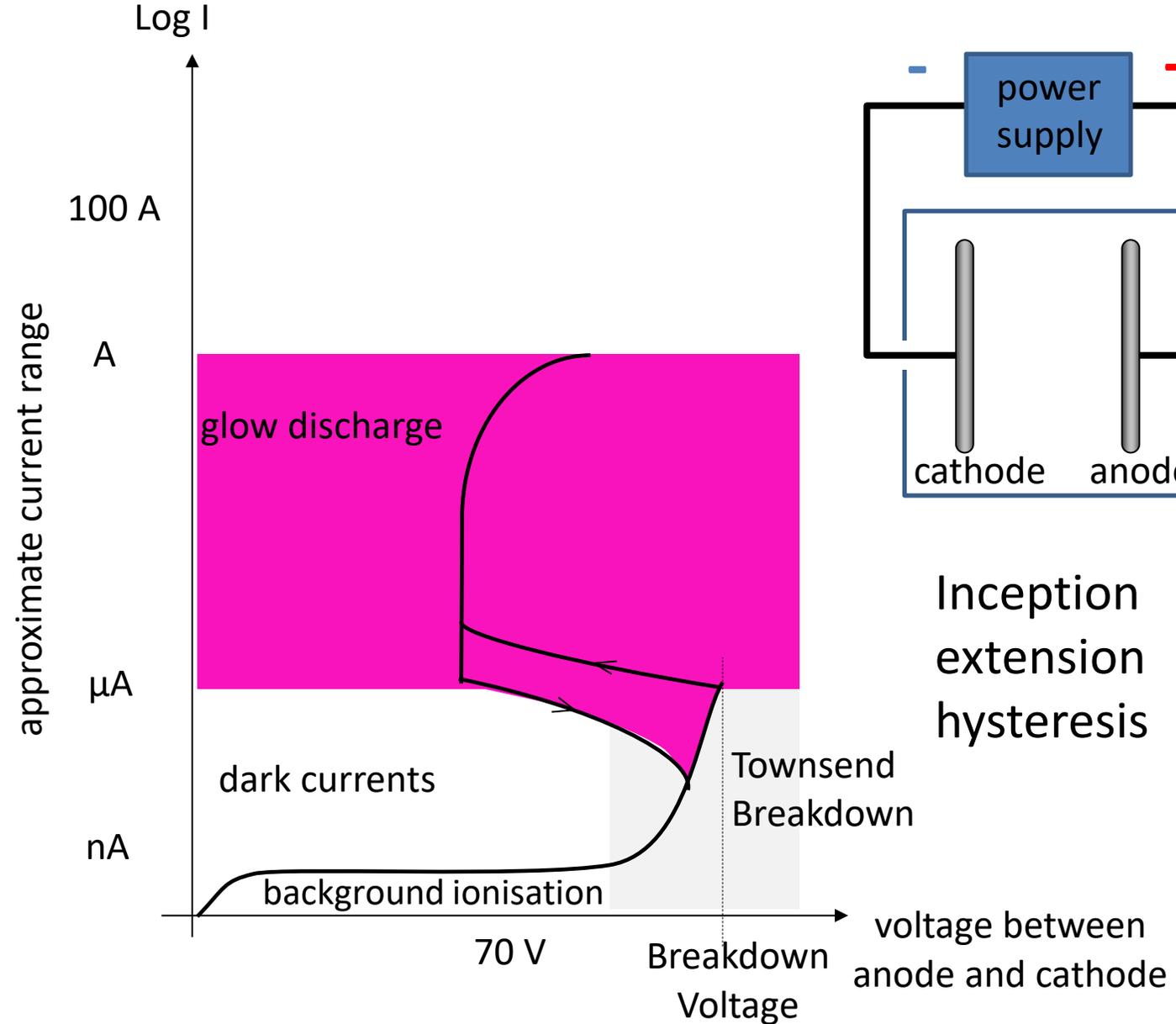
Bad

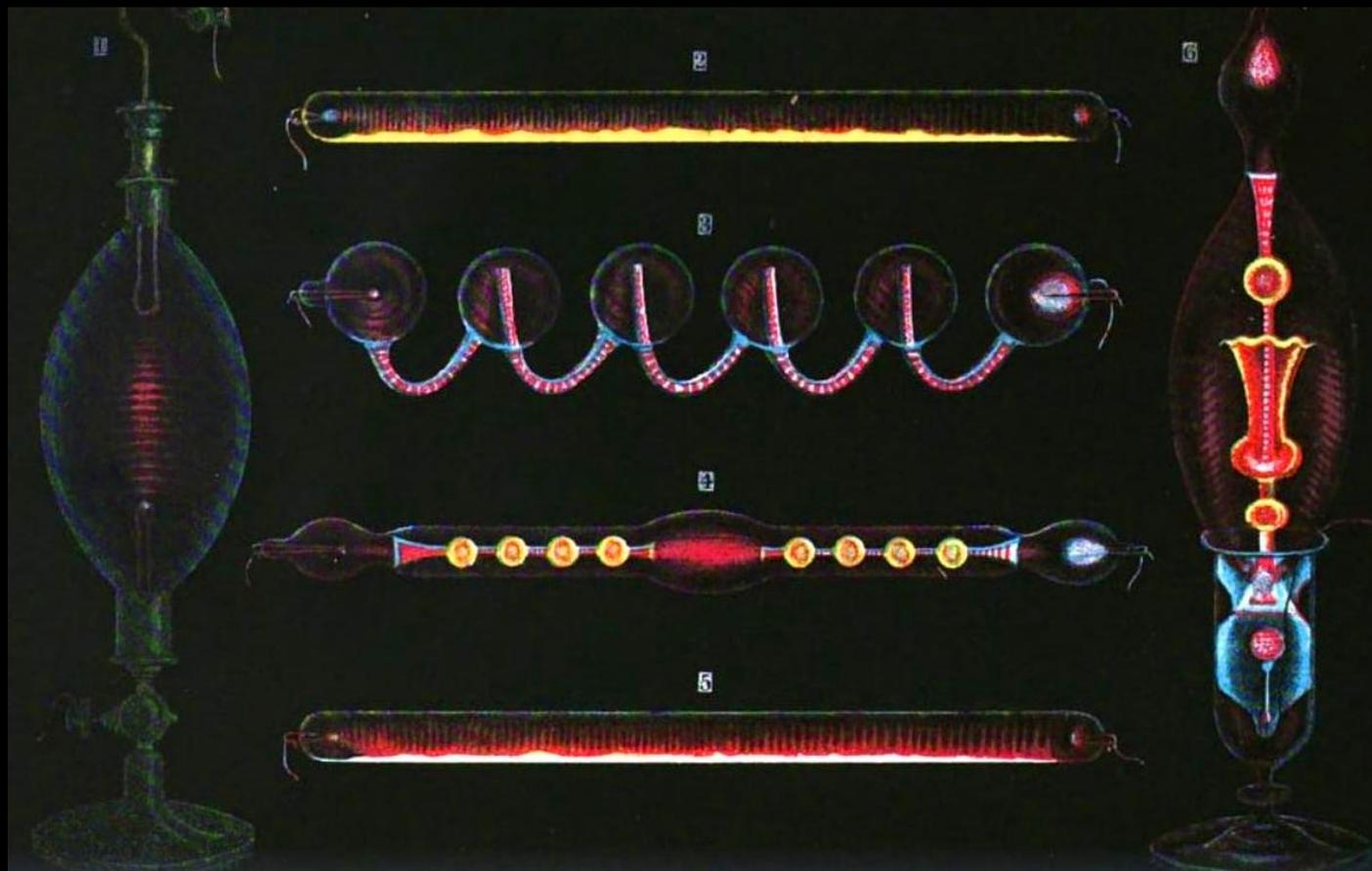


Good

Electrical Discharges

If the pressure is low enough





Basic Plasma Properties

Density, n

(per cm^3 or per m^3)

n_e = density of electrons

n_i = density of ions

n_n = density of neutrals

Charge State, q

$H^+ \rightarrow q = +1$

$Pb^{3+} \rightarrow q = +3$

$H^- \rightarrow q = -1$

Temperature, T (eV)

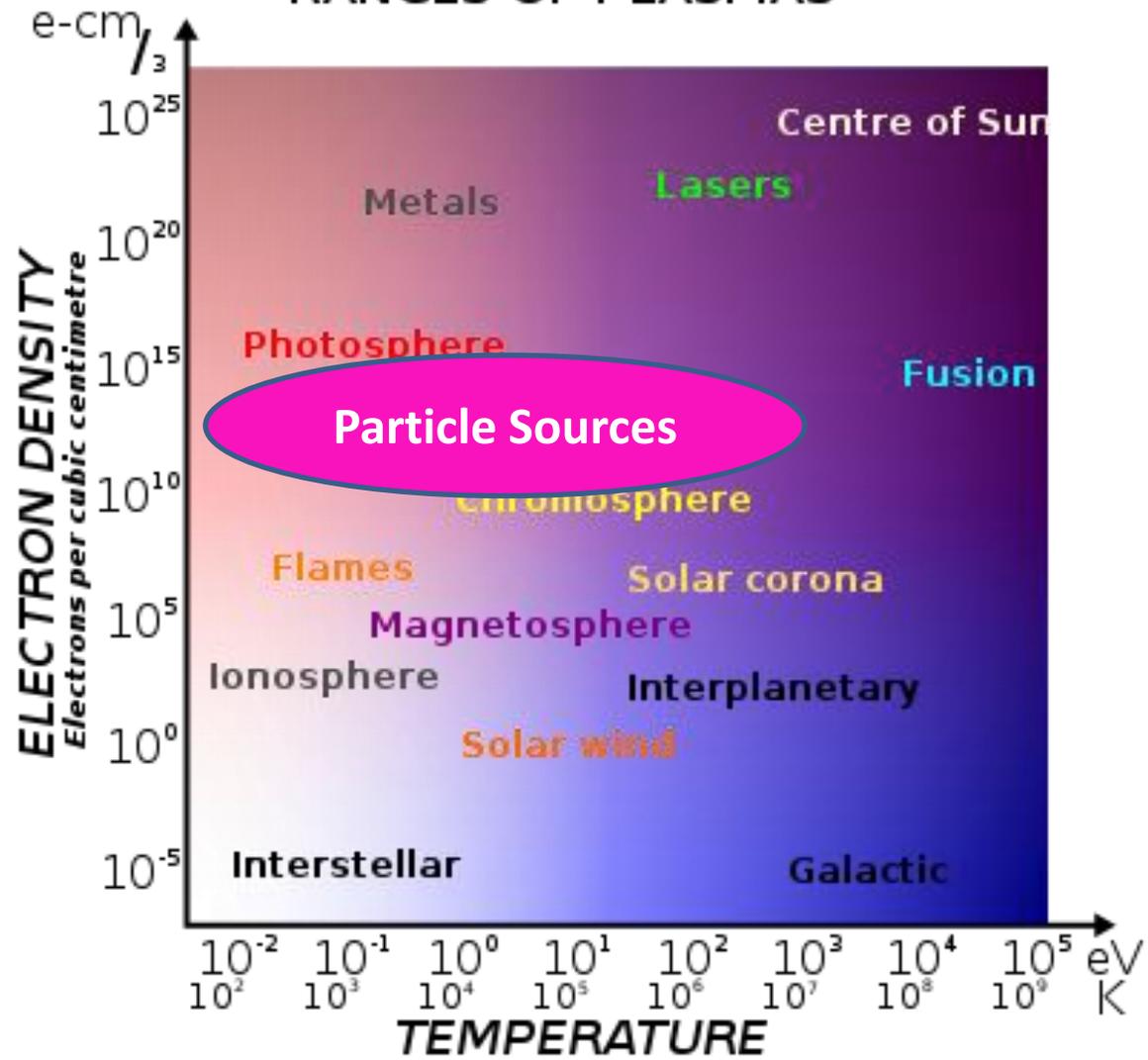
T_e = temperature of electrons

T_i = temperature of ions

T_n = temperature of neutrals

11600°K = 1 eV

RANGES OF PLASMAS

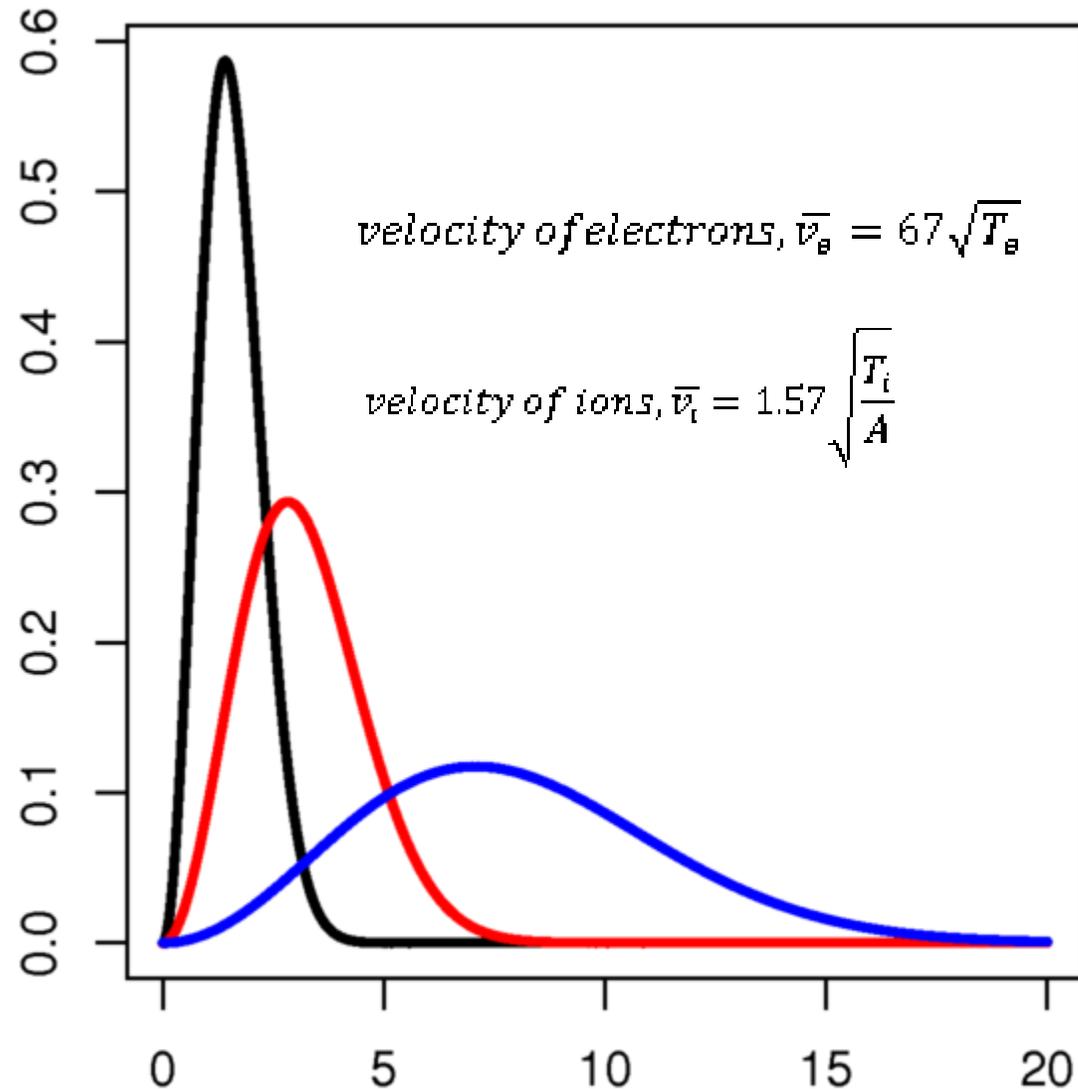


Temperature Distribution

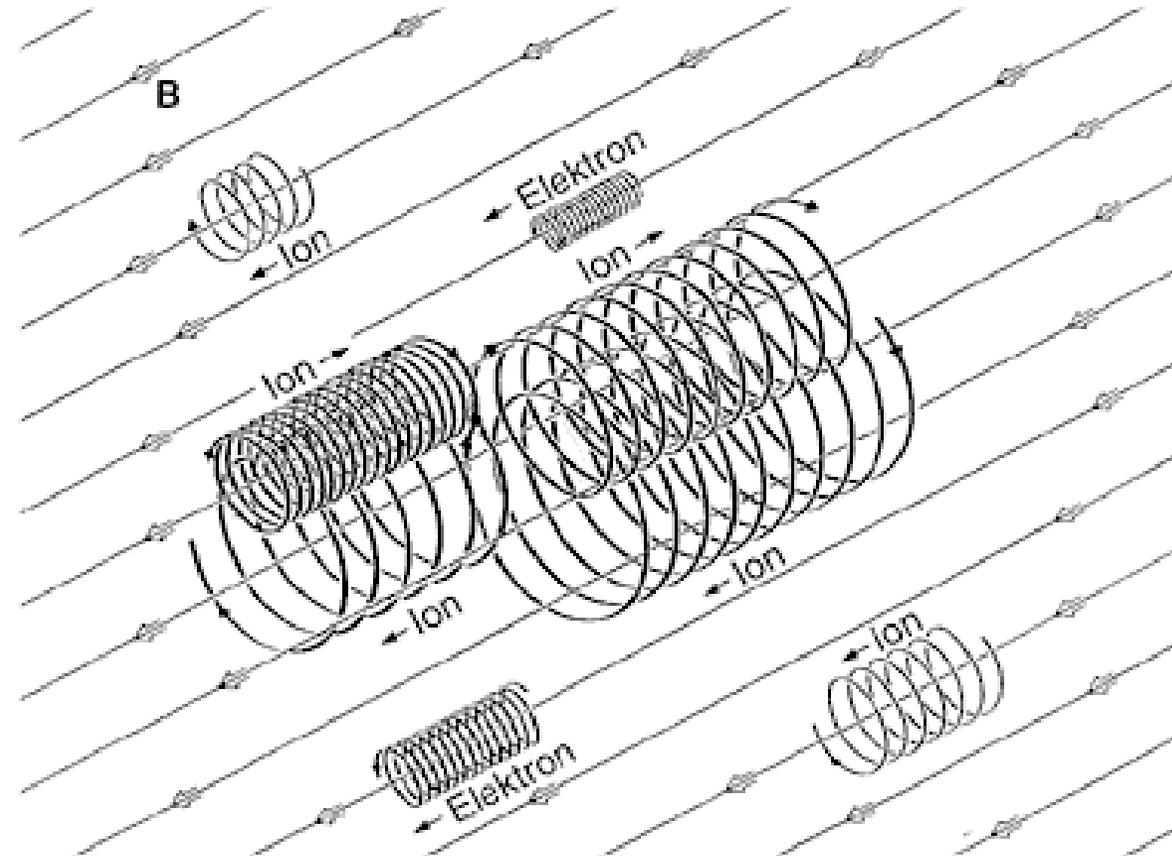
Maxwell Boltzmann
statistics

In magnetic fields:

$$v_x \neq v_y \neq v_z$$

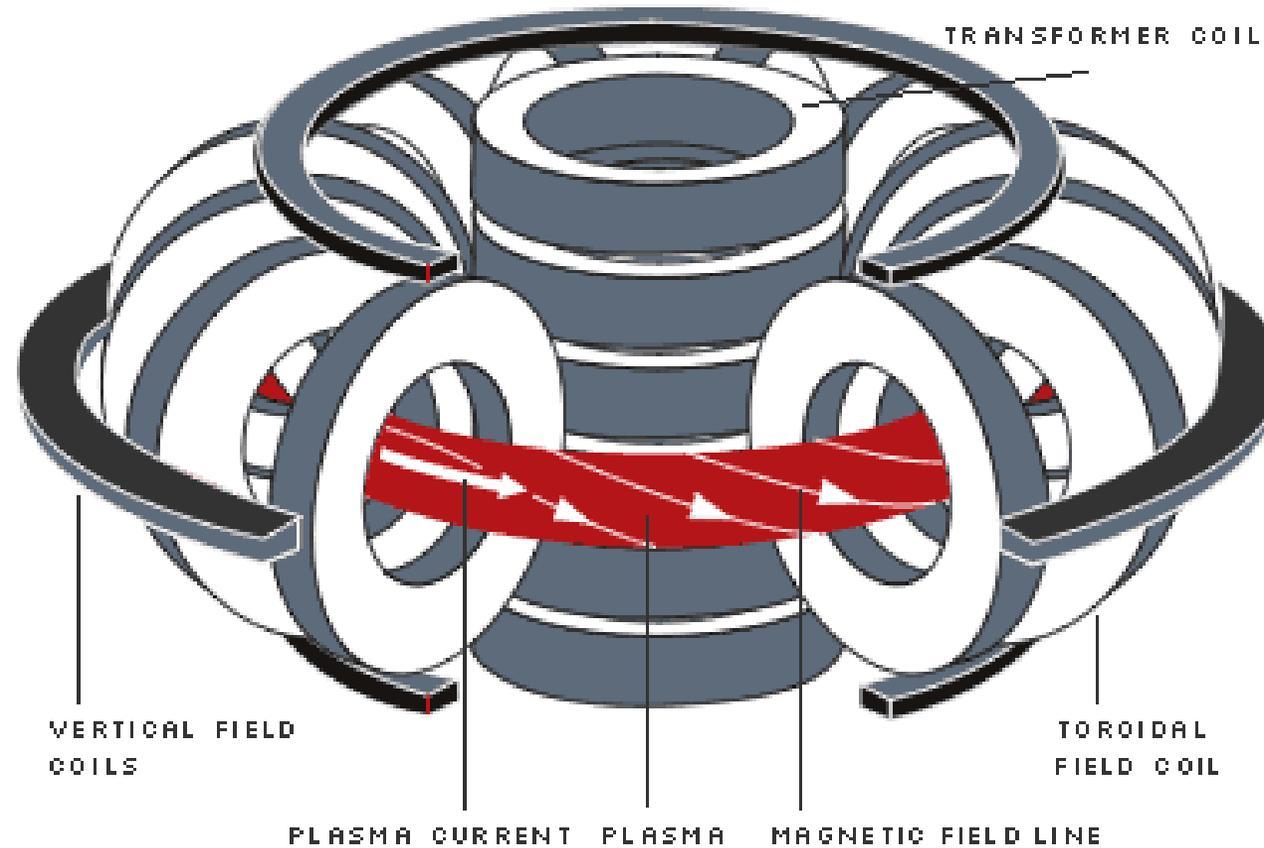


Magnetic Confinement

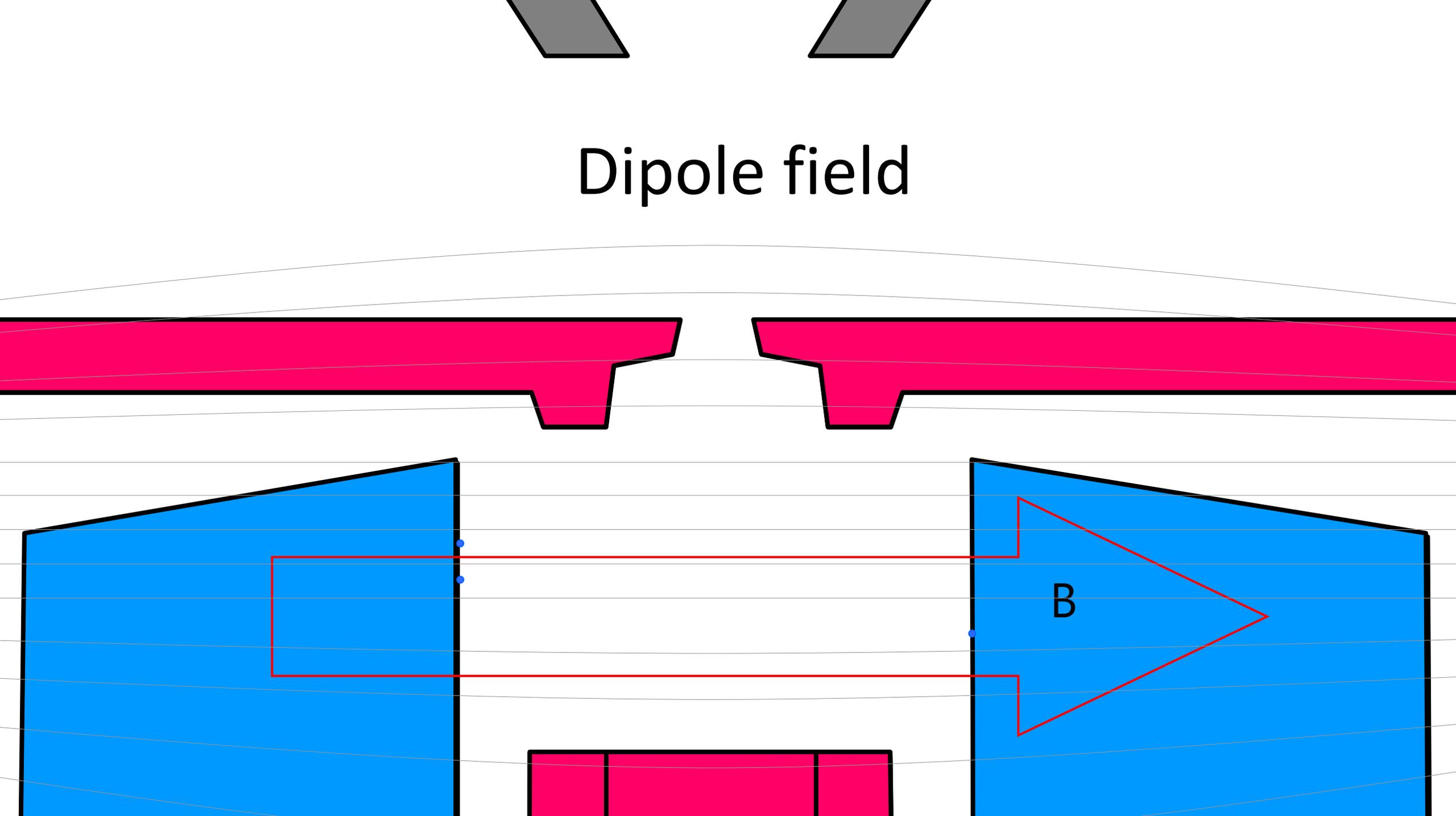


Particles spiral along magnetic field lines

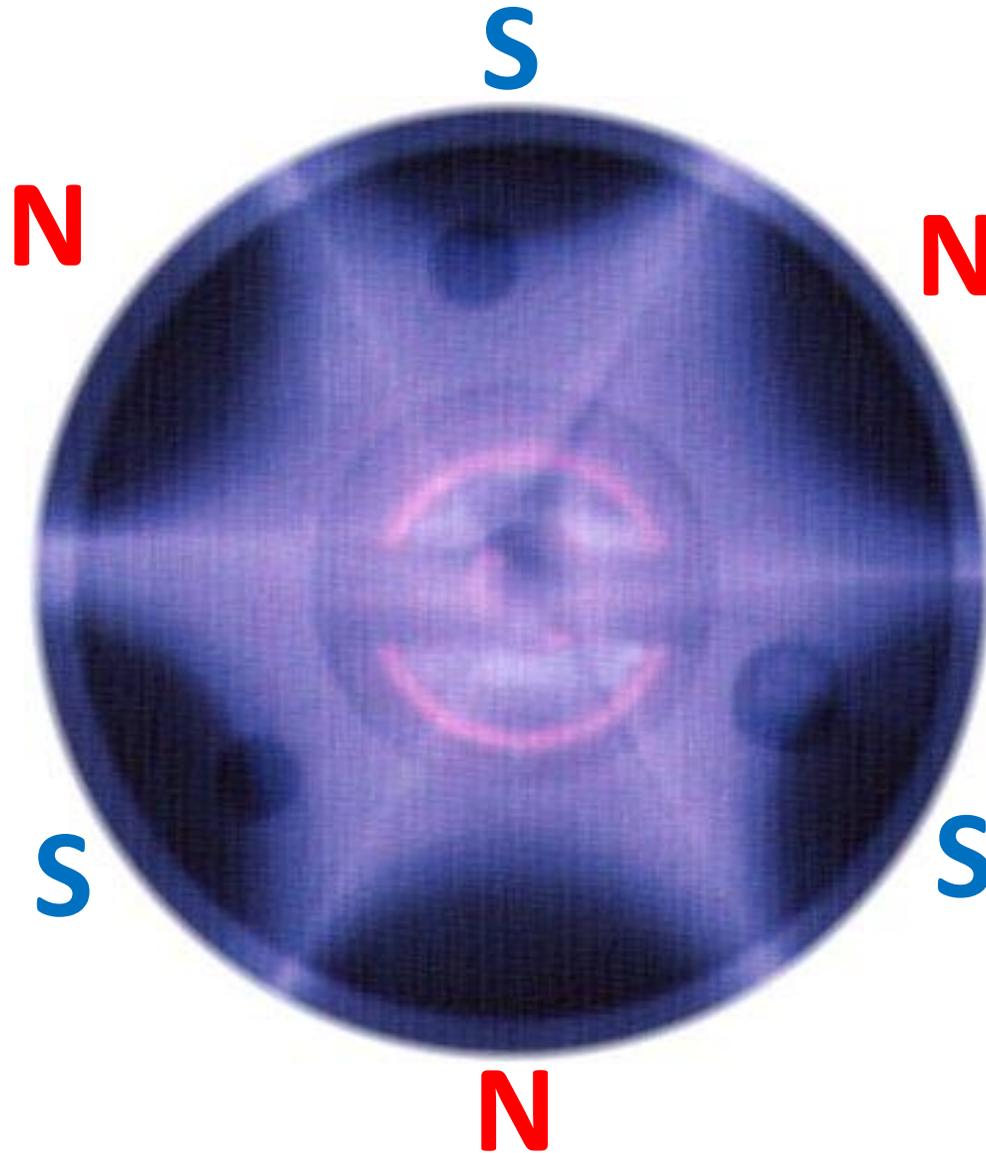
Solenoid field



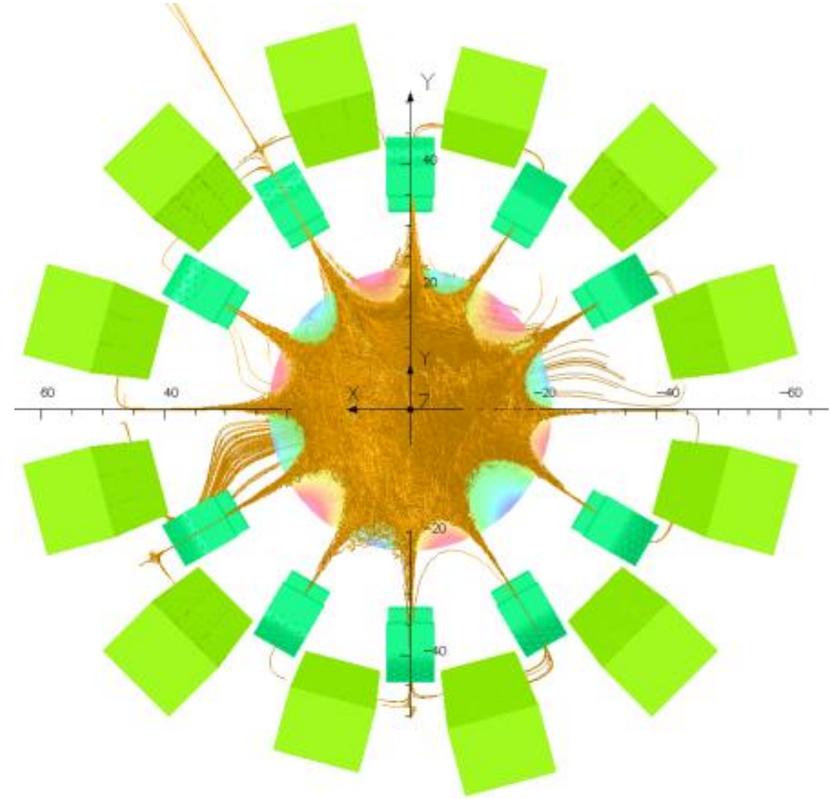
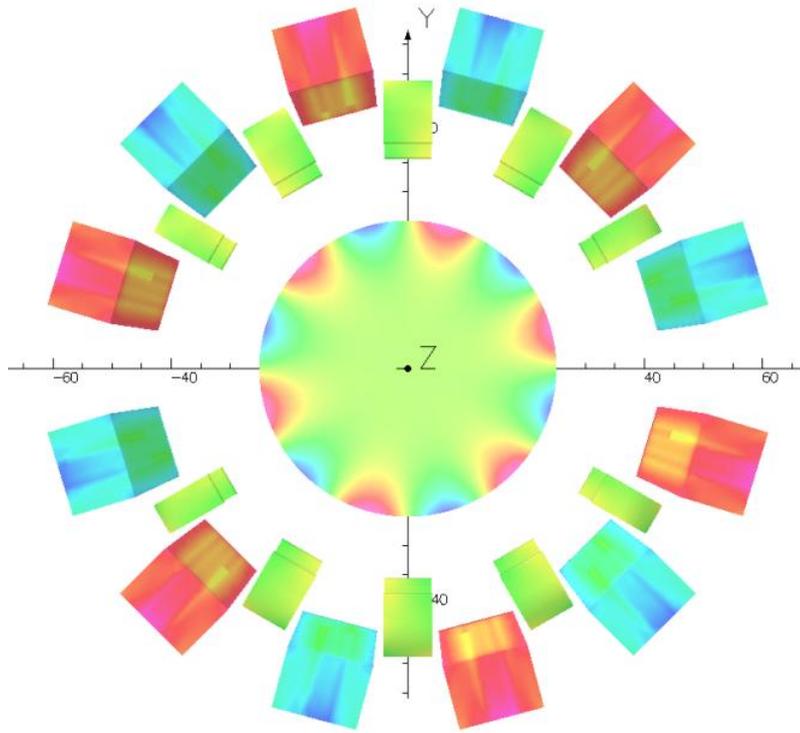
Dipole field



Hexapole



Multicusp Confinement



Percentage Ionisation

$$\frac{n_i}{n_i + n_n}$$

> 10 % → Highly Ionised

< 1 % → Weakly Ionised

Quasi Neutrality

$$\sum q_i n_i = n_e$$

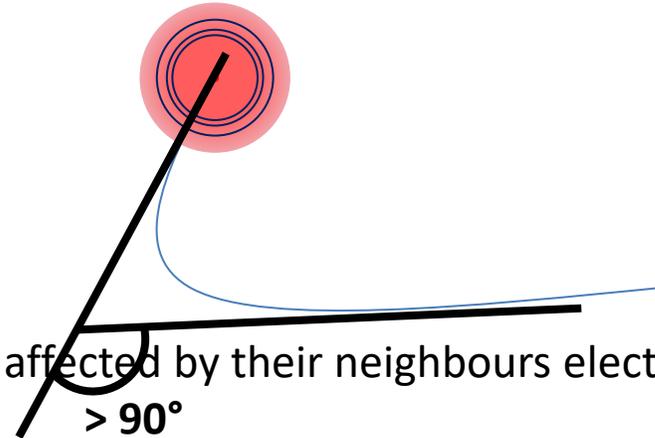
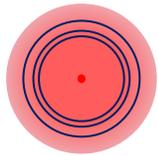
Collisions

e-

Concept of mean free path does not work in a plasma

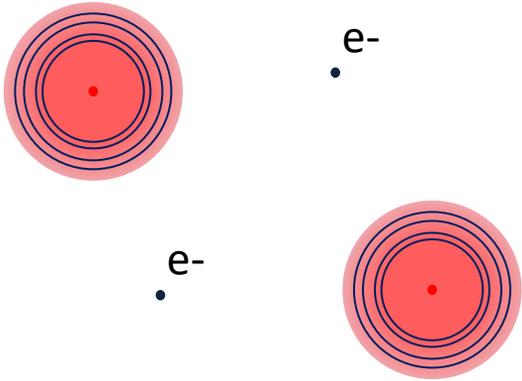
The average time it takes for a particle to be deflected by 90°

Charged particle trajectories are constantly affected by their neighbours electric fields



e-
Relaxation time = 90° deflection time

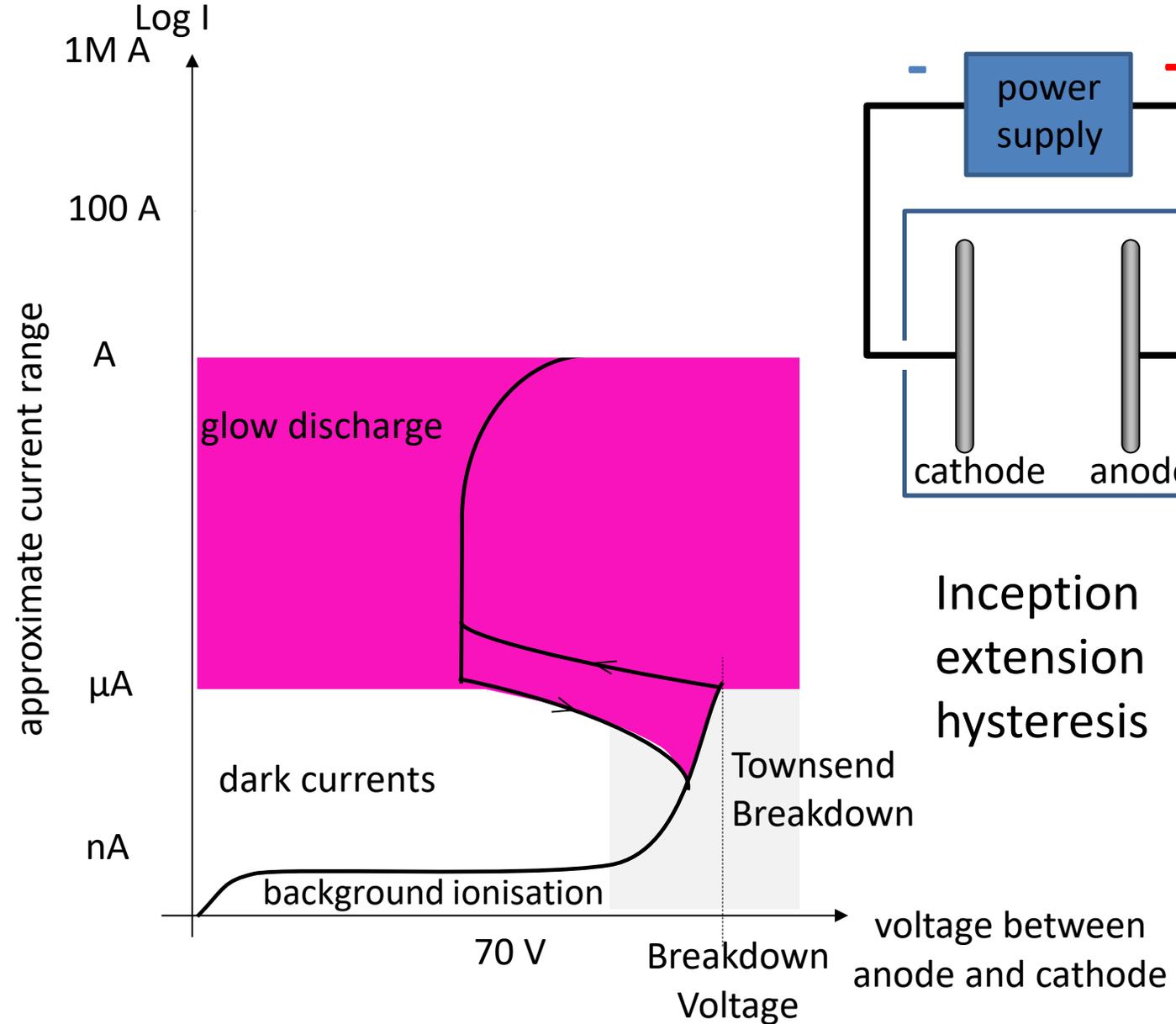
Debye Length



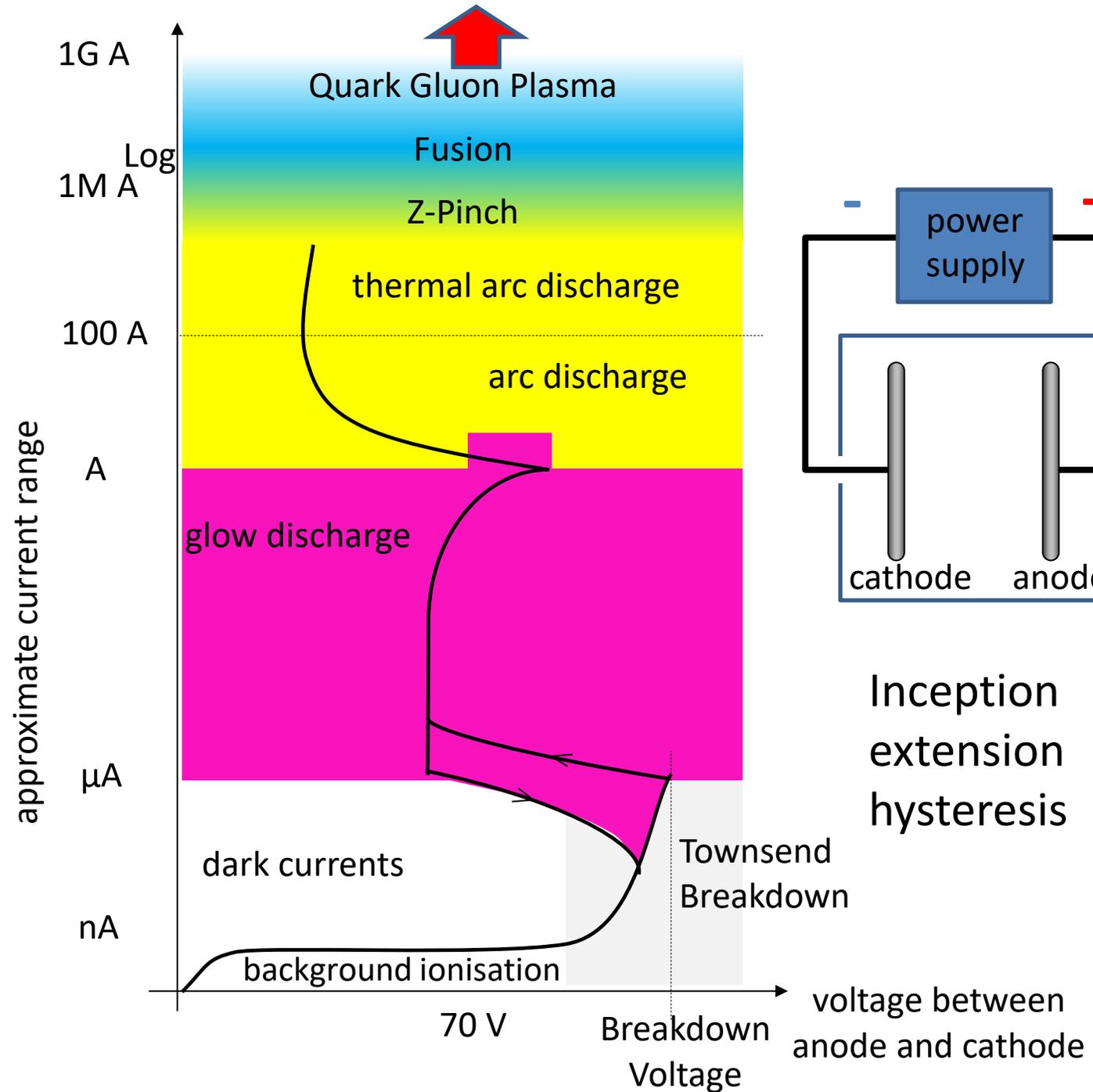
$$\lambda_D = \sqrt{\frac{\epsilon_0 k T_e}{n_e q_e^2}}$$

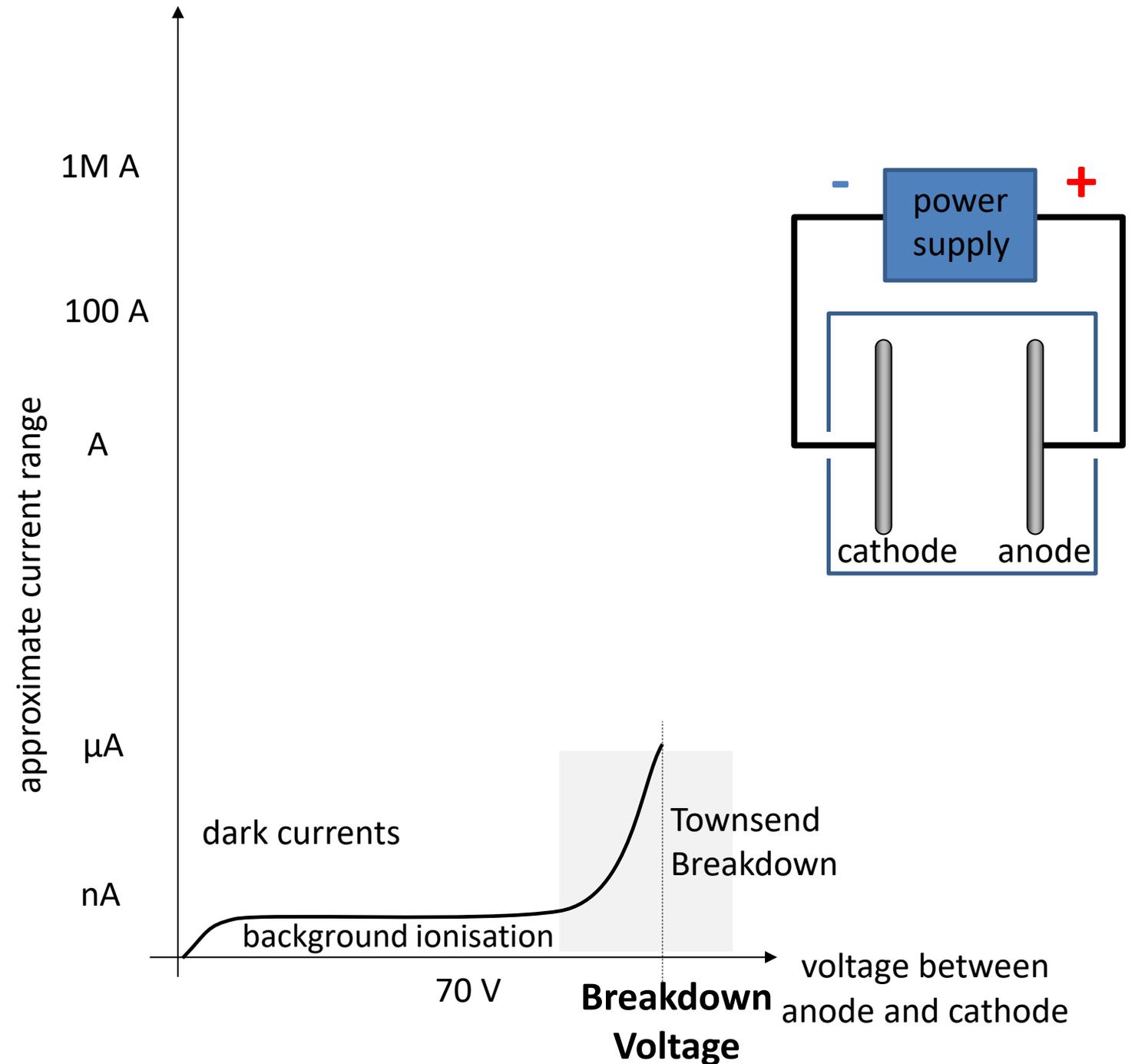
Electrical Discharges

If the pressure is low enough



If the pressure is low enough





Breakdown strength of Air

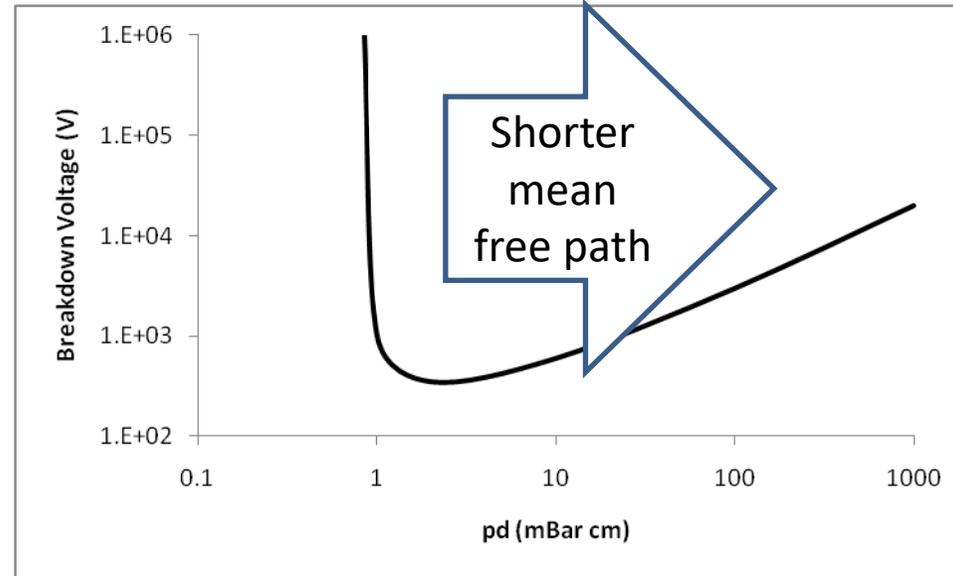
In air at normal room conditions two electrodes require about 30 kV for each cm of spacing to breakdown (as a rule of thumb)

Or 3 kVmm^{-1}

Paschen Curve



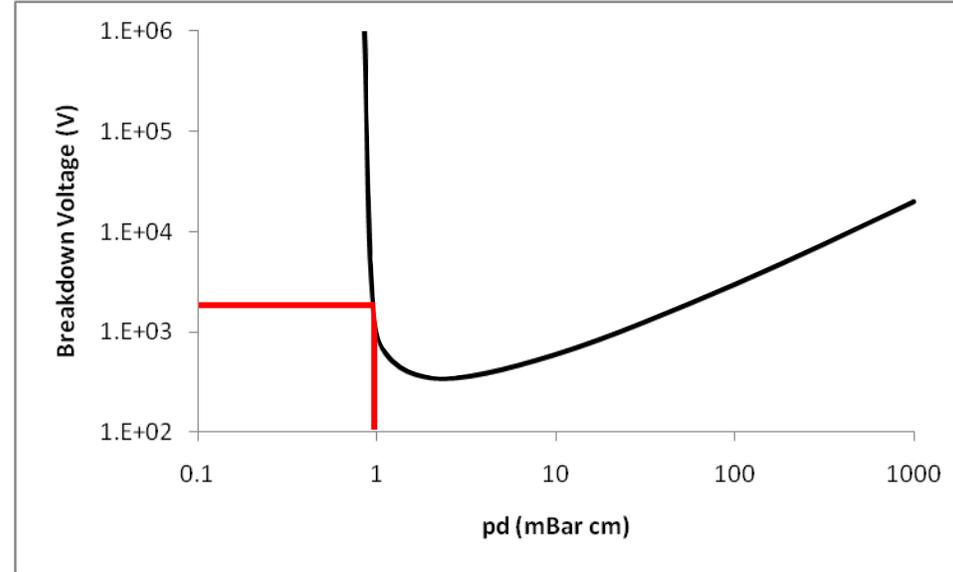
Friedrich Paschen 1889



Paschen Curve



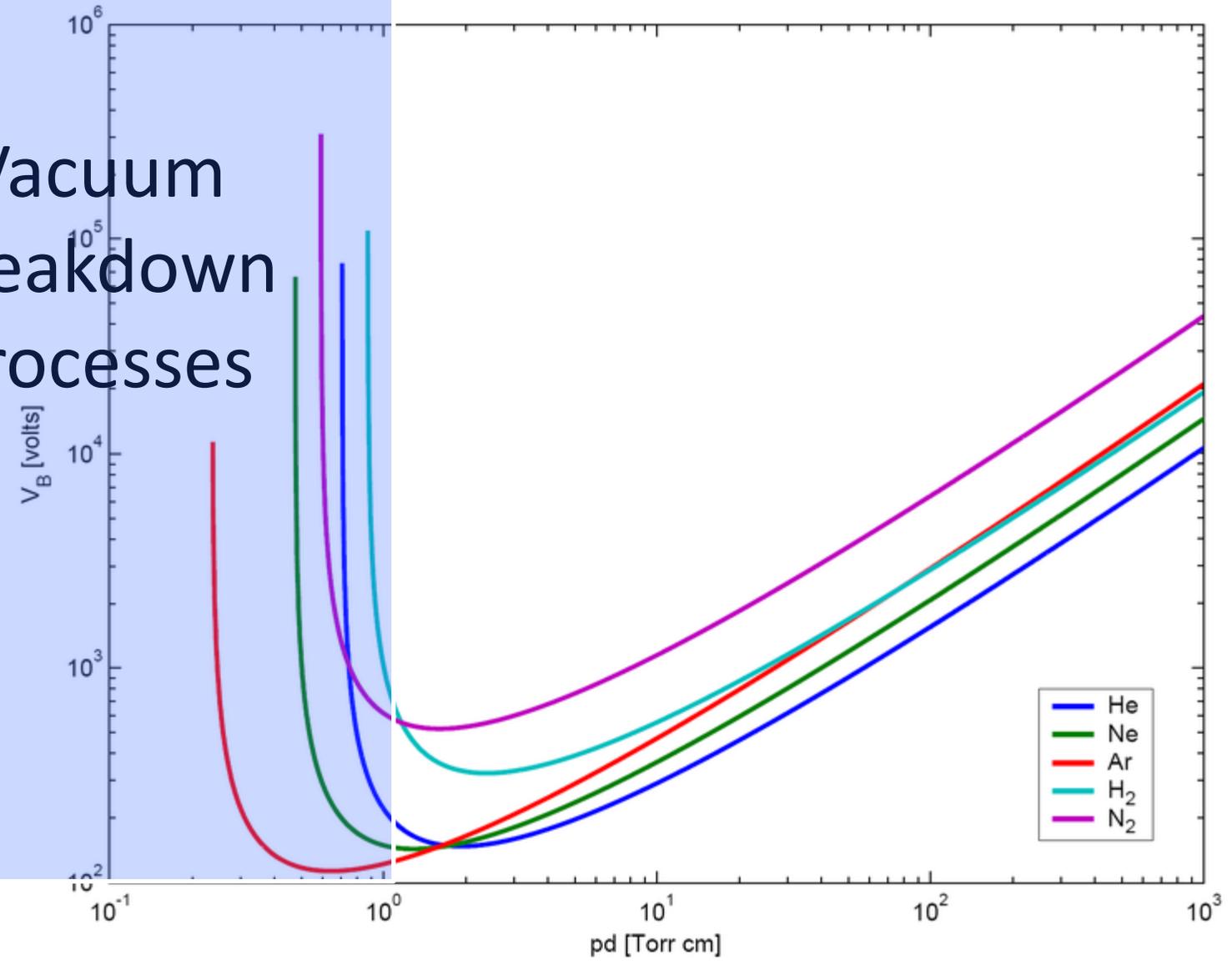
Friedrich Paschen 1889



Operating just below the Paschen Minimum:

Longer gaps have
lower breakdown voltages!

Vacuum Breakdown Processes

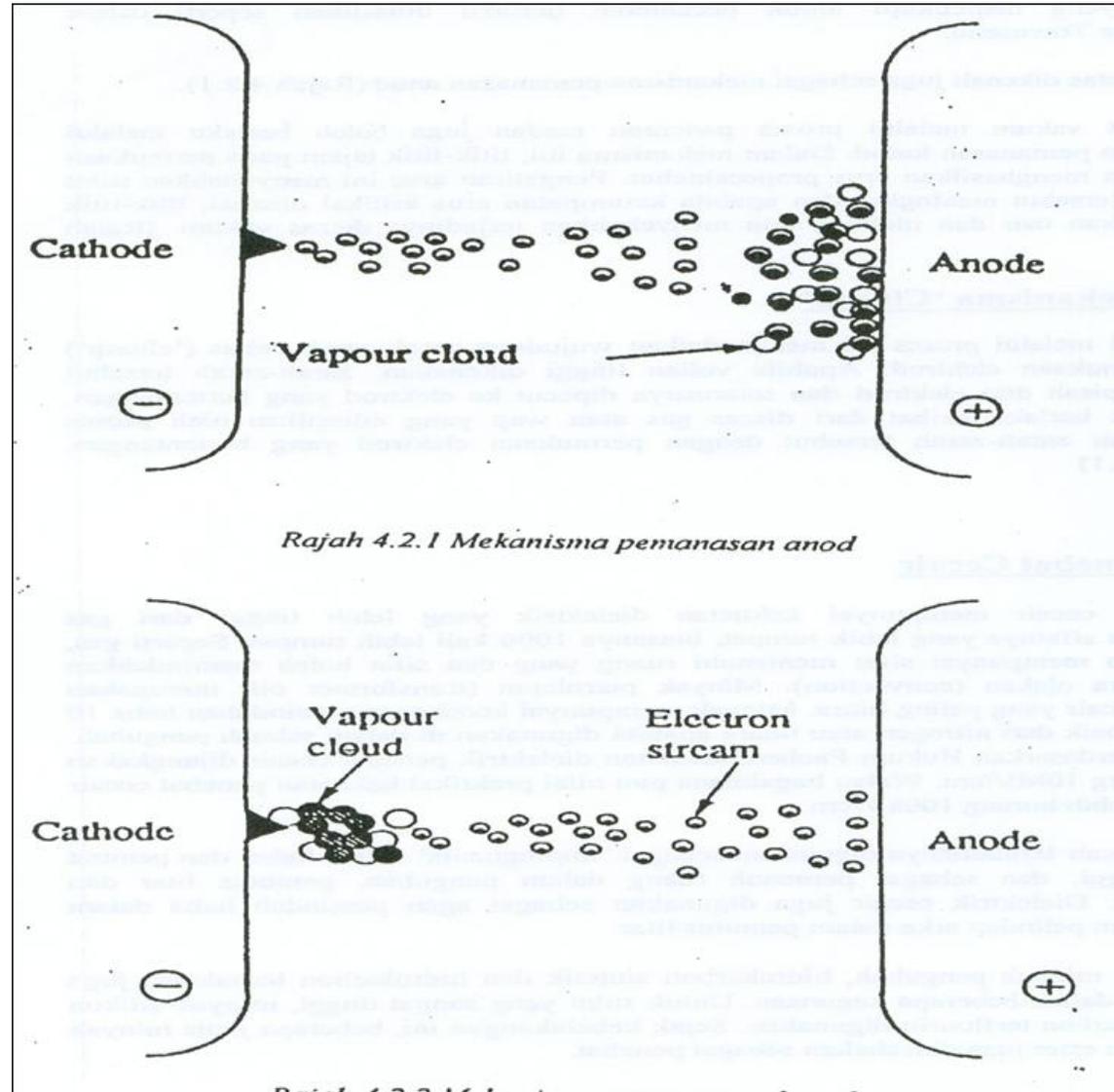


Vacuum Breakdown

Where do the charge carriers come from?

Insulating micro-inclusions can also cause field enhancement

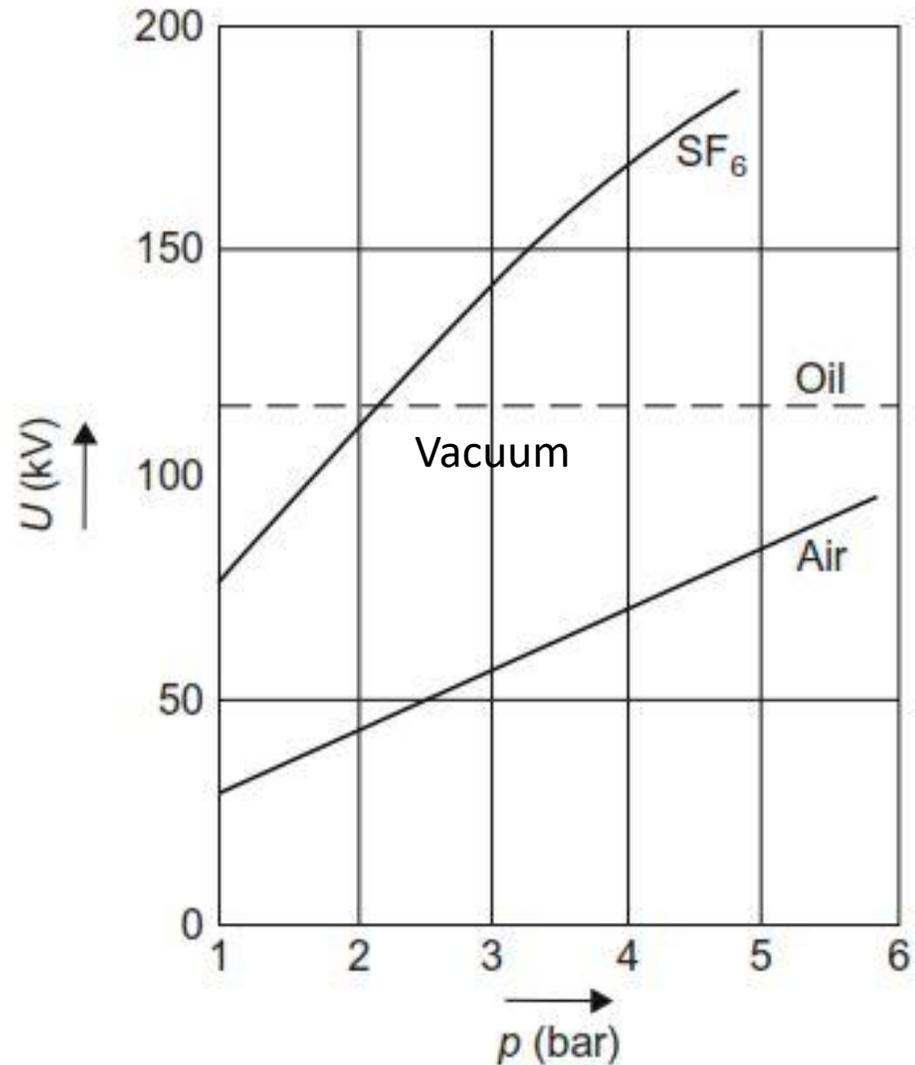
Conducting particles from cathode



Conducting particles from anode

If the timing is right (wrong!) alternating applied voltage can cause multipactoring in RF systems- A resonant electron breakdown!

What about other insulating media?

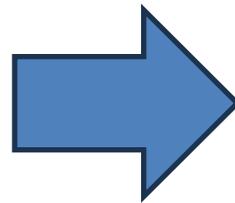


- Sulfur hexafluoride (SF_6)
- Oil

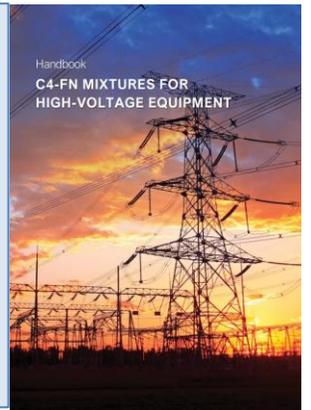
Sulfur hexafluoride (SF₆)



SF₆ is the most potent greenhouse gas:
1 kg SF₆ “lost” = 23 tonnes of CO₂
stays in the atmosphere for 3,200 years



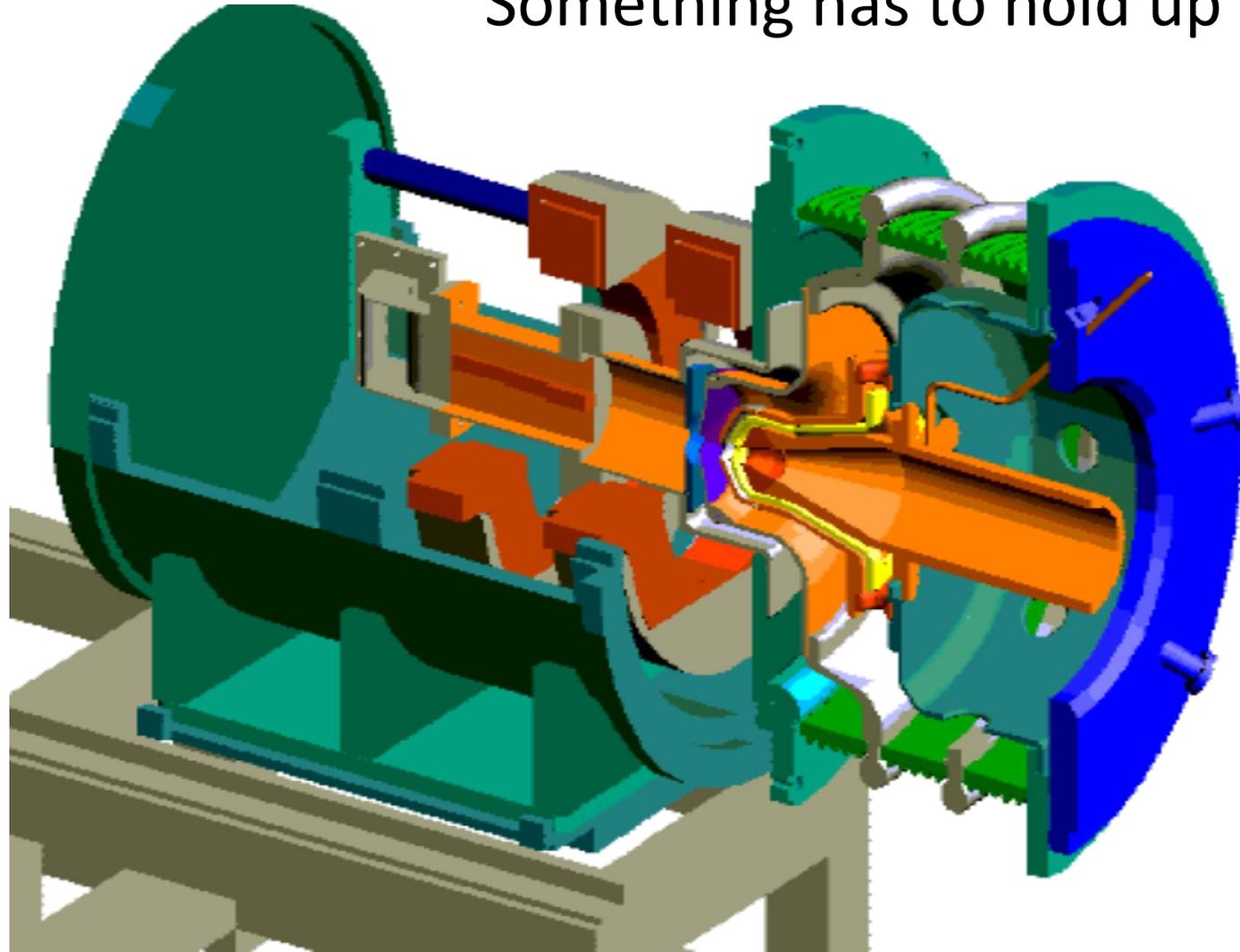
A possible solution is to modify the system to use a modern alternative
e.g.
C4-FN (fluronitrile) mixture
(O₂ / CO₂ / N₂)



GE and Hitachi

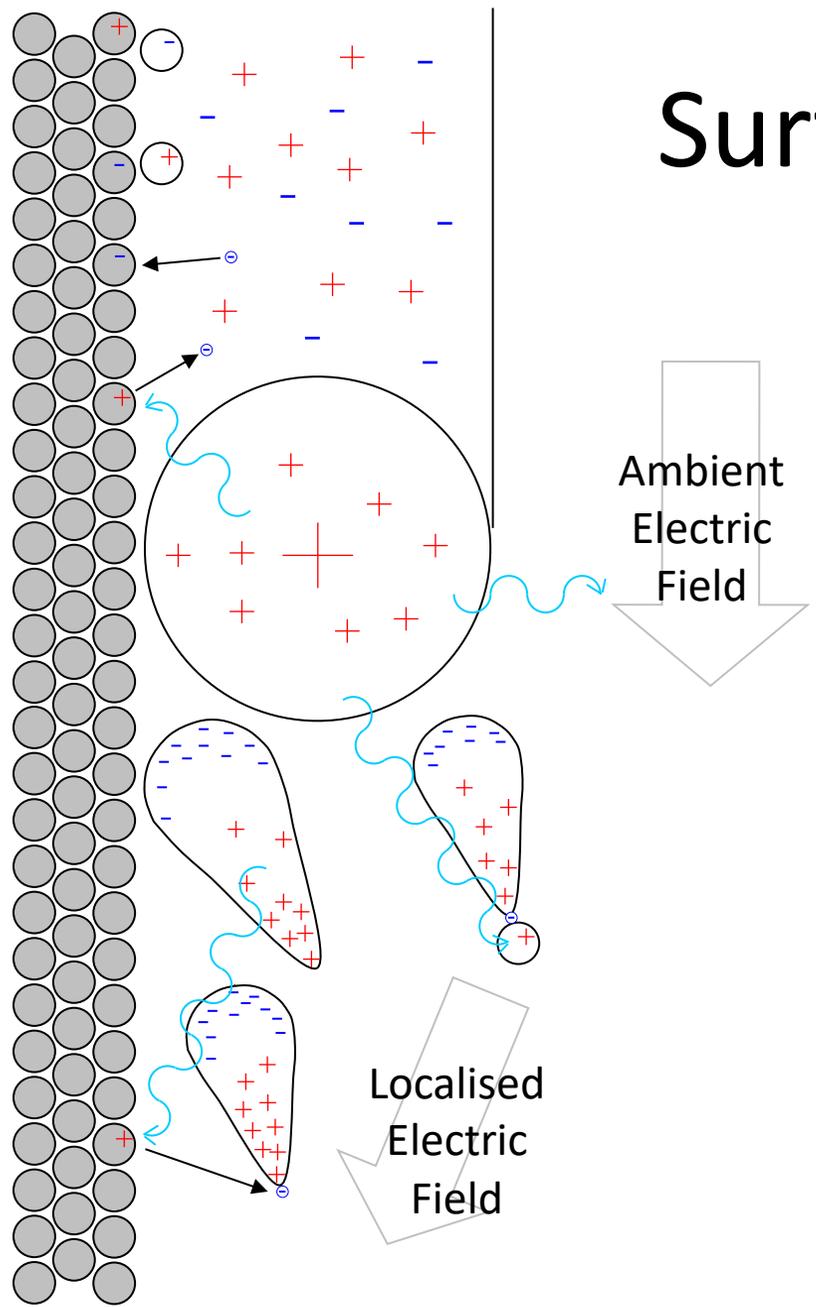
Insulators

Something has to hold up the electrodes!



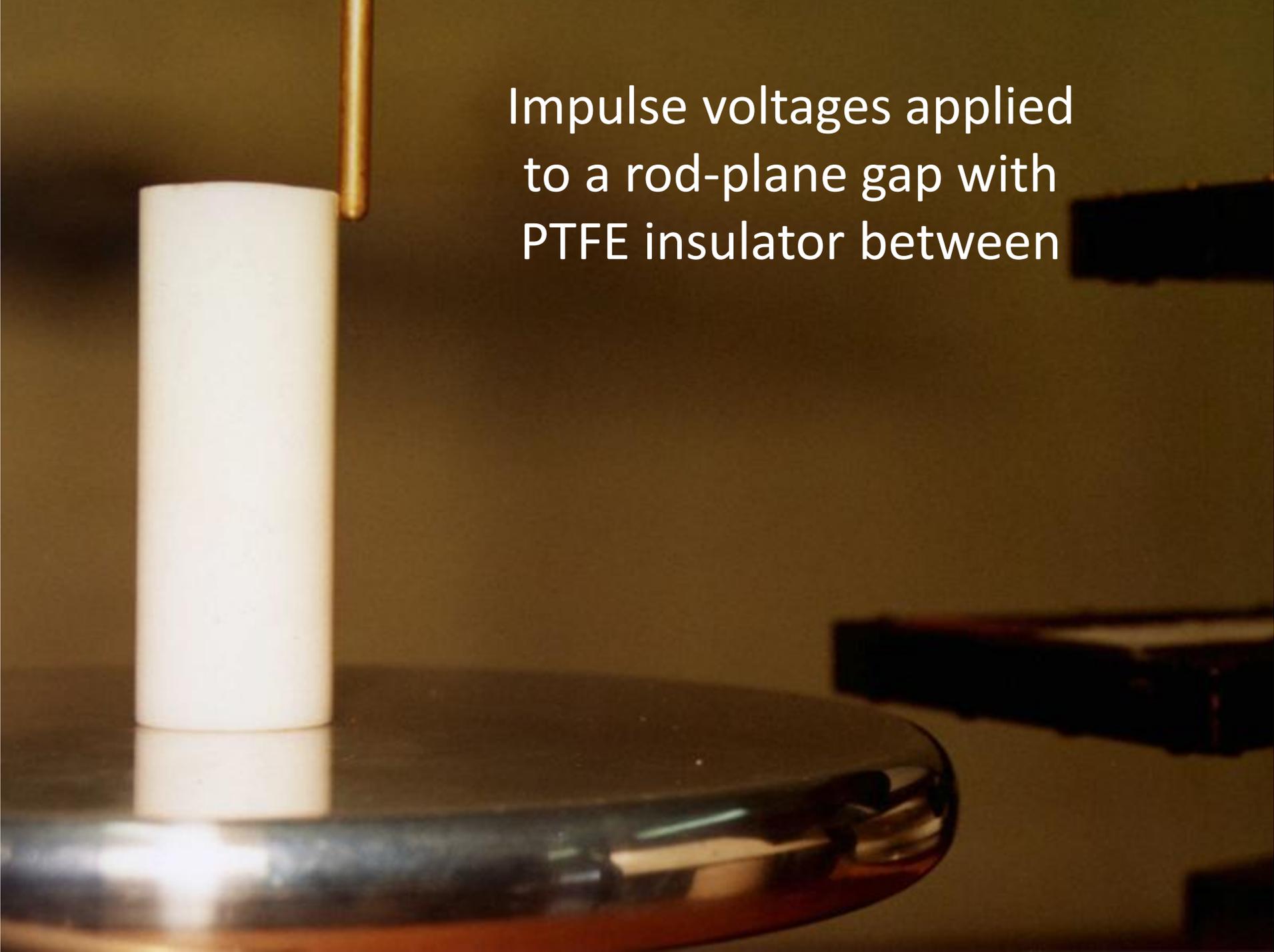
Surface Breakdown

Insulator surfaces are the weakest part of the insulation system

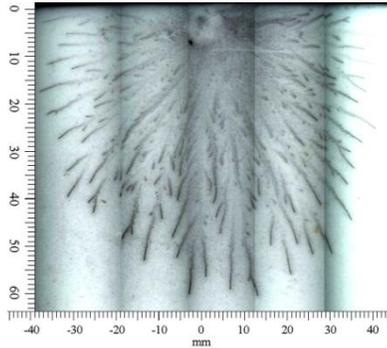


- Electrons
- ~ Photons
- Neutral Gas Molecules
- Neutral Surface Molecules
- ⊕ Positive Ions (Gas Molecules)
- ⊖ Negative Ions (Gas Molecules)
- ⊕ Positive Ions (Surface Molecules)
- ⊖ Negative Ions (Surface Molecules)

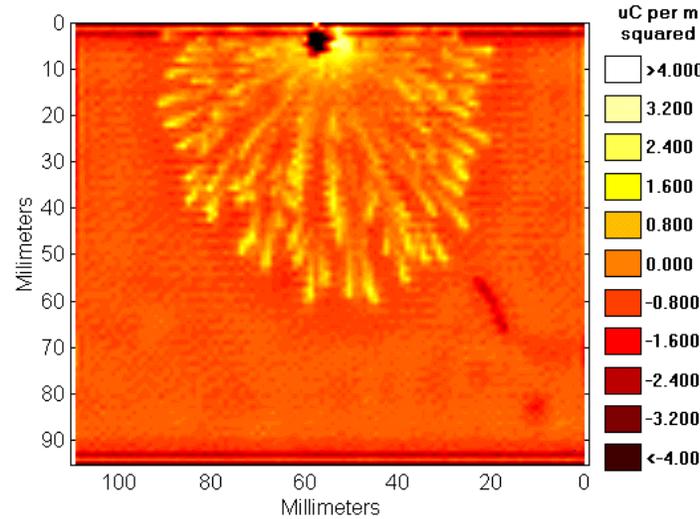
Impulse voltages applied
to a rod-plane gap with
PTFE insulator between



Surface Charging

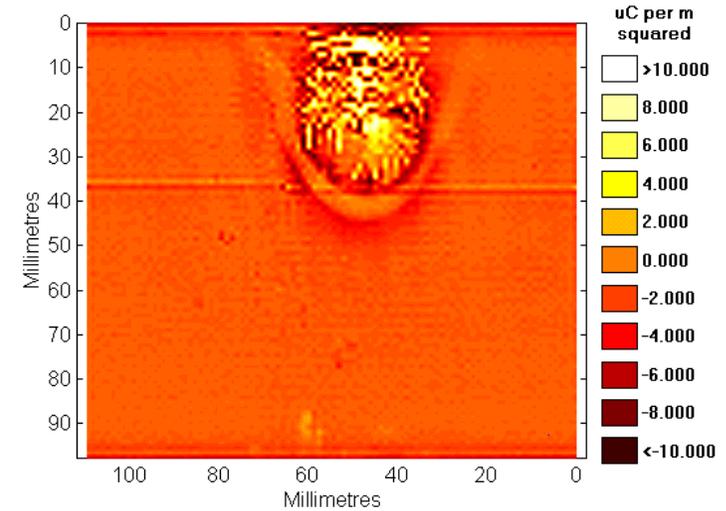


Dust Figure



Charge Distribution

+36 kV Impulse

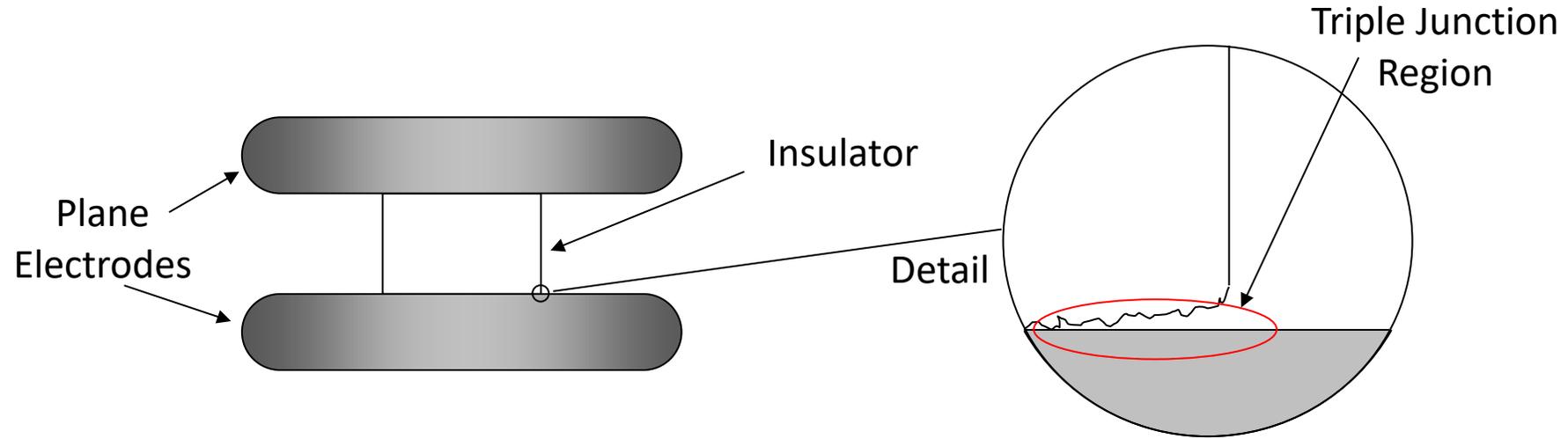


Charge Distribution

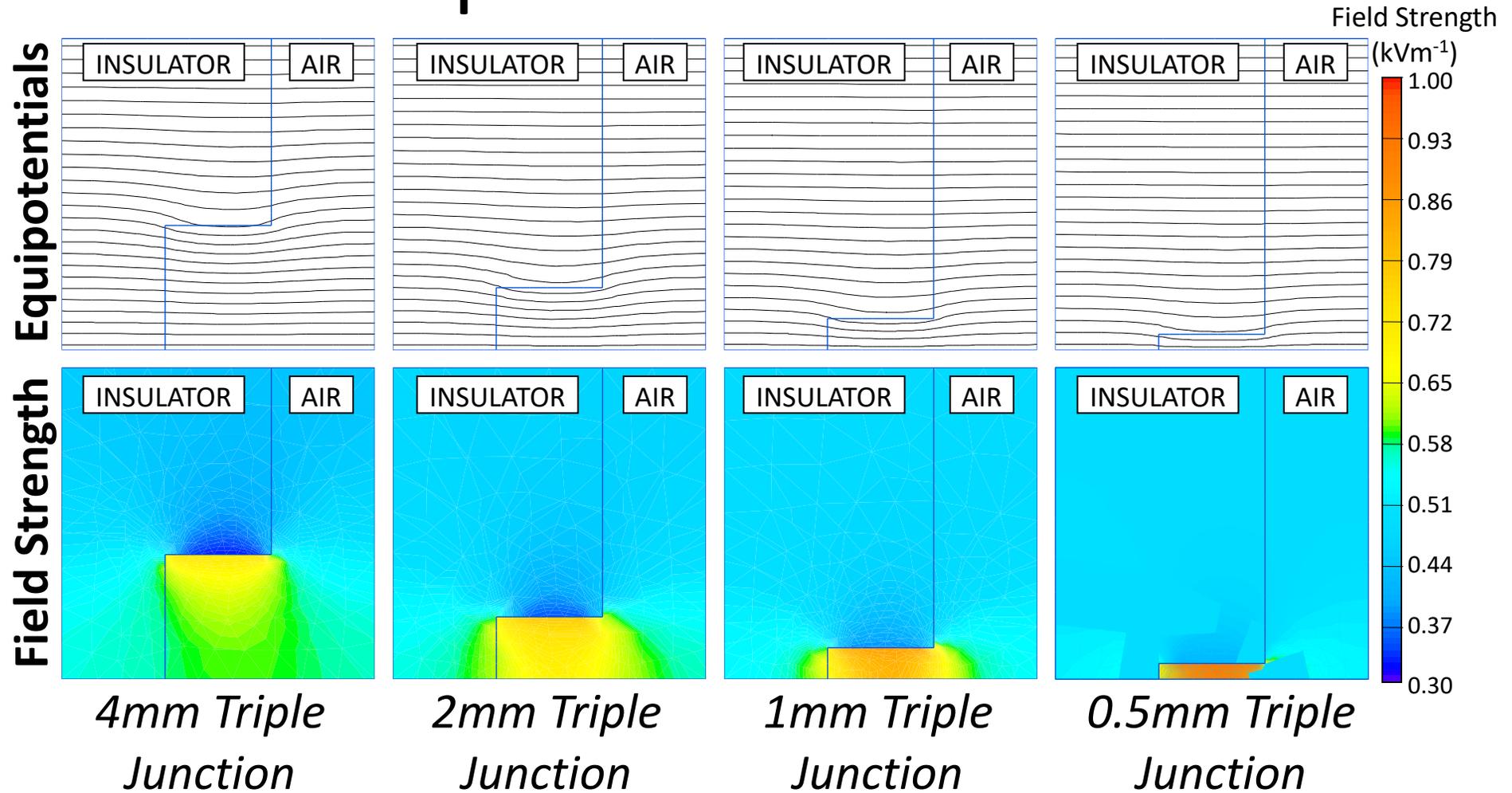
-70 kV Impulse

Polarity is very important if the gap is asymmetrical

Triple junctions always exist at some scale



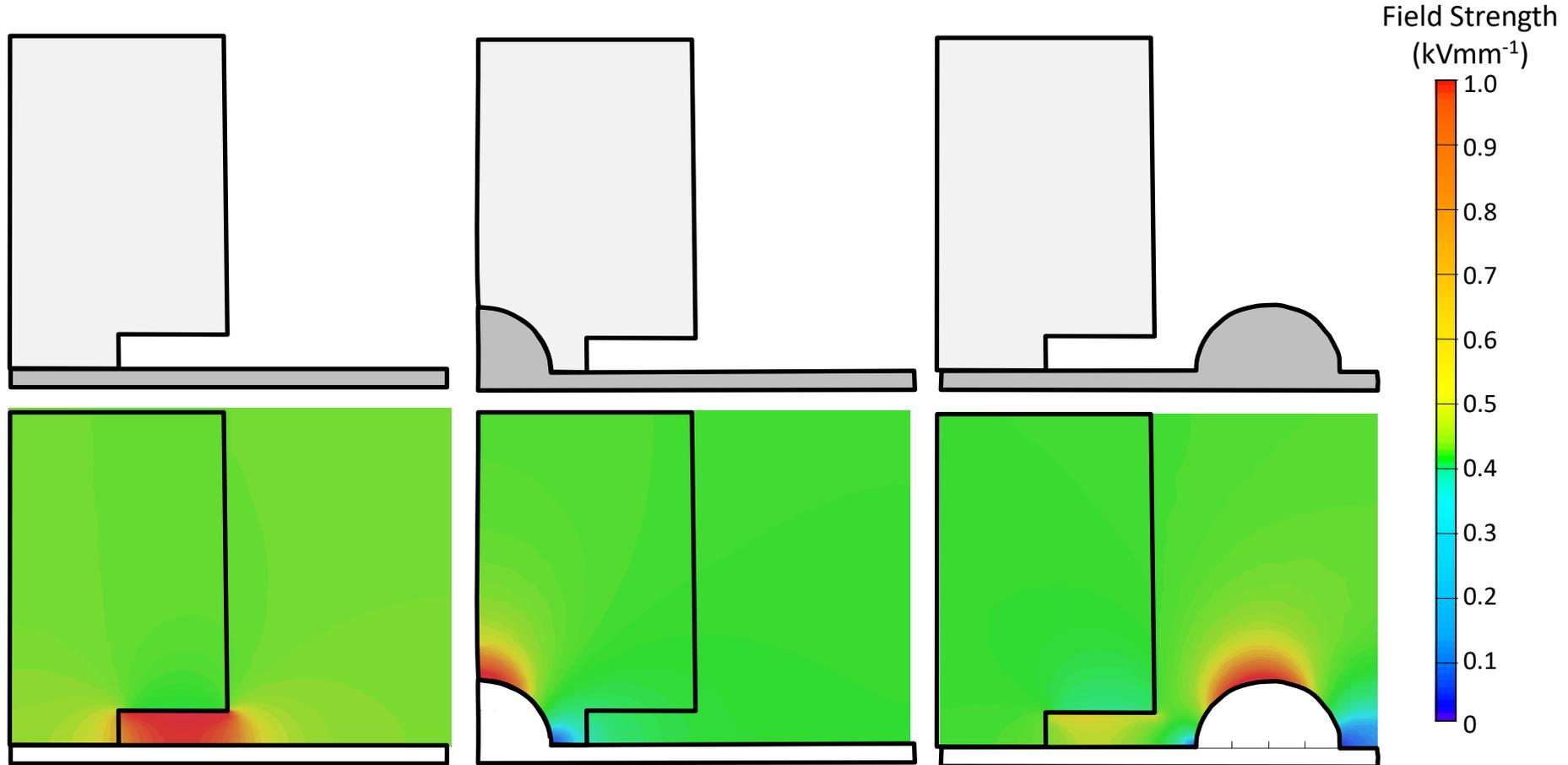
Triple Junction Effect



PTFE ($\epsilon_r = 2.2$) ambient field of 0.5 kVmm^{-1}

Triple Junction Screening

1 mm PTFE triple junction ambient field of 0.5 kVmm^{-1}



No Screening

Inside
Insulator

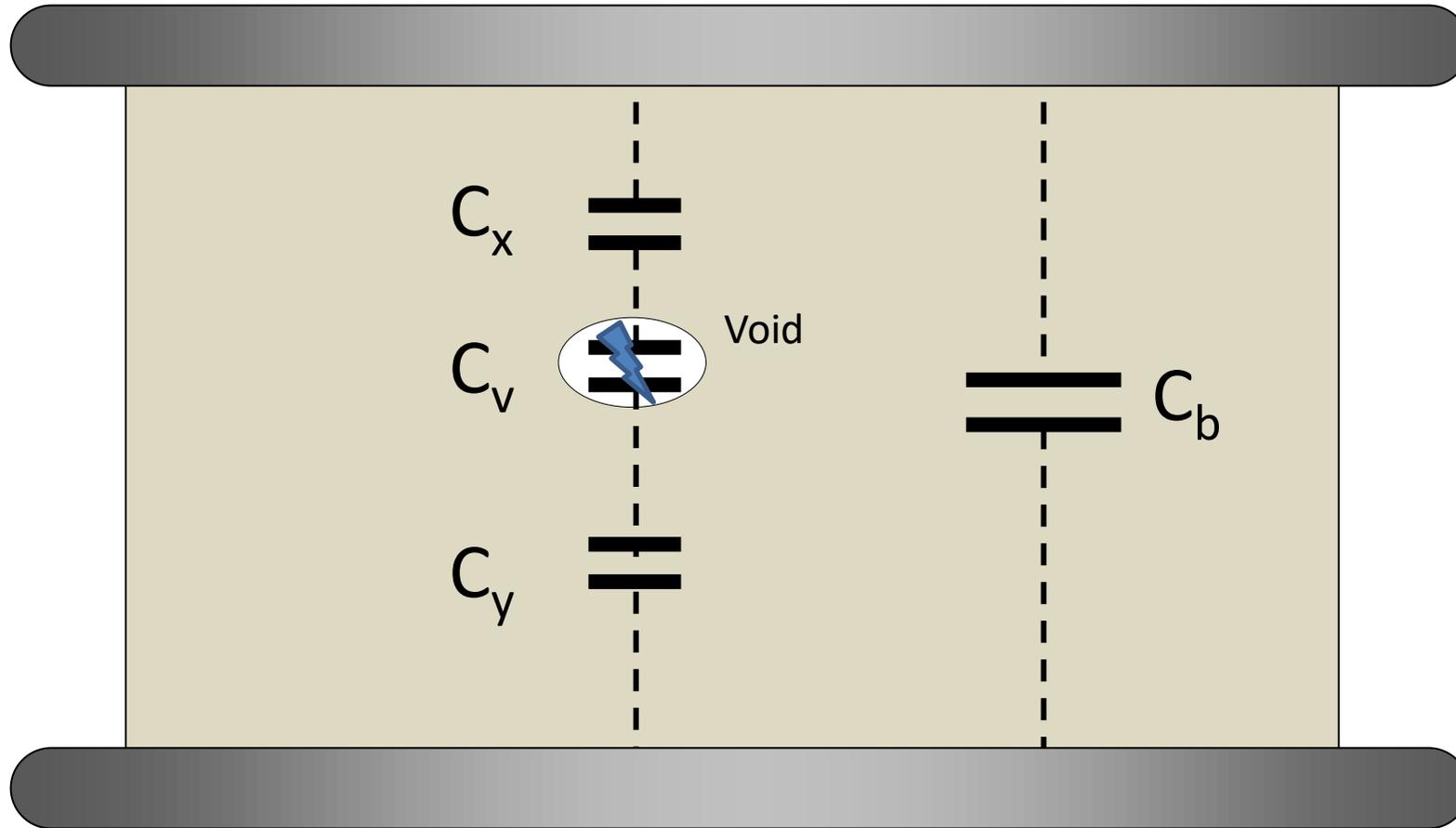
Outside
Ring



Electrical Breakdown

- Global Breakdown
 - Complete rupture or failure of the insulation between two electrodes
- Local Breakdown
 - Partial breakdown of part of the insulation between two electrodes
 - corona
 - partial discharge

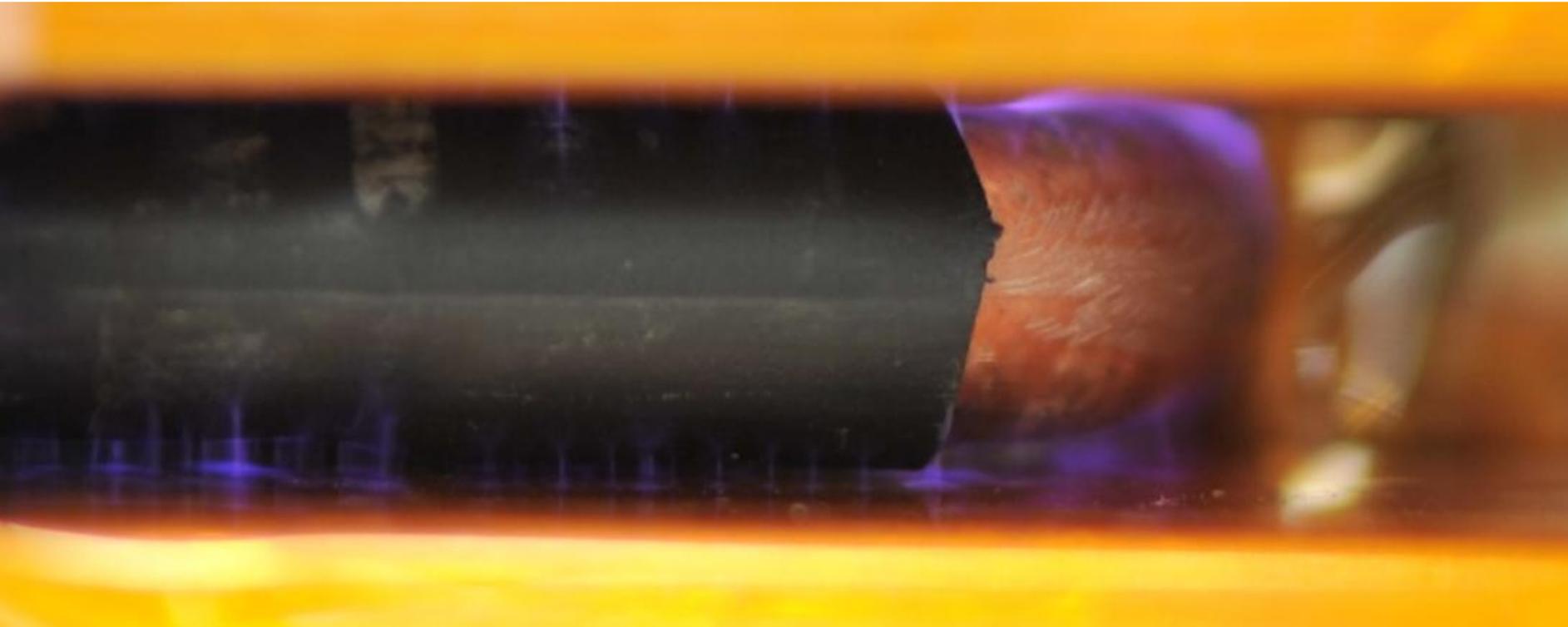
Partial discharges in voids



The largest volt drop is across the smallest capacitance

A cautionary tale

More insulation is not always a good idea...



Higher
permittivity
material pushes
the field into the
lower
permittivity area

Insulator Surface Tracking

- Partial discharge activity can chemically degrade insulator surfaces
- Insulators degrade to carbon
- Conductive carbon deposits can enhance fields, increasing partial discharge activity
- Carbonised tracks can grow across high voltage gaps over time
- Cleanliness and pollution are important factors
- Introducing convolutions into the surface increases the tracking length

Insulator Materials

Depends on application!

For example:

Al₂O₃ is commonly used in vacuum

AlN is used when a high thermal conductivity is required

Macor is used when a complex shape needs to be machined

Porcelain is used in compression

Epoxy resin is used to impregnate and pot

Mica is used for thin high voltage withstand

Glass is used when visible transparency is required

XLPE is used for extrusion in cables

Rexolite is used for high frequency RF

Commercial Insulators

- Dirt, dust and waterproof
- Sheds increase tracking length and protect sections of surface

A well designed insulation system is one you don't ever have to worry about





High voltage
platforms don't
have to be too
complicated, but...



Water and
home-made
insulators
don't mix



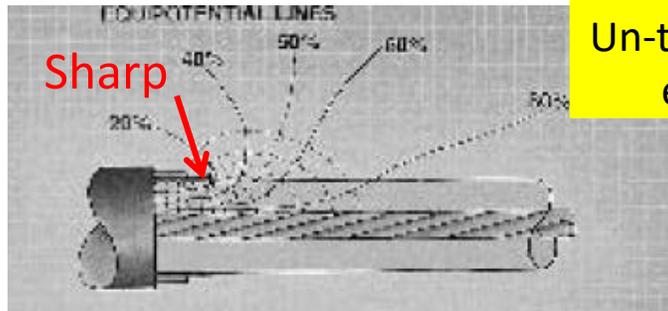


Commercial insulators are relatively cheap (\approx €200) and will work in all conditions

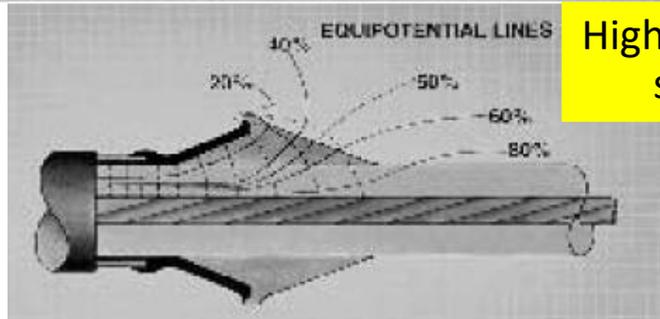


Cable terminations

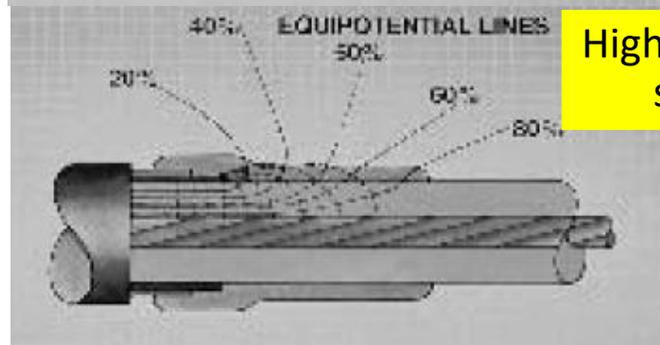
Correct electrostatic termination of high voltage cables is essential



Un-terminated earth screen



High permittivity stress cone



High permittivity sleeve



Stress cone electrode

Correct impedance termination of pulsed cables is also important – voltage reflections

Connectors and Feedthroughs



Depends on...

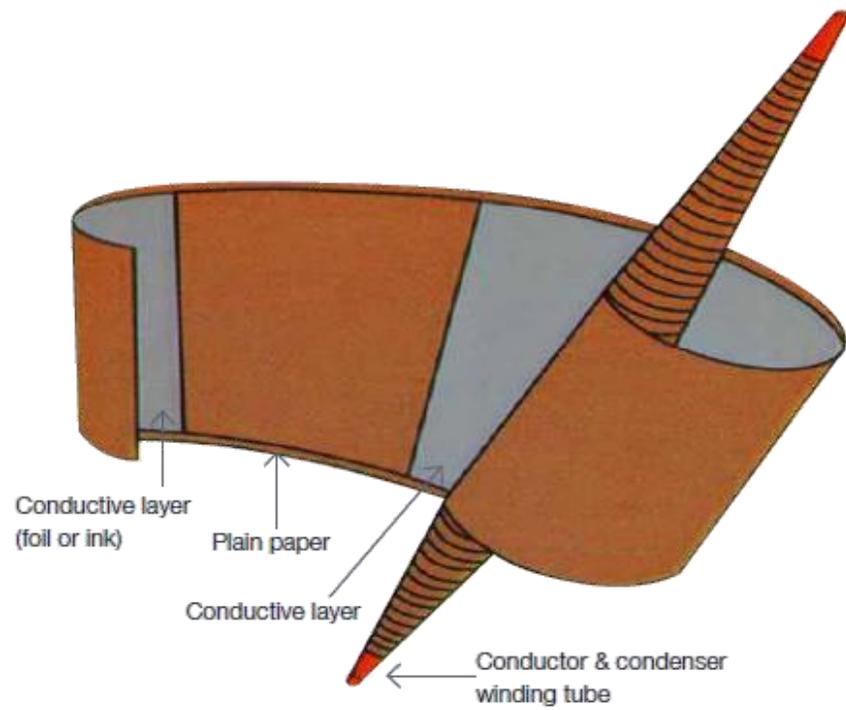
- Application
- Maintenance
- Permanence
- Voltage



> 50 kV needs
feedthroughs
or bushings



Big Bushings



Isolated Power

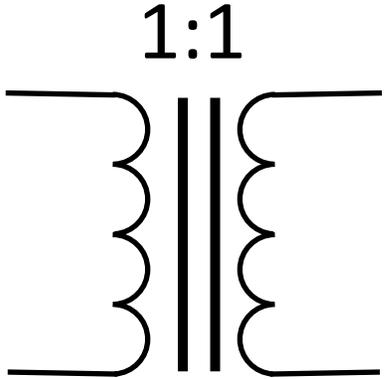
How to get mains power to equipment floating on a HV platform?



Motor- alternator set



Waveguide DC break



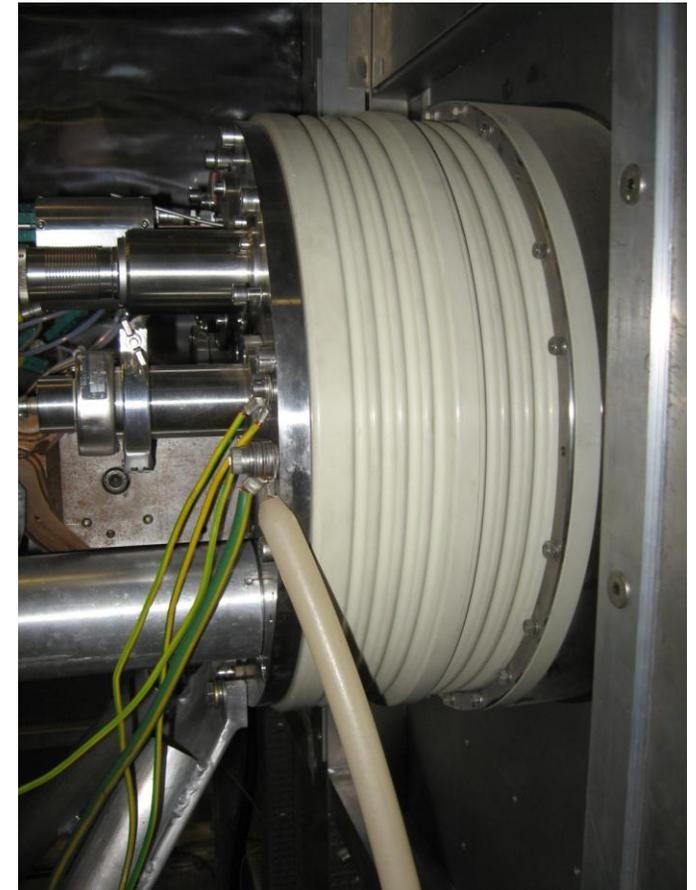
Isolation transformer

Earthing (Grounding)

- An earthing system should grow like a tree
- Provide a low impedance path to earth
- Avoiding parallel paths will prevent earth loops



Solid single point earth

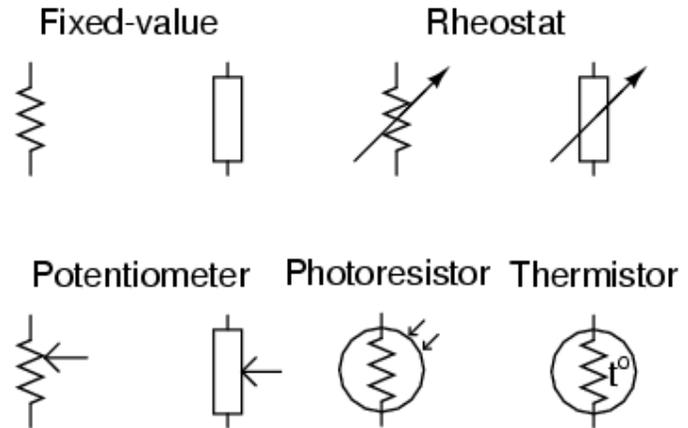


High voltage platform becomes
“Local earth”

Power Supply Technologies

- Transformers
- Semiconductors: Diodes, Transistors, Thyristors, IGBT
- Linear or switched mode
- Cascade rectifier (Greinacher/Cockcroft–Walton multiplier)
- Electron and gas discharge devices:
 - Tetrode, thyratron etc. for switching
 - Klystrons, magnetrons etc. for RF
- Pulse Forming Networks PFN
- Vandergraph, Peloton

Resistors



Resistance in Ohms Ω

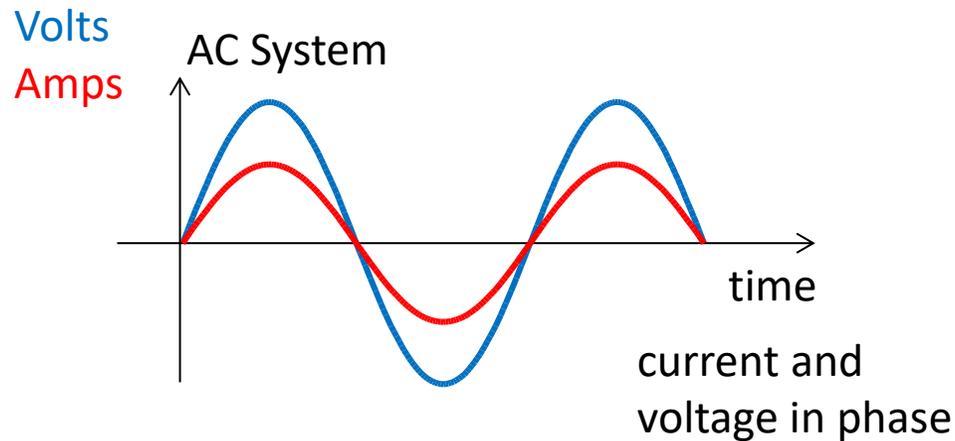
Power in Watts W

Voltage rating

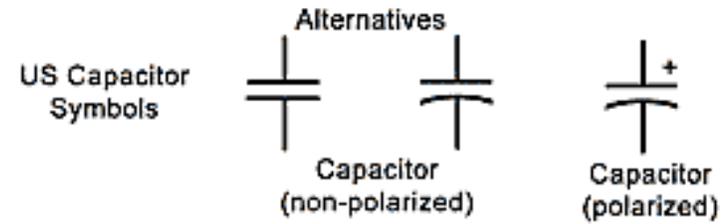
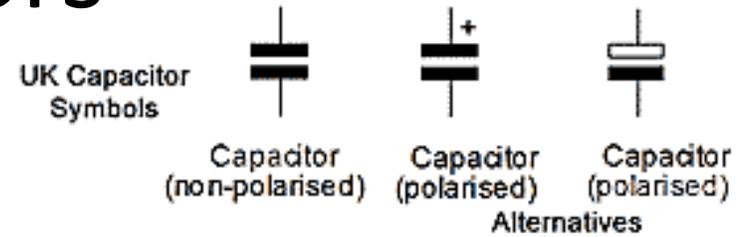
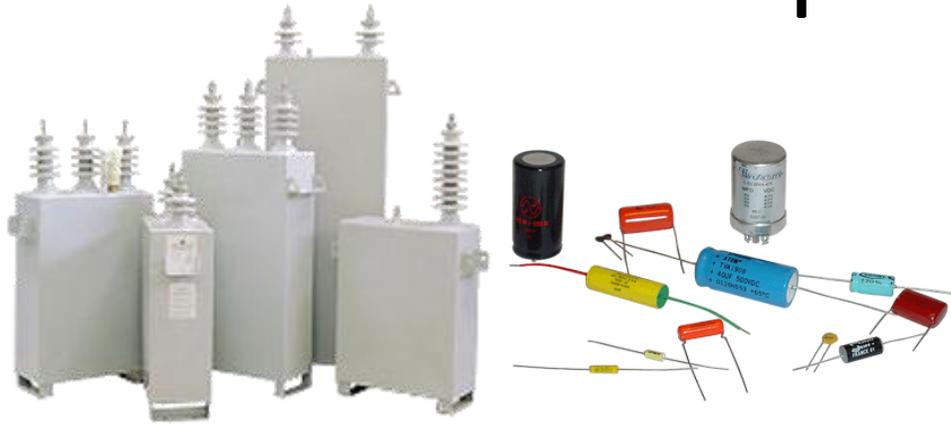
Tolerance in %

Ohms law $V = IR$

Power = $VI = I^2R = V^2/R$



Capacitors



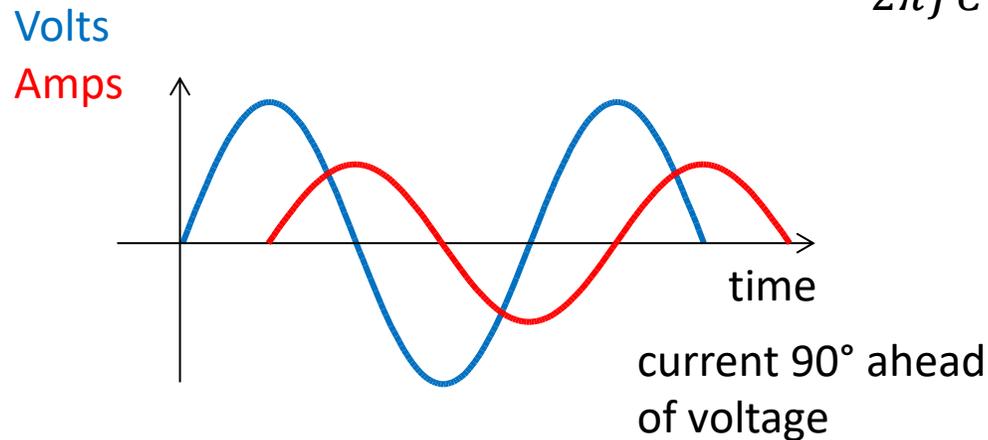
Frequency dependency

$$V = I X$$

$$V = I \frac{-j}{2\pi f C}$$

Capacitance in Farads, F

High pass filters



Inductors



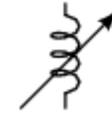
Fixed-value



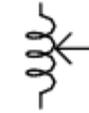
Iron core



Variable



Variac



Tapped



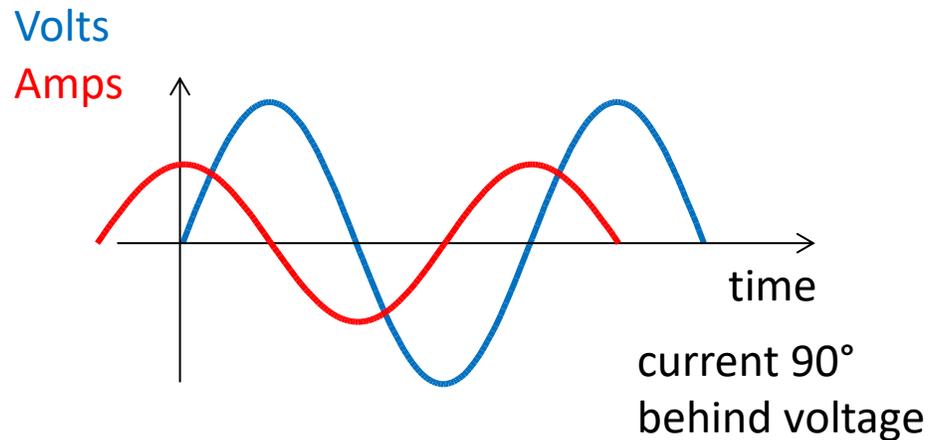
Frequency dependency

$$V = I X$$

$$V = I j2\pi Lf$$

Inductance in Henrys, H

Low pass filters



CIVIL

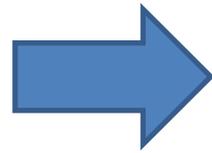
Particle Accelerator Magnets

Dipoles

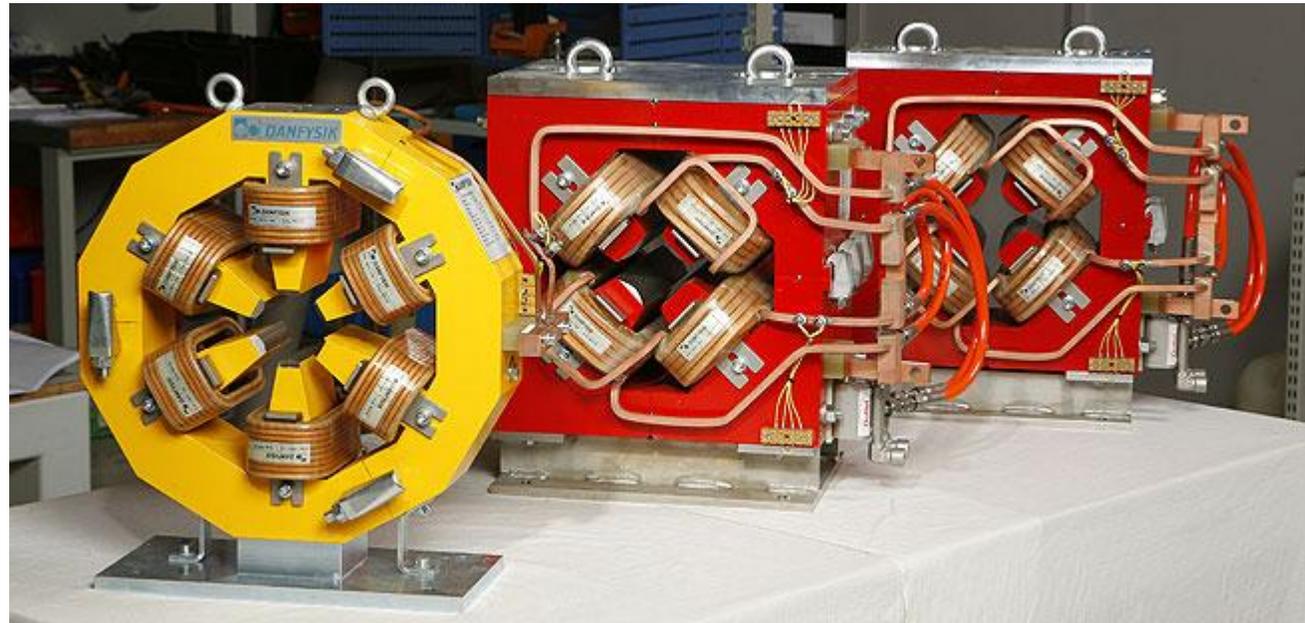
Quadrupoles

Sextupoles

Octupoles



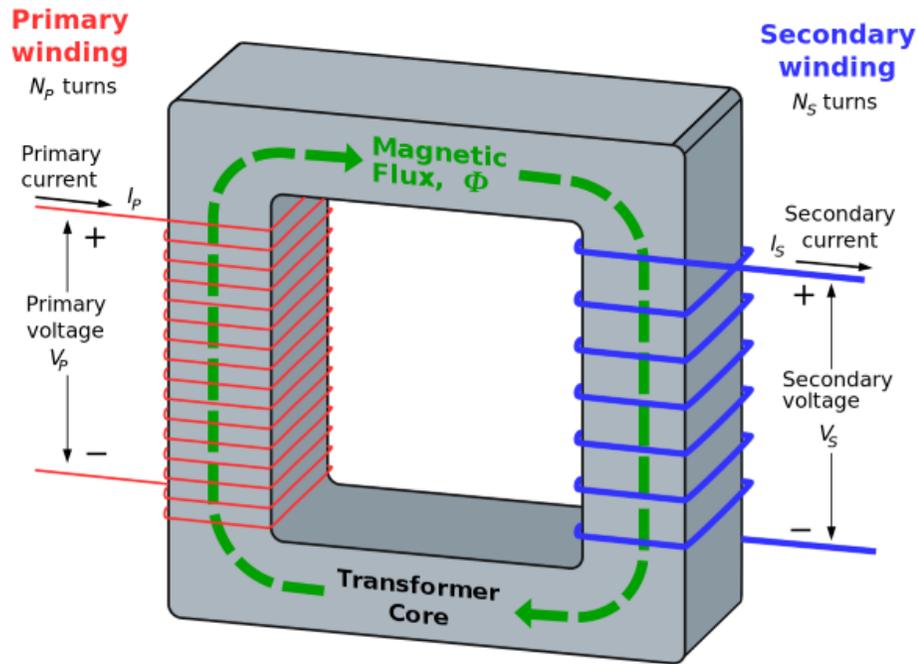
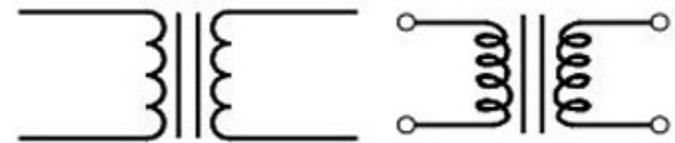
Inductors + small R
($<1\Omega$)



Transformers



Circuit diagram symbols



$$\text{Turns ratio} = \frac{N_p}{N_s}$$

Inductors that see the load through the transformer

Resonance

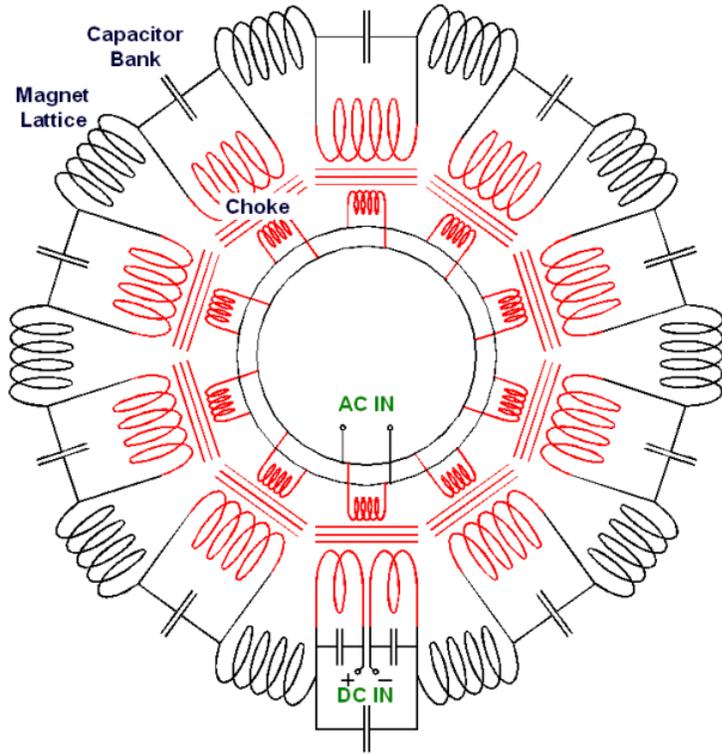
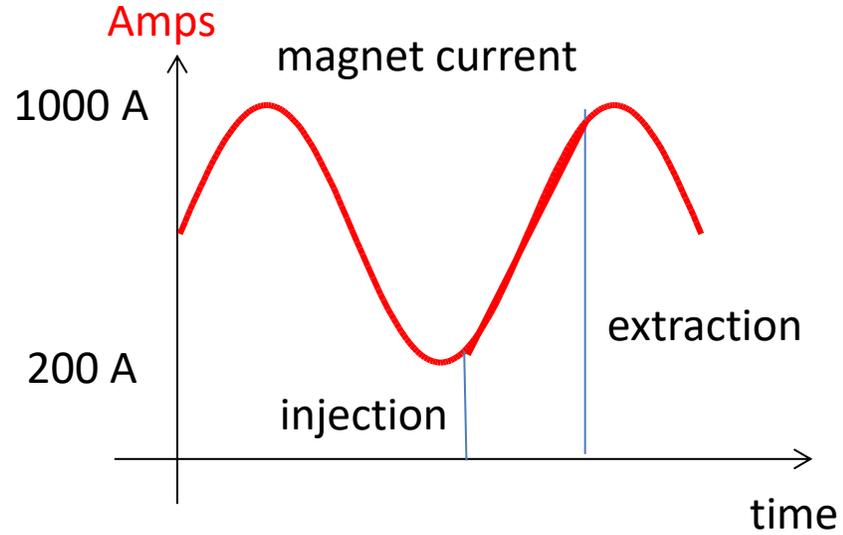


30 tonne dipole magnet (X10)



ISIS White Circuit

Synchrotron needs a magnetic field that rises in a few ms:

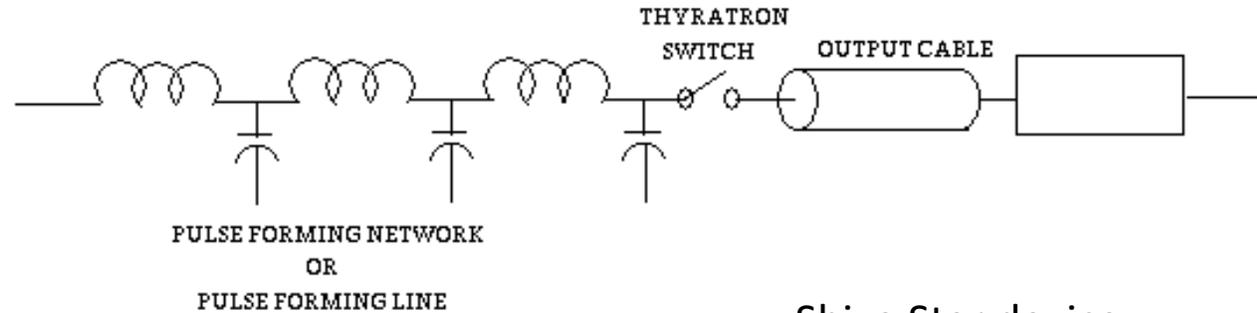


$662 A_{DC} + 400 A_{pk-pk} (50 Hz AC)$



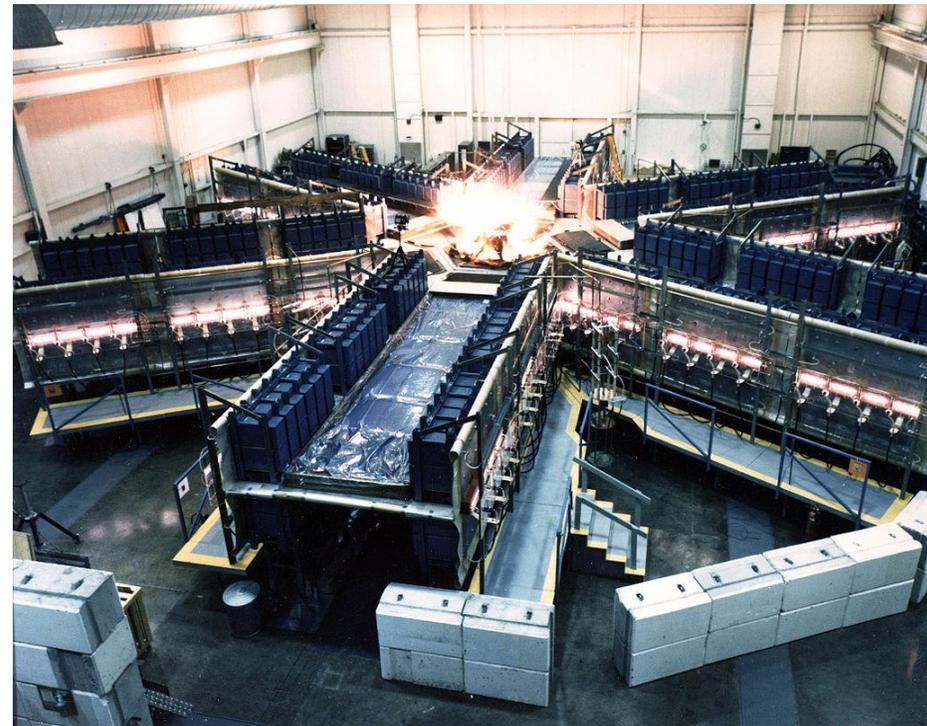
Pulse Forming Networks

Short pulses
Up to a few $1 \mu\text{s}$



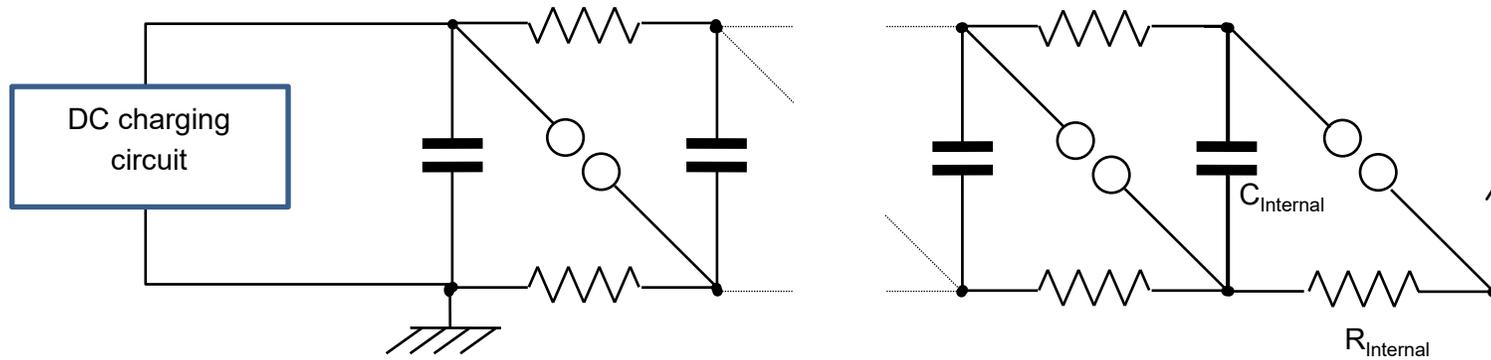
ISIS Extraction Kicker systems
500 ns 40 kV 5kA

Shiva Star device
 $1 \mu\text{s}$ pulses 120 kV and 6 MA



Marx Generators

Longer pulses
Up to a few 1 ms
and higher voltages

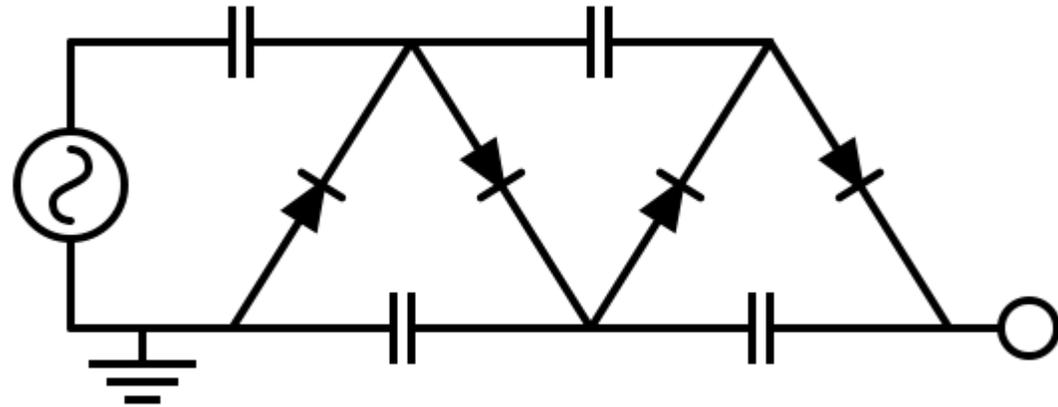


n stages charged in parallel
added in series by spark gaps

Very high pulsed voltages up to 20 MV



Cockcroft Walton Voltage Multipliers



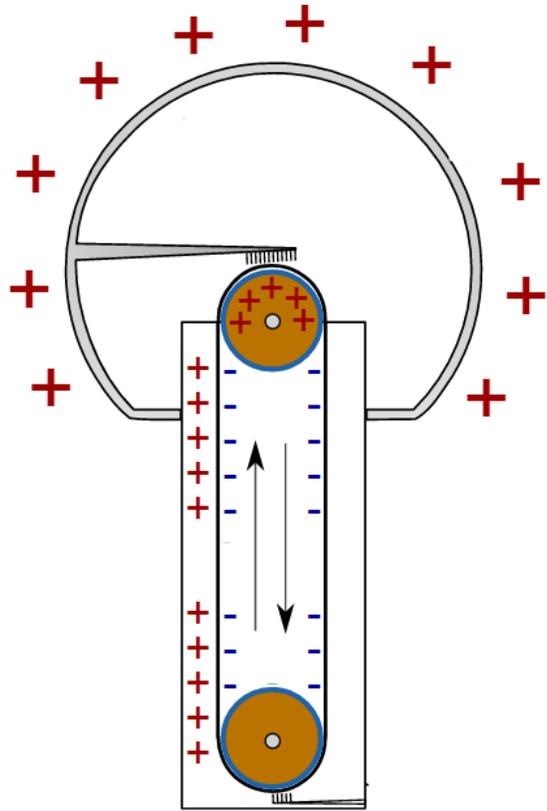
High Voltage DC



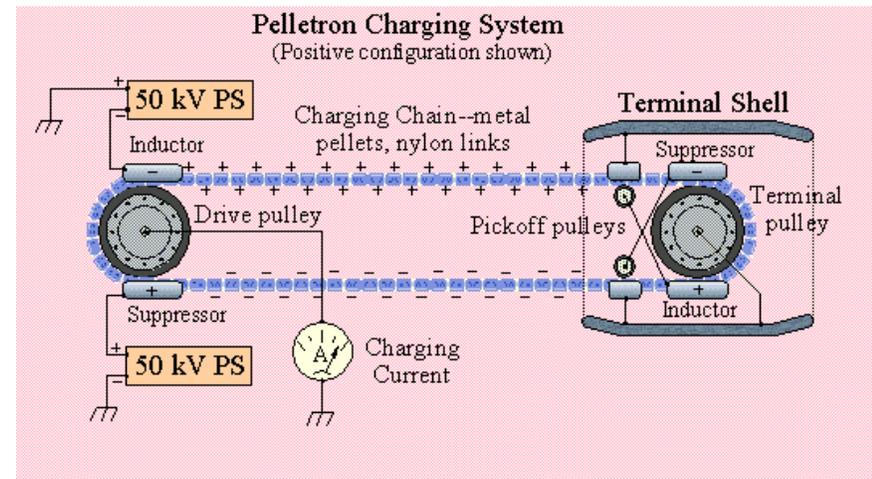
Old ISIS 665 kV preinjector

HV DC (mA)

Vandergraph, Pelletron



Daresbury 20 MV Vandergraph



Step-up transformer diode rectifier

HV DC (A)



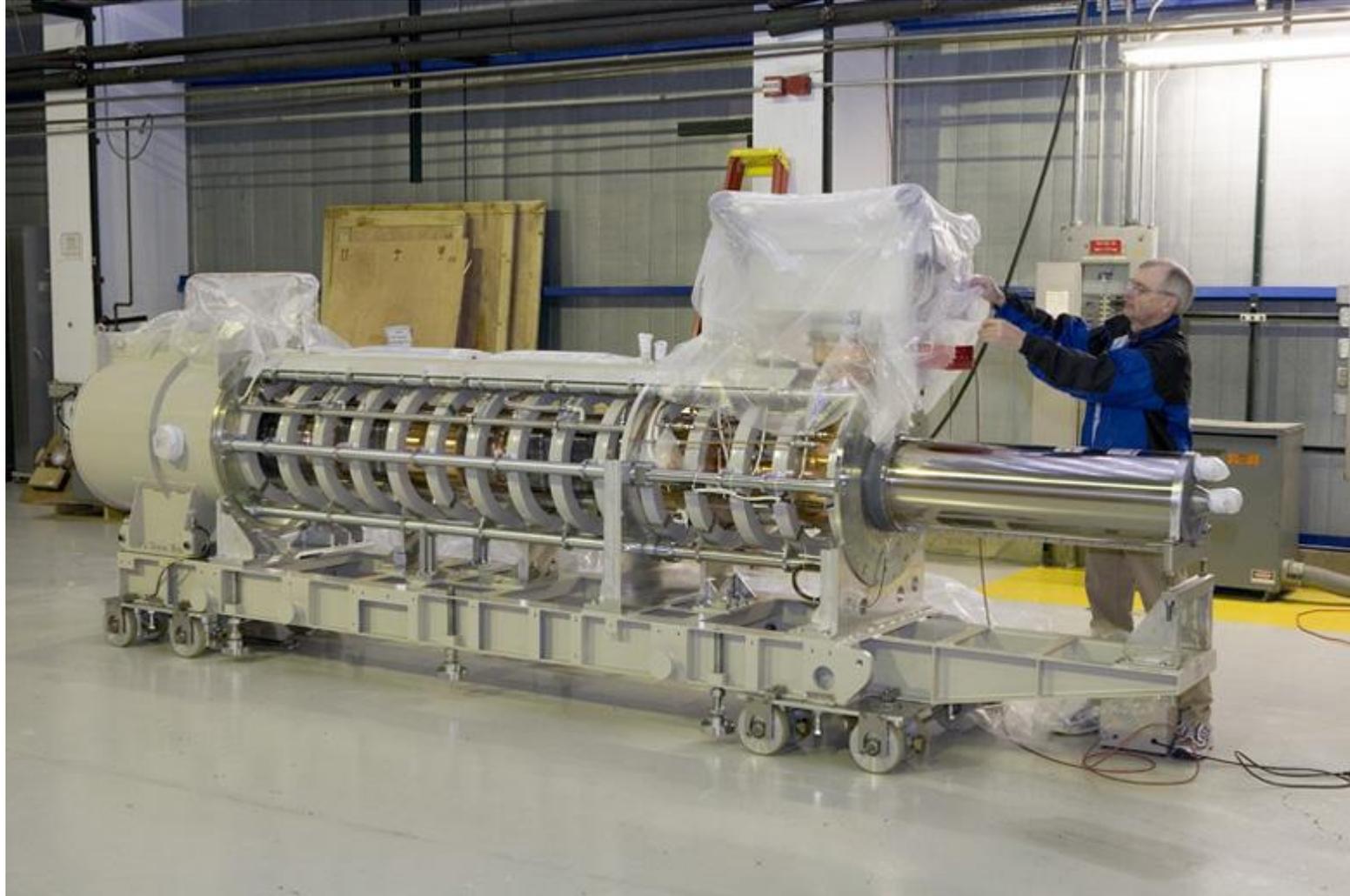
ITER NBI

1 MV 60 A



RF Klystrons

10 MW 100-1000 MHz



Power Electronics

SOLID STATE switches and amplifiers:

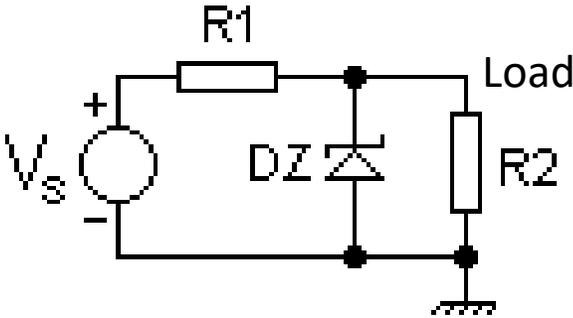
- Diodes, Zener etc.
- Transistors, Thyristors, IGBT, GTO, etc.

ELECTRON TUBES switches and amplifiers :

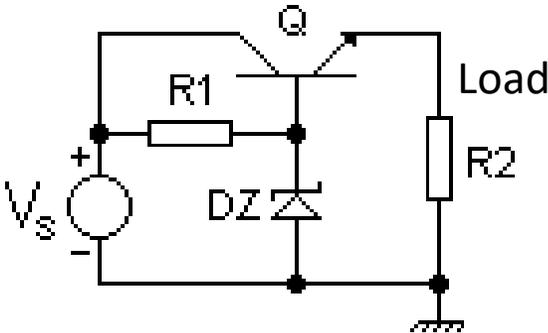
- Thyratron
- Tetrode
- Klystron, Magnetron, Gyrotron etc.

Linear vs Switched

Shunt

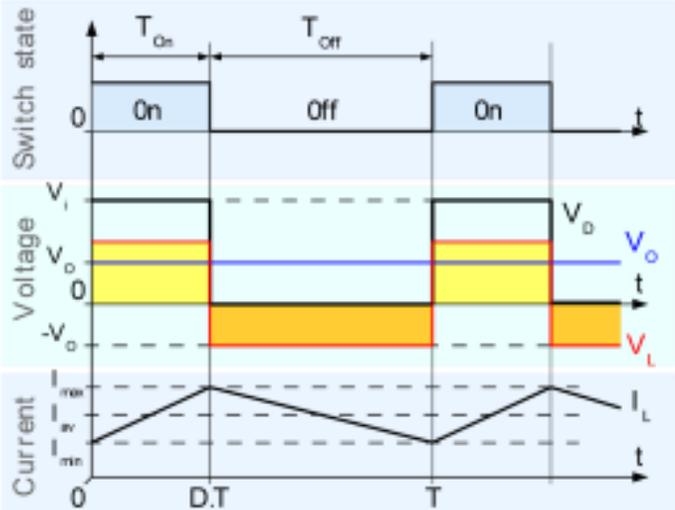
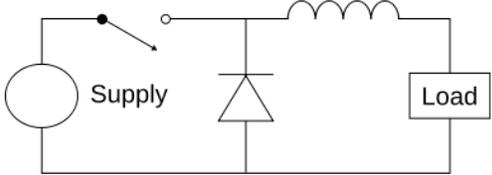


Series



Wasteful vs Noisy
 Quiet vs Efficient
 Heavy vs Light

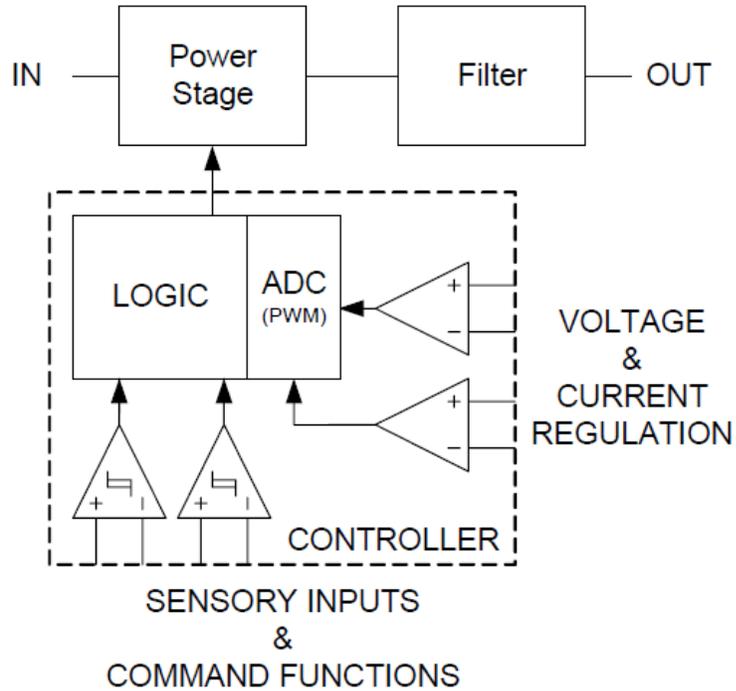
Buck Converter



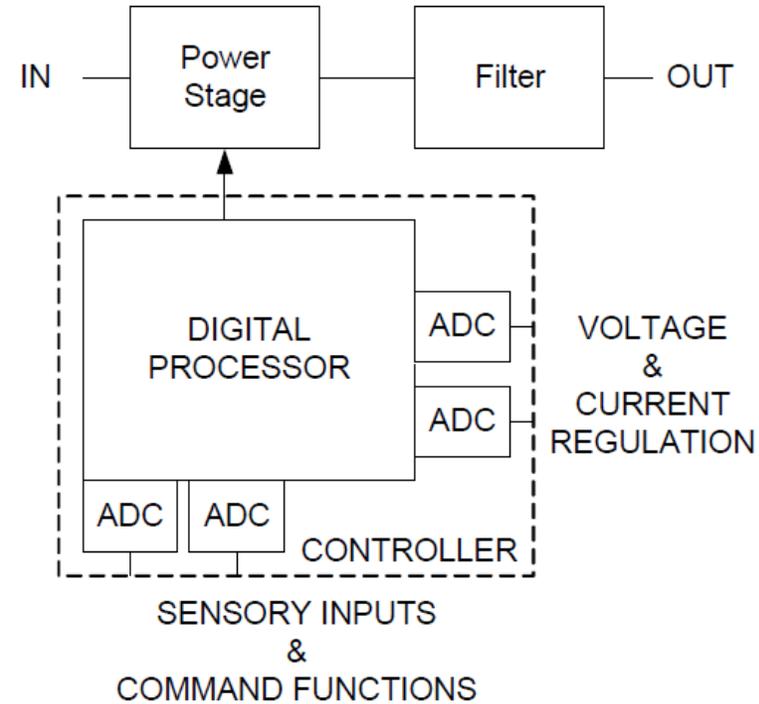
Duty cycle controls the average load voltage and current

Many other types of switched mode PS
 Boost, Buck-boost, Split-pi, Ćuk, SEPIC, Zeta, Switched capacitor, Flyback, Ringing choke converter, Half-forward, Forward, Resonant forward, Push-pull, Half-bridge, Full-bridge, Resonant, zero voltage switched

Digital Power Supply?



traditional
switched
mode



digital

High Voltage Power Supply Manufacturers



Custom Built Power Supplies

- Tight specification is essential if engaging a manufacturer
- Or of course you could make your own if you have the experience...

Safety

- Electric shocks can kill
- Stored energy in capacitors

$$\frac{1}{2}CV^2 = 0.5 \times 1 \mu\text{F} \times 30 \text{ kV} = 450 \text{ J}$$

- X-rays

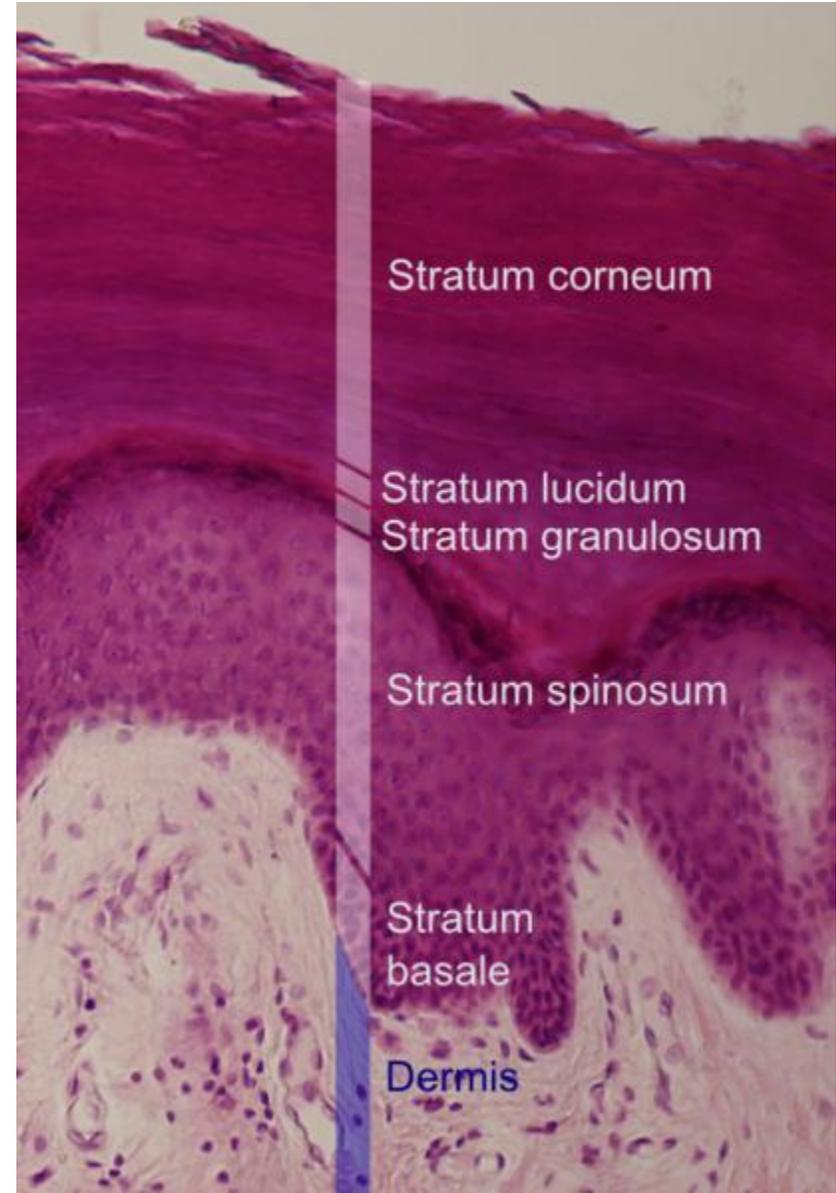
Electric Shocks

Hand to hand resistance:

100 k Ω dry/thick skin

1 k Ω wet/broken skin

- The stratum corneum breaks down 450–600 V leaving 500 Ω
- You can feel 5 mA
- 60 mA can fibrillate the heart



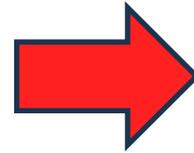
Functional Safety

IEC 61508

“Don’t do anything stupid”



The good ol' days



“Prove how safe it is”



Now

Functional Safety

IEC 61508

“Prove how safe it is”

- System analysis
- Safety Integrity Levels (SIL) ratings
- Failure mode analysis
- Inspection and maintenance regimes
- Documentation



HV Safety Philosophy

1. Impossible to accidentally lock someone in the HV area.
2. Ability to shut down the power inside and outside the HV area.
3. Impossible to power on the HV without locking the area.
4. Impossible to enter the HV area without making it safe.

HV Safety Philosophy

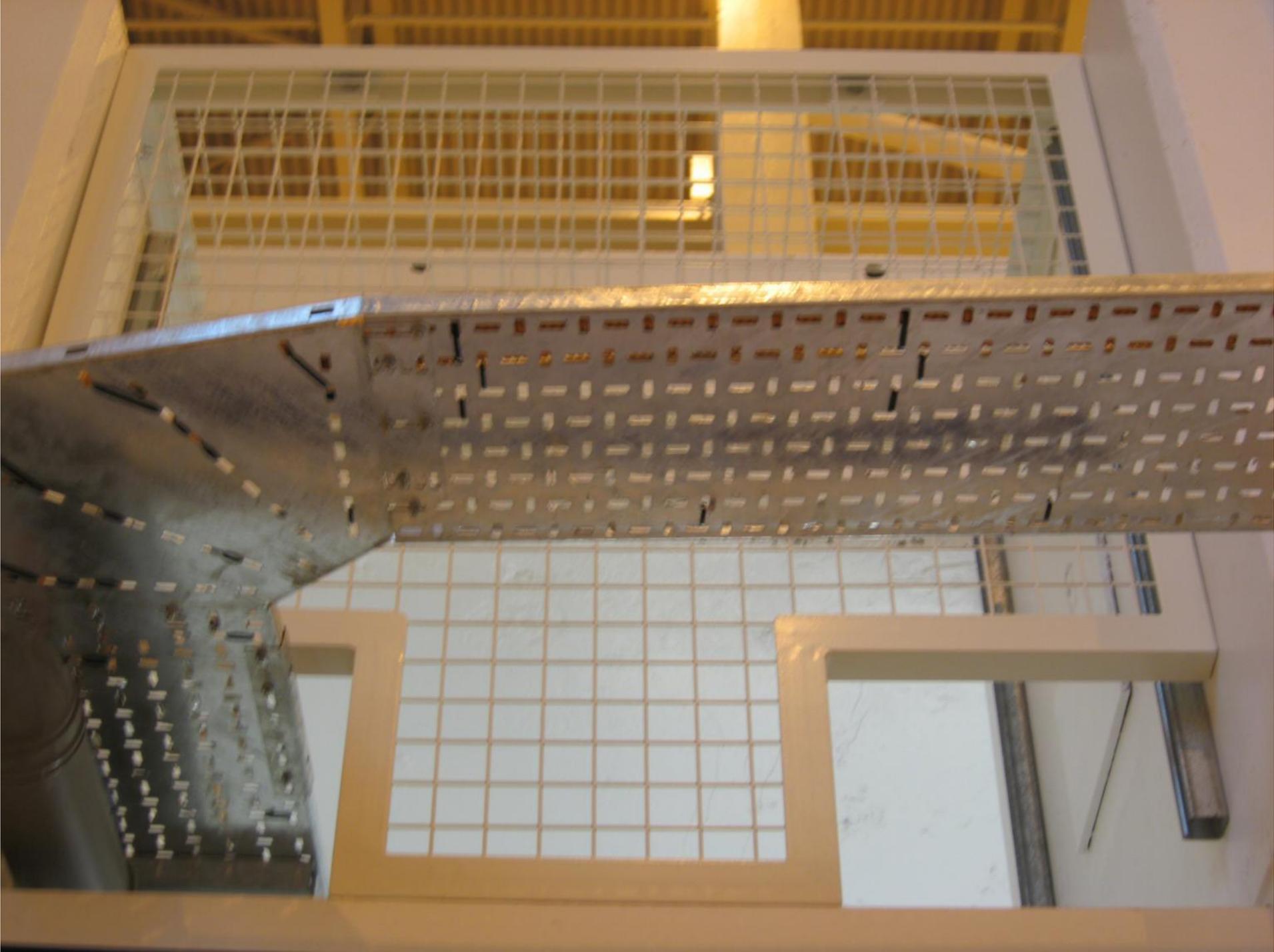
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4. Impossible to enter the HV area without making it safe.

SEARCH











SMASH GLASS TO OPEN
TUBE (RETRACT) OF I.C. EMERGENCY

   **Emergency Exit**
Break Glass Tube & Push Here

HV Safety Philosophy

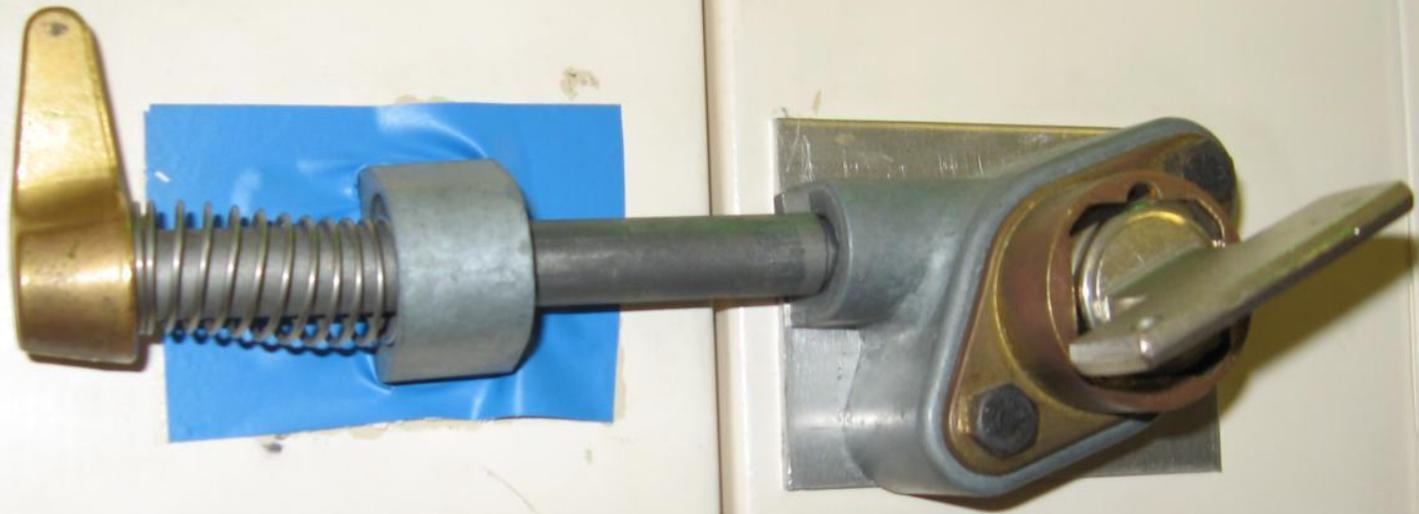
1. Impossible to accidentally lock someone in the HV area.
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HV Safety Philosophy

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BIAS 03



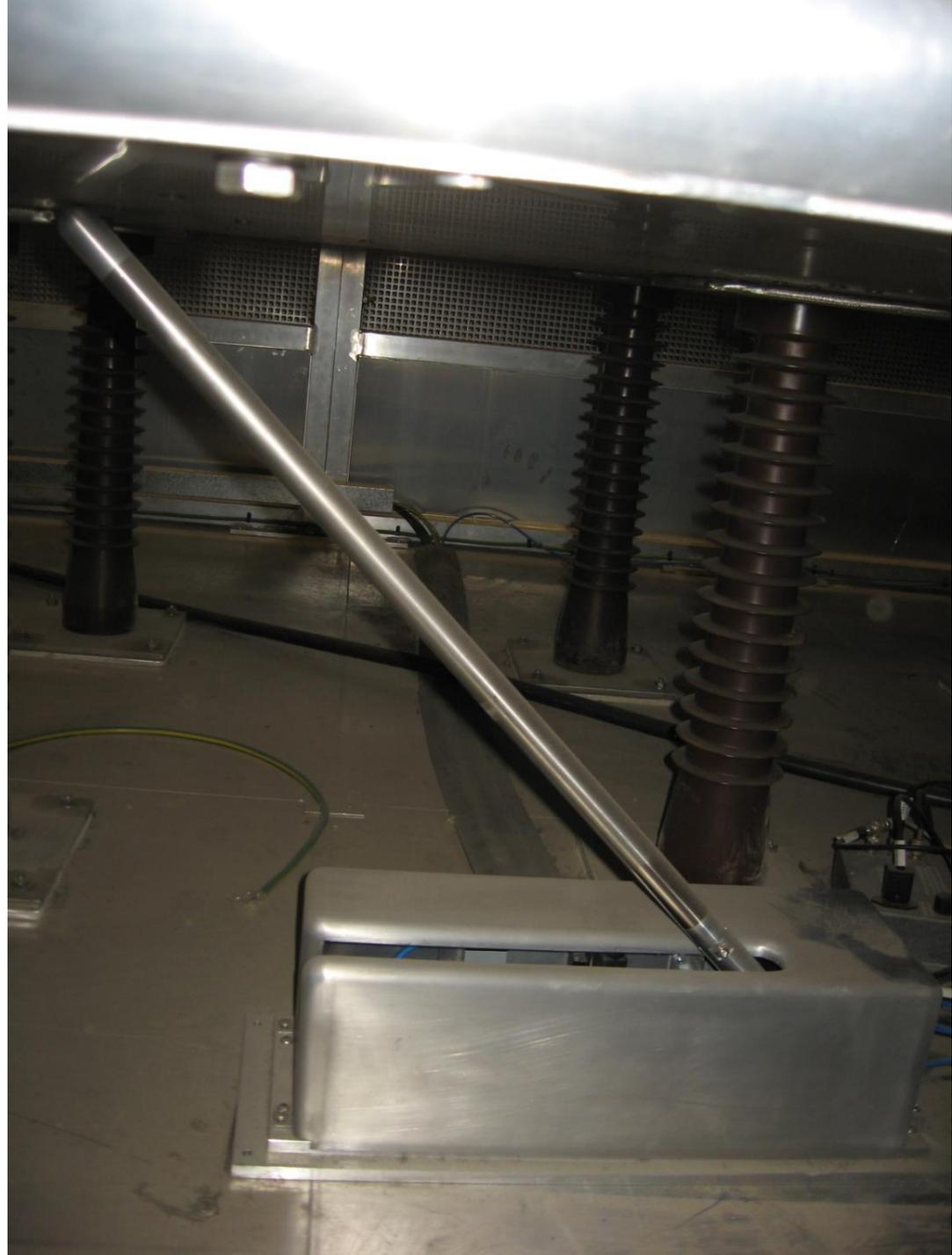
HV Safety Philosophy

1. Impossible to accidentally lock someone in the HV area.
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3. Impossible to power on the HV without locking the area.
4. Impossible to enter the HV area without making it safe.





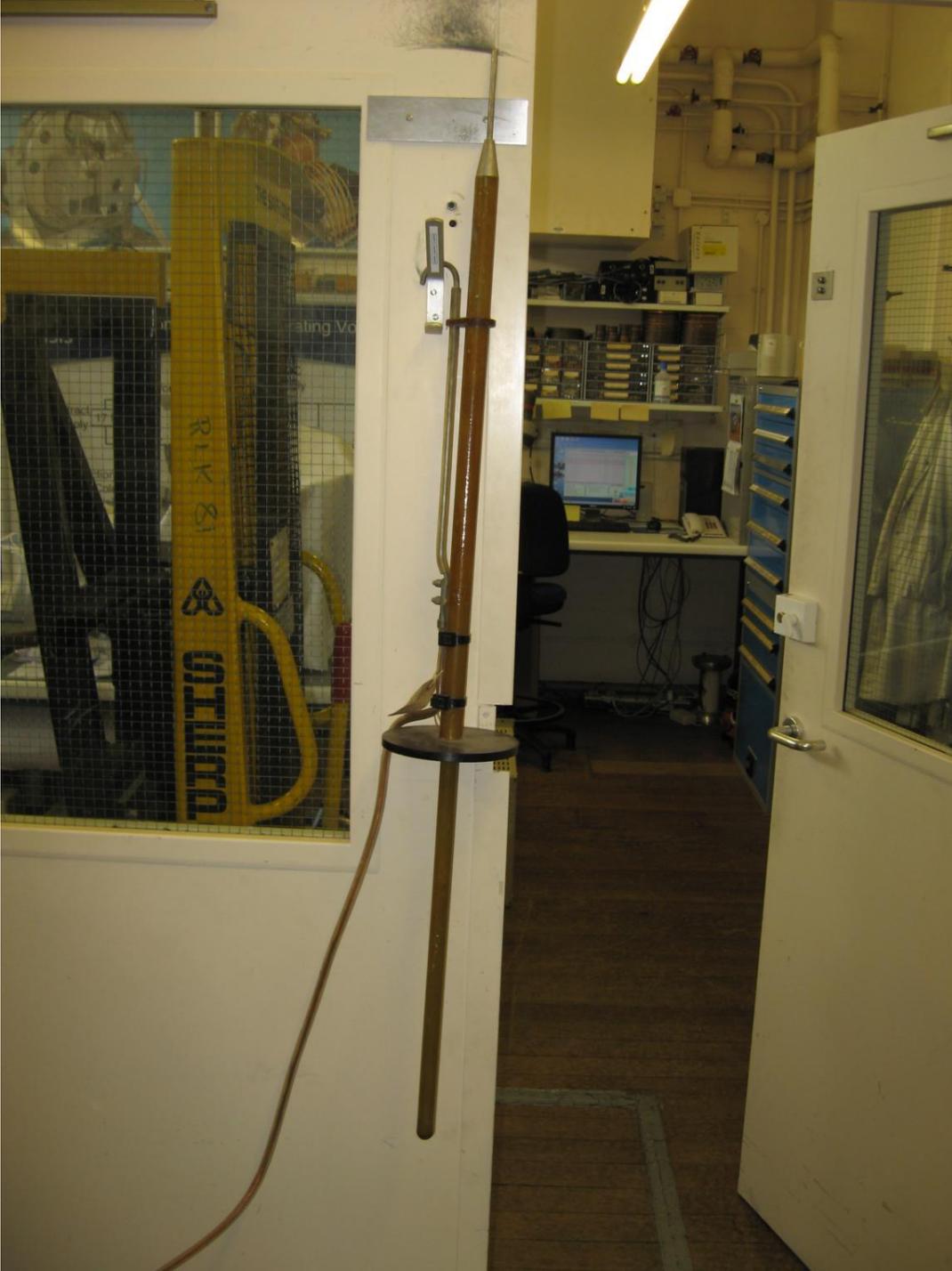
Automatic Earthing System



Earth Stick







Earth stick should be hung just inside the entrance of the high voltage area

You can never prevent humans from circumventing safety systems...



But you must make sure that they require some effort to **wilfully bypass**

Complacency and familiarity can kill!

Thank you for listening
Questions?